

RADC-TR-77-144 Phase Report April 1977

A PLASMA MODEL OF MISSILE EXHAUST PLUMES (Axial and Radial Conductivity Distributions for the Redeye Missile)

Georgia Institute of Technology

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered READ INSTRUCTIONS REPORT DOCUMENTATION PAGE BEFORE COMPLETING FOR 1. GOVT ACCESSION NO. 1. RECIPIENT'S CATALOG NUMBER RADC TR-77-144 FERIOD COVERED A PLASMA MODEL OF MISSILE EXHAUST PLUMES . Phase Repeat (Axial and Radial Conductivity Distributions for the Redeye Missile). PERFORMING ORG. REPORT HUMBER N/A . AUTHORA B. CONTRACT OF GRANT HU BER(s) John D. Nogard Glenn S./Smith F39692-75-C-9118 PERFORMING ORGANIZATION NAME AND ADDRESS Georgia Institute of Technology Atlanta GA 30332 11. CONTROLLING OFFICE NAME AND ADDRESS Rome Air Development Center (RBC) Griffies AFB NY 13441 14. MONITORING ASENCY NAME & ADDRECS(II different from Controlling Office) Same UNCLASSIFIED 18a. DECLASSIFICATION/DOWNGRADING N/ASCHEDULE 16. DISTRIBUTION STATEMENT (of this Record) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the abstract entered in Black 20, If different from Report) 10. SUPPLEMENTARY TES RADC Project Engineer: Jacob Scherer (RBC) 19. KEY WOROS (Continue on reverse side if necessary and identify by block number) Electromagnetic Compatibility Missile PLUME Plasma Electromagnetics P. ABSTRACT (Continue on ruverse side if nequency and identify by block member) The effort reported on is part of a program to completely specify the susceptibillity effects of the electromagnetic environment on weapon systems. Since the electromagnetic coupling into a system is dependent upon skin currents, the electrical properties and the effects of the ex'sus' plume must be completely determined. This report provides a mathematical description of the chemical and electrical characteristics of a typical tactical rocket. In particular the coaxial and radial distributions of the constitutive parameters

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PREFACE

This effort was conducted by Georgia Institute of Technology under the sponsorship of the Rome Air Development Center Post-Doctoral Program for RADC. Jack Edwards of RADC/RBCA was the task project engineer and provided overall technical direction and guidance.

The RADC Post-Doctoral Program is a cooperative venture between

RADC and some sixty-five universities eligible to participate in the program.

Syracuse University (Department of Electrical Engineering), Purdue University

(School of Electrical Engineering), Georgia Institute of Technology (School of Electrical Engineering), and State University of New York at Buffalo

(Department of Electrical Engineering) act as prime contractor schools with other schools participating via sub-contracts with the prime schools. The

U.S. Air Force Academy (Department of Electrical Engineering), Air Force

Institute of Technology (Department of Electrical Engineering), and the

Naval Post Graduate School (Department of Electrical Engineering) also

participate in the program.

The Post-Doctoral Program provides un opportunity for faculty at participating universities to spend up to one year full time on exploratory development and problem-solving efforts with the post-doctorals splitting their time between the customer location and their educational institutions. The program is totally customer-funded with current projects being undertaken for Rome Air Development Center (RADC), Space and Missile Systems Organization (SAMSO), Aeronautical Systems Division (ASD), Electronics Systems Division (ESD), Air Force Aviolics Laboratory (AFAL), Foreign Technology Division (FTD), Air Force Weapons Laboratory (AFWL), Armament Development and Test

Center (ADTC), Air Force Communications Service (AFCS), Aerospace Defense Communications Agency (DCA), Navy, Army, Aerospace Medical Division (AMD), and Federal Aviation Administration (FAA).

Further information about the RADC Post-Doctoral Program can be obtained from Mr. Jacob Scherer, RADC/RBC, Griffiss AFB NY 13441, telephone Autovon 587-2543, commercial (315) 330-2543.

The authors would like to acknowledge the assistance of the following people at MICOM, Huntsville, Alabama, for providing support during the LAPP rocket exhaust analysis: Captain R. Darone, Dr. G. Brown, Dr. W. Walker, and Dr. W. Jenkins.

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I. INTRODUCTION

It is well known that skin currents on a missile may be greatly modified in the presence of the exhaust plume, since any electromagnetic radiation incident on the rocket body will also penetrate through the exhaust plume, created by the rocket motor. Therefore, to completely specify the electromagnetic environment of the rocket in powered flight, the electrical properties of the exhaust plume must be calculated from a knowledge of the chemical/thermodynamic reactions and mixing schemes which are thought to occur along the turbulent wake of the rocket's trajectory.

cription of the chemical and electrical characteristics of the ricket exhaust plume of a typical tactical rocket, such as the Redeye Missile. In particular, the axial and radial distributions of the electrical constitutive parameters in the wake of the rocket are developed from a plasma model of the exhaust plume. These data must be known before a physical model (simulator) can be constructed and used in an experimental measurement program, and they are also necessary for a forthcoming theoretical electromagnetic analysis of the rocket with and without a plume which will show the effect of the exhaust plume on the susceptibility of the ricket to electromagnetic radiation.

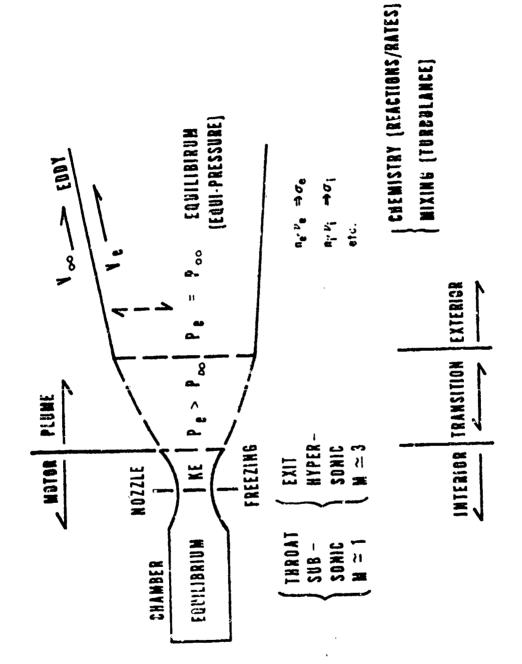


FIGURE 1. Schematic Representation of the Rocket Motor & Exhaust Plume

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II. MON-EQUILIBRIUM PLUME PREDICTIONS

In an effort to obtain an accurate numerical solution for the plume electrical parameters, three computer codes have been considered:

- i. "Low Altitude Plume Program" (LAPP) which was supplied by MICOM/Huntsville.
- ii. "Rocket Exhaust Plume" codes (REP-3 and REP-4)
 developed at the Imperial College, London and
 marketed in North America by Combustion, Heat
 and Momentum, Incorporated (CHAM).
- iii. "Naval Weapons Center" code (NWC) at NWC/China
 Lake, CA and available at Thiokol Chemical
 Corporation, Brighman City, Utah.

A. Description of the Exhaust Plume Computer Codes

The calculation of the properties of the rocket exhaust can be separated into two parts, viz., an interior problem inside the motor chamber and nozzle and an exterior problem outside the motor in the ambient atmosphere, cf., Figure 1.

The interior problem begins with an equilibrium solution of the thermo-chemical problem in the motor chamber; this is followed by a non-equilibrium expansion through the nozzle to the exit plane of the motor. The solution to the interior problem provides parameters at the exit plane that are used in the plume calculation, i.e., the exterior problem. Typical inputs to the computer programs which solve the exterior problem are the following radial distributions over the infinite plane that is coincident with the exit plane of the nozzle:

- i. species concentrations
- ii. pressure
- iii. temperature
- iv. velocity
- v. size, number and velocity distributions of the liquid particles (if any are to be considered)
- vi. base geometry (if it is to be considered).

Additional information must be specified to solve the external problem, such as the reactions to be considered and their rates, the electron and ion collision cross-sections, ambient pressure, P_{∞} , and the velocity of the rocket, V_{∞} .

The LAPP code uses either a Donaldson-Grey or a Ting-Libby eddy viscosity model to calculate a non-equilibrium solution of the thermochemical reaction problem in the plume. No radial pressure variations are included in this code. The NWC code is a simplified version of the LAPP code and only produces an equilibrium solution of the thermochemical reaction problem in the plume. In both of these codes, there is a non-equilibrium expansion region from the exit plane exhaust pressure, P_{ω} , to the ambient atmospheric pressure, P_{ω} .

The REP-4 code includes the following items which are not considered by the LAPP or NWC codes:

- 1. lateral momentum equations
- 2. multi-phase flow
- 3. slip (drag) of solid or liquid particles
- 4. kinetic heating

- 5. radiation
- 6. base geometry

The REP-3 coa: is an earlier and less sophisticated version of the REP-4 code; however, the REP-4 code requires additional development before it can be applied directly to the problem in this study.

Decause of the high cost of the REP-4 code, a decision was made to purchase a single run of the REP-3 code for comparison with the LAPP and NWC codes.

The firal computer runs of these codes for the Redeye missile used the following parameters:

- i. the latest JANNAF reactions/rates
- ii. the ambient pressure of 0.832 atmospheres corresponding to an altitude of approximately 5000 feet
- iii. the velocity of the rocket near zero, which
 corresponds to a static-firing (velocity = 0)
- iv. nozzle radius 0.0484"
- v. Lewis Number = 1; Prandtl Number = 1
- vi. Jed velocity = 8644 fps; Edge velocity = 10 fps
- vii. Jet temperature = 2116°K; Edge temperature = 278°K

Also, at the exit plane, the following mole fractions of the solid propellant constituents were assumed.

	<u>jet</u>	EDGE
СО	2.70x10 ⁻¹	0
co ₂	5.84x10 ⁻³	0
C£	2.42x10 ⁻³	0
н	8.53x10 ⁻³	o
HCL	1.61×10 ⁻¹	0
H ₂	4.22x10 ⁻¹	0
н ₂ 0	5.18x10 ⁻²	0
N ₂	7.79×10 ⁻²	7.90×10 ⁻¹
0	1.83×10 ⁻⁶	0
ОН	1.25×10 ⁻⁴	o
02	1.03×10 ⁻⁷	2.10x10 ⁻¹
KCL	1.12×10 ⁻⁵	0
ĸ	1.37×10 ⁻⁷	O
NaCl	1.20×10 ⁻⁴	0
Na	5.31×10 ⁻⁶	0
Cl-	3.31×10 ⁻⁶	0
ĸ+	3.14×10 ⁻⁷	0
Na ⁺	1.71×10 ⁻⁷	0
e ¯	3.46×10 ⁻⁸	o

III. ROCKET EXHAUST PLUMES

The exhaust plume through which the incident electromagnetic wave must travel is in the plasma state, i.e., due to the relatively high exit temperatures of the gases which are propelled out of the rocket motor nozzle (T = 3000°K), some of the chemical species in the exhaust gases are singely ionized. On the average, the exhaust plume forme a macroscopically neutral ionized gas consisting principally of light and very mobile free electrons and heavy and less mobile free ions of both polarities The electron and positive and negative ion gases are both embedded in a cloud of relatively immobile neutral atoms and molecules. The presence of a static or quasi-static magnetic field, e.g., the earth's magnetic field, will tend to bias the plasma to the extent that the plasma may become anisotropic to the passage of an electromagnetic wave. If the temperature of the plasma is very high, then the plasma can support pressure (acoustic) waves. Also, if the intensity of the incident radiation is very high, then the wave may experience some non-linear effects.

To apply these considerations to the case of an electromagnetic wave passing through the plasma plume of a rocket, it is noted that the wave, in principle, interacts with all three components of the plasma, viz., the free electrons, the free ions (both polarities), and the neutral particles. However, the interaction of the wave with the neutral particles is so small due to their low mobilities in comparison to the interactions between the wave and the charged particles that it can be neglected. Normally, since the ions are much more massive than the electrons (typically, $m_i \simeq 50,000 \ m_g$), the velocity imparted to the

ions by the wave is usually negligibly small compared to the velocity given to the electrons. Usually, the resulting ion convection current in the plasma is much smaller than the electron convection current. However, in a rocket plume, the ion collision frequency is much less than the electron collision frequency (typically, $v_i \approx 5 \times 10^{-3} v_e$), and the ion species number density (due to simple dissociation) is much larger than the electron number density (typically, $n_i \approx 1,000 n_e$). Collectively, then, the reduced ion collision frequency and the enhanced ion number density can compensate for the reduced mobility of the ions and may result in an ion conductivity which is greater than the electron conductivity in certain regions of the wake. Thus, a two fluid model, viz., an electron fluid and a combined negative and positive ion fluid, is needed to accurately describe the plasma plume.

The intensity of the electromagnetic radiation incident on the plasma plume in a typical in-flight environment is not large enough to introduce non-linear effects into the wave propagation, but it is large enough to dominate the static magnetic field bias of the earth's weak magnetic field. Therefore, for simplicity, the plume is modeled as a linear and isotropic plasma. Also, the temperature of the exhaust gases are not high enough to support any significant pressure waves; therefore, for simplicity, the plume is modeled as a "cold" plasma.

A. Plasma Model

With the above assumptions, the equation of motion for the velocity \underline{v} of an isolated electron or ion due to interactions resulting from a Lorentz force $\underline{F}_{e/m}$, a temporal change in moment \underline{P} , a spacial change in stress \underline{S} , and a biasing force \underline{F}_{0} , is given in the "time" domain by

$$\underline{\underline{w}} = \underline{\underline{r}}_{e/m} - \underline{\dot{p}} - \underline{\underline{v}} \cdot \underline{\underline{s}} + \underline{\underline{r}}_{0}$$

where:

$$\frac{\dot{\mathbf{a}}}{\dot{\mathbf{a}}} = \frac{\mathbf{d}\mathbf{f}}{\mathbf{q}} \cdot \mathbf{a} = \frac{\mathbf{g}\mathbf{f}}{\mathbf{g}} \cdot \mathbf{a} + \mathbf{a} \cdot \mathbf{a} = \frac{\mathbf{g}\mathbf{f}}{\mathbf{g}} \cdot \mathbf{a}$$
 (\vec{\vec{a}}{\vec{a}} \vec{\vec{a}}{\vec{a}} \vec{a} \vec{0})

$$\frac{\mathbf{F}}{\mathbf{e}/\mathbf{m}} = q(\mathbf{E} + \mathbf{v}\mathbf{A}\mathbf{B}) \simeq q\mathbf{E}$$
 (B << E)

$$\frac{\dot{\mathbf{P}}}{\mathbf{P}} = (\mathbf{m}\mathbf{v}) \mathbf{v}$$

$$\underline{S} \approx 0$$
 (T ≈ 0)

$$\underline{\mathbf{F}}_{0} = \underline{\mathbf{q}}\underline{\mathbf{v}}\underline{\mathbf{h}}\underline{\mathbf{g}}_{0} \simeq 0 \qquad \qquad (\mathbf{B}_{0} << \mathbf{E})$$

where ν is the measured collision frequency and q is the charge carried by the species. In the "frequency" domain, with $e^{-i\omega t}$ time variation, the equation of motion reduces to

$$-i\omega m\underline{v} = q\underline{E} - m\underline{v}v$$

The solution of the equation of motion for the velocity v is simply

$$\underline{\mathbf{v}} = \frac{\mathbf{q}\mathbf{E}}{\mathbf{m}(\mathbf{v} - \mathbf{i}\mathbf{\omega})}$$

If the convection current density \underline{J} is defined by

$$J = nqv$$

where n is the number density of the species considered, then a complex conductivity σ_c , or, equivalently, areal and imaginary conductivity σ_r and σ_i , can be defined as

$$\underline{\mathbf{J}} = \sigma_{\mathbf{C}} \underline{\mathbf{E}} = (\sigma_{\mathbf{r}} + \mathbf{i} \ \sigma_{\mathbf{i}}) \underline{\mathbf{E}}$$

where

$$\sigma_c = \epsilon_o \omega_p^2 \frac{v + i\omega}{v^2 + \omega^2}$$

and

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$$\sigma_{\mathbf{r}} = \epsilon_0 \frac{v \omega_{\mathbf{p}}^2}{v^2 + \omega^2}$$

$$\sigma_i = \epsilon_0 \frac{\omega_p^2 \omega}{v^2 + \omega^2}$$

where the plasma frequency $\omega_{\mathbf{p}}$ is defined by

$$\omega_{\rm p} = \sqrt{\frac{{\rm nq}^2}{{\rm m}\epsilon_{\rm o}}}$$

where m is the mass of the species considered.

B. Constitutive Parameters

The above equations thus describe the plasma as a non-polarized conducting material with a permeability $\mu_{\rm O}$, permittivity $\epsilon_{\rm O}$, and a complex conductivity $\sigma_{\rm C}$. To avoid a description of the plasma with a complex conductivity, the complex convection current is modeled with a real conduction current plus a polarization current. If an equivalent lossy dielectric is described by the real conductivity σ and the electric susceptibility $\chi_{\rm p}$, then

$$\sigma = \sigma_{\mathbf{r}}$$

$$\chi_e = -\sigma_i/\omega \epsilon_0$$

Threfore,

$$\mu = \mu_0$$

$$\epsilon = \epsilon_0 (1 + \chi_e) = \epsilon_0 (1 - \frac{\omega_p^2}{\omega_{+v}^2})$$

$$\sigma = \sigma_r = \epsilon_0 \frac{v\omega_p^2}{\omega_{+v}^2}$$

Thus, it is also possible to describe the plasma as a polarized conducting material with a permeability μ_0 , permittivity $\epsilon \neq \epsilon_0$, and a real conductivity σ . Note that ϵ is actually less than ϵ_0 .

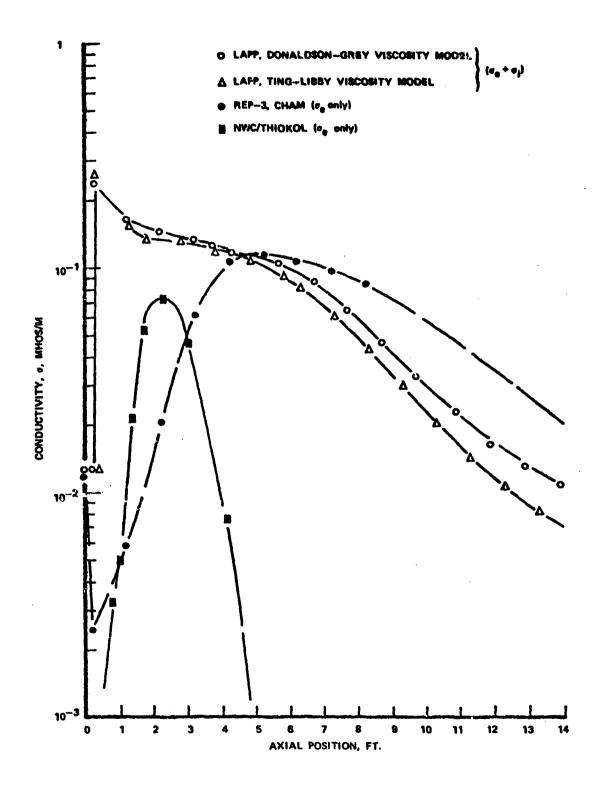


FIGURE 2. Comparison of Conductivities
Predicted by Computer Codes

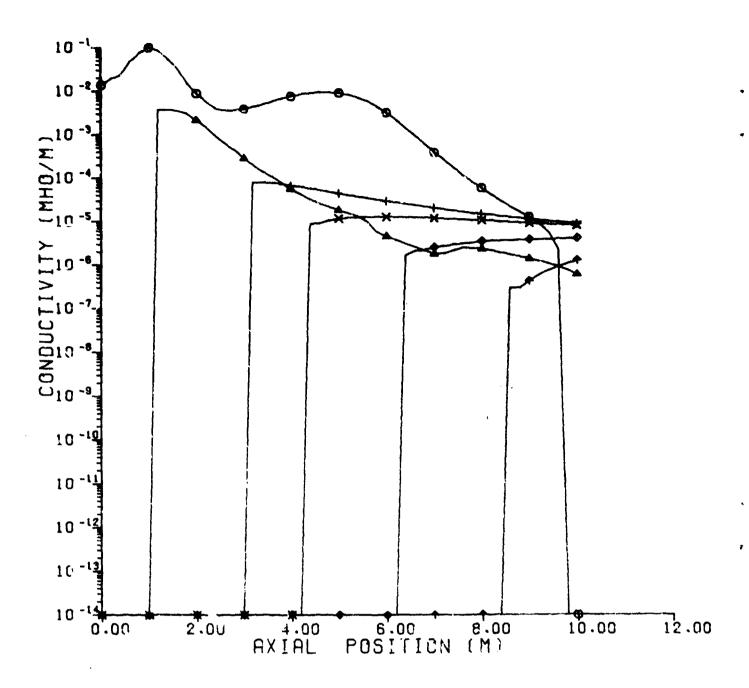
IV. PREDICTED CONSTITUTIVE PARAMETERS

The predicted maximum conductivity profiles from the LAPP (both viscosity models), REP-3, and NMC computer codes are plotted in Figure 2. Appendix B and C contain the complete axial and radial profiles of the conductivity as calculated from the LAPP computer codes from which the graphs in Figure 2 were compiled.

All of these codes gave values of the permittivity of the plume at UFH frequencies essentially the same as that of free space, $\varepsilon_{_{\rm O}}$. In Figure 2, the maximum value of the conductivity on each transverse cross-section of the plume is plotted as a function of axial position along the plume for each of the codes. A comparison of these data shows that the shapes of these curves are quite different; however, the maximum values of the conductivity predicted by the codes are nearly the same.

For the construction of the simulated plume, the highest predicted values of the conductivity should be used, since these will produce the maximum effect on the susceptibility of the rocket. This effect has been verified by the theoretical thin-wire electromagnetic model. The conductivities from the LAPP code are generally higher than those of the REP-3 code, particularly in the transition region of the plume which is close to the rocket. Therefore, the decision was made to use the conductivities predicted by the LAPP code with the Donaldson-Grey eddy-viscosity model for constructing the simulated plume.

A brief description of the LAPP code is contained in Appendix A.



RADIAI.	FOSITION (M)	ROCKET	•	REDEYE
O	0.000	POSITION	•	5000(FT)/10(FT/S)
Δ	0.500	PRESSURE	•	0.832 (ATMOSPHERES)
+	1.000			
×	1-500			
Φ	2.000			
, 1	2.500			

FIGURE 3a. Conductivity vs. Axial Position With Radial Position as a Parameter.

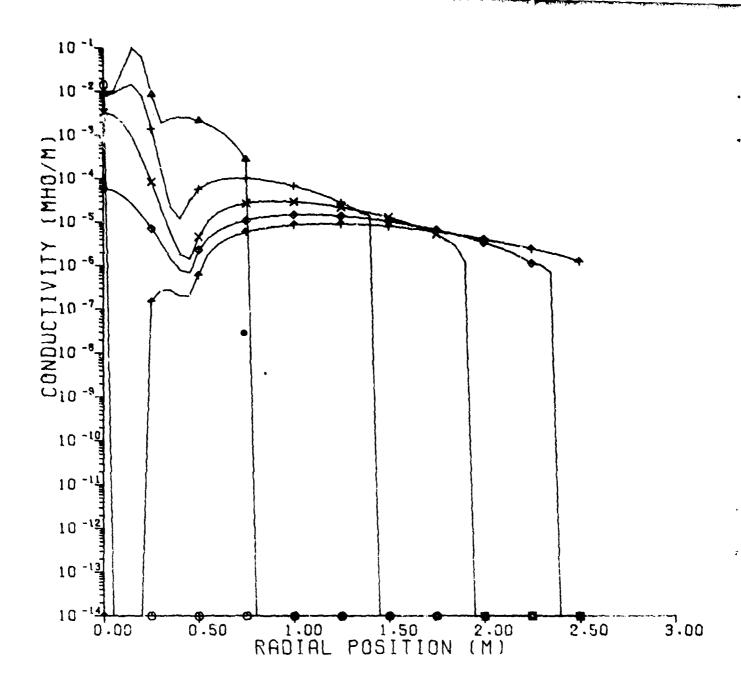
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V. PREDICTED CONDUCTIVITY PROFILES

The output of the LAPP computer code, as discussed in Appendix A, contains the electron density and electron-neutral collision frequency at all radial points for each axial print-out station. The electrical conductivity of the exhaust plume has been calculated at these same points to determine the complete axial and radial conductivity profile in the wake of the rocket.

A sample of the output for the Redeye missile is shown in Appendix B. Each succeeding page contains printouts at axial stations corresponding to the print increment. Note that the data is not equally spaced in either the axial or the radial directions. Appendix C contains the same data as in Appendix B; but for convenience, the data is presented at equidistance spaces in both the axial and radial directions.

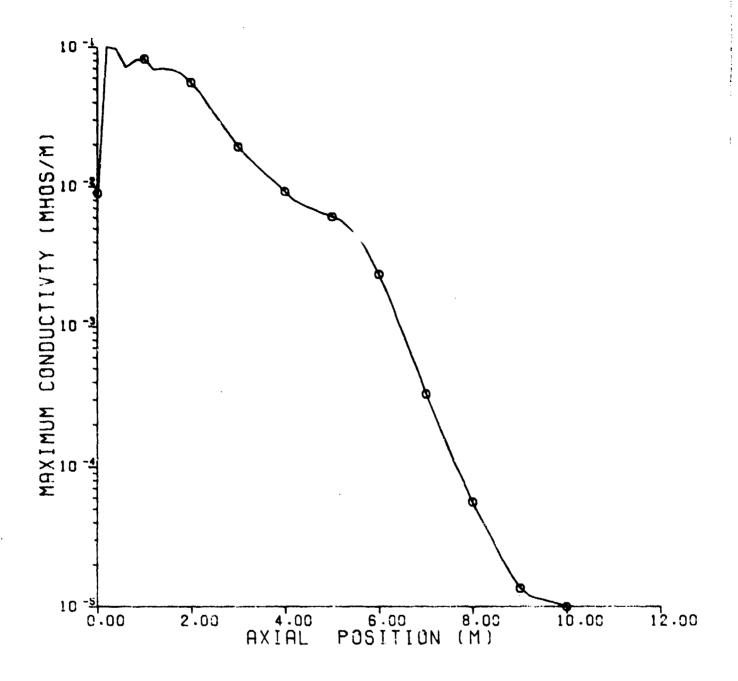
the equilized data contained in Appendix C. In Figure 3a, the conductivity is plotted as a function of axial distance behind the rocket nozzle at several radial positions; in Figure 3b, the conductivity is plotted as a function of radial distance from the center line of the rocket motor at several axial positions. In Figure 4, the maximum value of the conductivity at each cross-section is plotted as a function of axial position. Figure 5 contains a 2-dimensional equi-contour plot of this same information. In Figure 6a, a 3-dimensional relief map is shown of the conductivity profile. Figure 6b is Figure 6a rotated by 180 degrees. For clarity, the radial scale is increased by a factor of 4. Notice that in the above plots, it is the log of the conductivity that is used.



AXIAL	POSITION (M)	ROCKET - REDEYE
O	0.000	POSITION - 5000(FT)/10(FT/5)
Δ	2.000	PRESSURE - 0.832 (ATMOSPHERES)
+	4.000	
×	6.000	
Φ	8.000	
4	10.000	

FIGURE 3b. Conductivity vs. Radial Position With Axial Position as a Parameter

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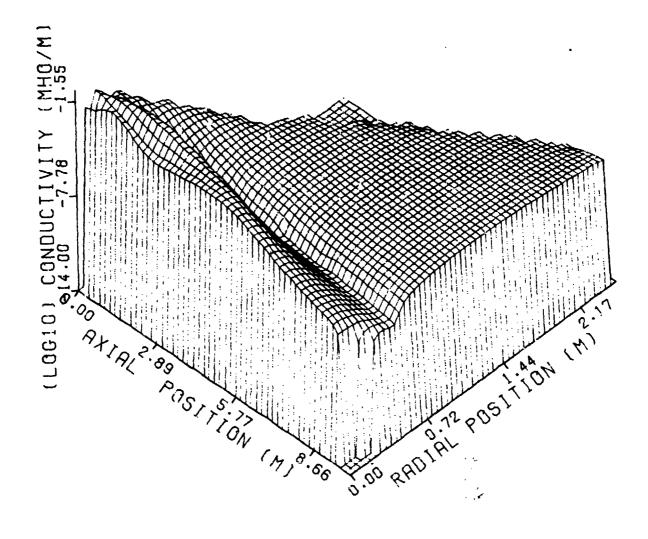
POSITION - 500G(FT)/10(FT/S)

PRESSURE - 0.832 (ATMOSPHERES)

FIGURE 4. Maximum Values of Conductivity.

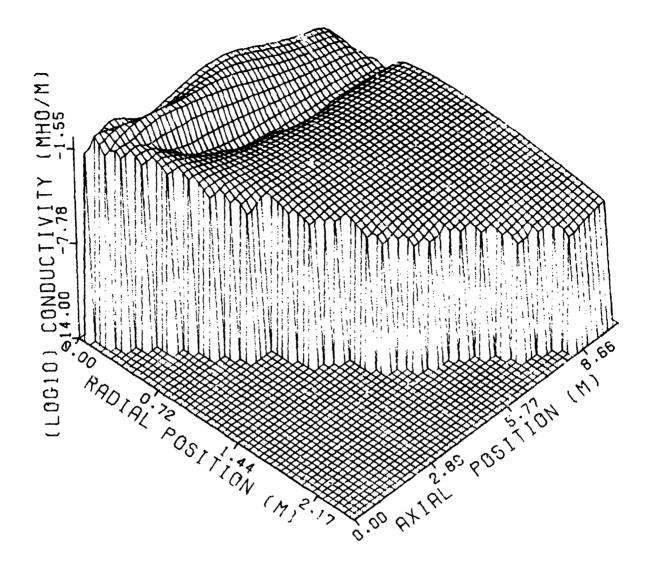
```
-12.9
                                                         E = -11.9
                                                         F = -11.4
                                                         G = -10.8
                                                         H = -10.3
                                                         I = -9.76
                                                        J = -9.23
                                                        K = -8.70
                                                         L = - 8.17
                                                        M = -7.64
                                                        N = -7.11
                                                        0 = -6.59
                                                         P = -6.06
                                                        Q = -5.53
                                         0000000
                                                        R = -5.00
                                                        S = -4.47
                                                        T = -3.94
                                                         V = -2.88
                                            RRR RR
RRRRRR
RRRRR
                                                            - 2.35
                                                        X = -1.82
CONDUCTIVITY (MHO/M)
                                                        Y = -1.29
 POSITION (M)
                                                        Z = - .759
 POSITION (H)
```

Figure 5. Equicontour Plot of Conductivity



POSITION - 5000(FT)/10(FT/S)
PRESSURE - 0.832 (ATMOSPHERES)

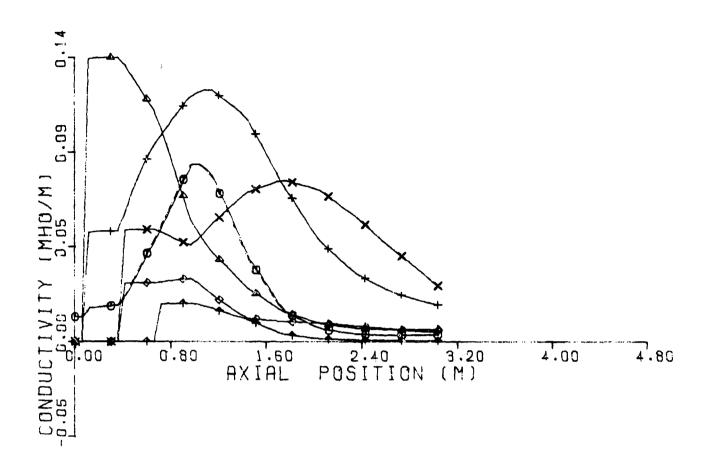
FIGURE 6a. Relief Map of Conductivity



POSITION - 5000(FT)/10(FT/S)
PRESSURE - 0.832 (ATMOSPHERES)

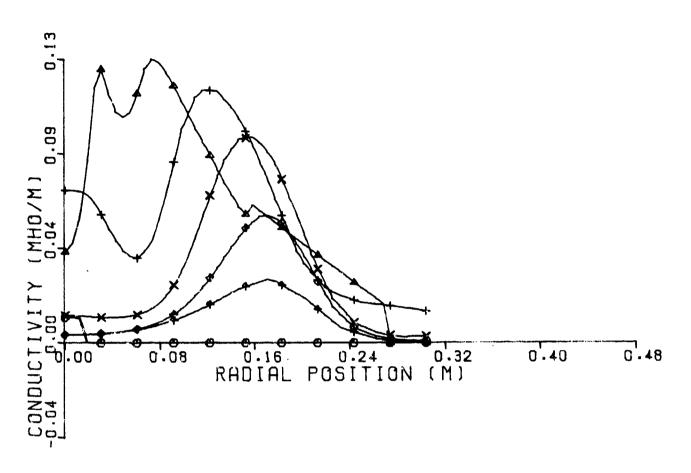
FIGURE 6b. Relief Map of Conductivity

Since the thin wire moment method codes predict that regions of the plume with values of conductivity less than approximately 1×10^{-2} mhos/meter are insignificant, the first 10 feet of the plume out to approximately 1 foot in radius contains the significant part of the plume. An enlargement of the conductivity of this portion of the plume is shown in Figure 7. Again, in Figure 7a, the conductivity is plotted as a function of axial distance behind the rocket nozzle at several radial positions; and, in Figure 7b, the conductivity is plotted as a function of radial distance from the center line of the rocket motor at several axial positions. In Figure 8, the maximum value of the conductivity at each cross-section is plotted as a function of axial position. Also, in Figure 9a, a 3-dimensional relief map of the conductivity is shown. Figure 9b is Figure 9a rotated by 180 degrees. Again, for clarity, the radial scale is increased by a factor of 6. Notice that the expanded plots are linear in the conductivity.



RADIAL	POSITION (M)	ROCKET	- REDEYE
O	0.000	POSITION	- 9000(FT) / 10(FT/SEC)
A	0.061	PRESSURE	- 0.832 (ATMOSPHERES)
+	0.122		
×	0.183		
₹.	0.244		
4	0.305		

FIGURE 7a. Conductivity vs. Axial Postion With Radial Position as a Parameter



AXIAL	FOSITION (M)	ROCKET	- RFDEYE
O	0.000	POSITION	- 5000(FT) / 10(FT/SEC)
Δ	0.610	PRESSURE	- 0.832 (ATMOSPHERES) -
+	1.219		-
×	1.829		
❖	2.438		
4	3.048		

FIGURE 7b. Conductivity vs. Radial Position With Axial Position as a Parameter

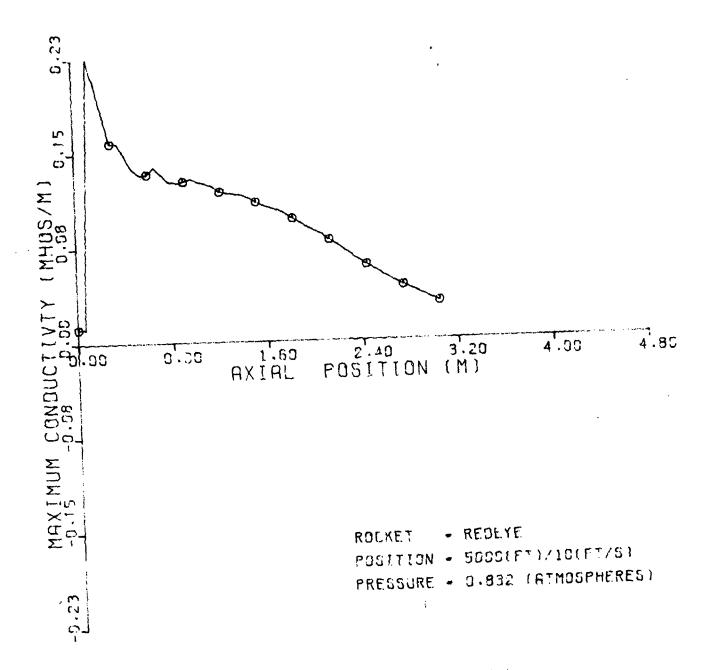
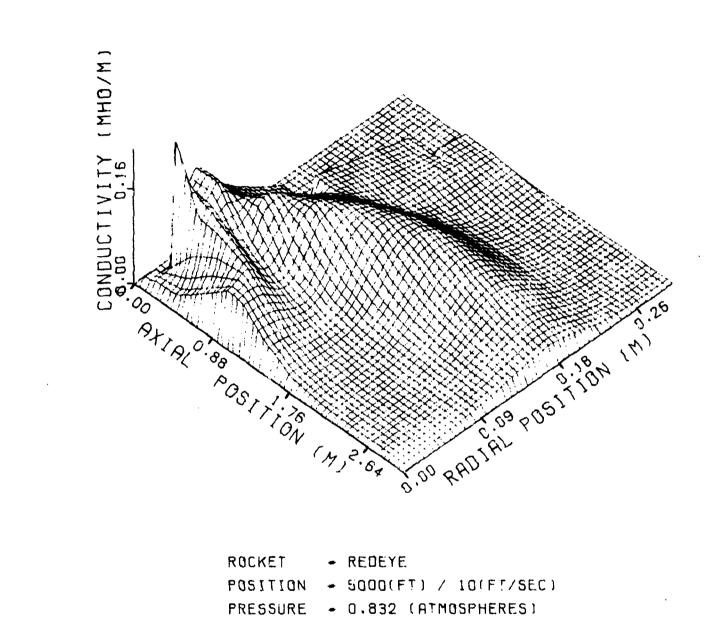
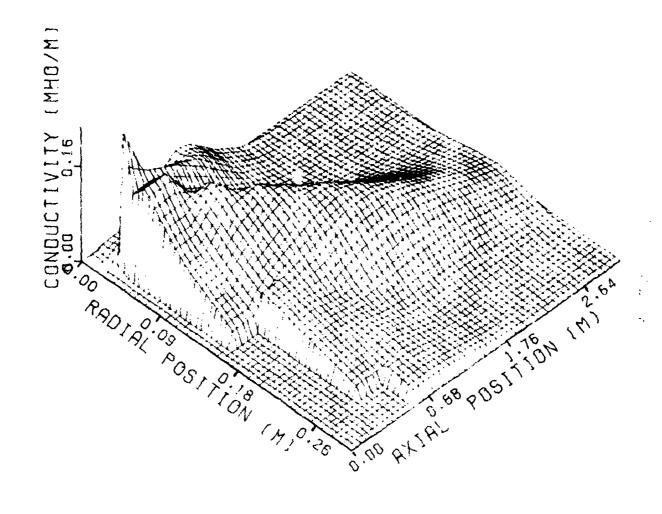


FIGURE 8. Maximum Values of Conductivity.



PRESSURE - 0.832 (ATMOSPHERES)

FIGURE 9a. Relief Map of Conductivity



POSITION - SOGG(FT) / SG(FT/SEC)
PRESSURE - 0.832 (ATMOSPHERES)

FIGURE 9b. Relief Map of Conductivity

REFERENCES

- [1] Mikatarian, Kau, and Pergament, "A Fast Computer Program for Non-Equilibrium Rocket Plume Predictions," AFRPL-TR-72-94, Air Force Rocket Propulsion Laboratory, Edwards Air Force Base.
- [2] JANNAF Thermochemical Tables (Dow Chemical Co., Midland, continuously updated).

APPENDIX A

The LAPP computer program for predicting nonequilibrium, low altitude rocket plume properties is described in this Appendix.

The analytical model assumes parallel turbulent (or laminar) mixing between concentric chemically reacting streams. The equations for tree shear layer mixing with nonequilibrium chemistry are solved via a mixed implicit/explicit finite difference scheme which efficiently predicts flow properties and composition, even when many chemical reactions are near equilibrium.

Al. " INTRODUCTION

magnetic wave/plume interactions and can be used to predict the electrical properties of a typical turbulent after-burning rocket exhaust plume. The program uses a gas dynamic model (parallel mixing between two concentric streams), and will account for nonequilibrium chemistry effects). Therefore, finite-rate chemical kinetics are incorporated into the rocket plume calculations to accurately predict plume temperatures, electrical properties, etc.

Conceptually, the numerical solution of the equations describing axisymmetric mixing with nonequilibrium chemistry presents few difficulties, except in non-equilibrium flows where one or more of the chemical reactions is at or near-equilibrium, a situation typical of relatively low altitude (< 70 kft) afterburning plumes.

Therefore, in the LAPP computer program a implicit/explicit numerical technique is used to solve the partial differential equations (in finite-difference form) describing turbulent (or laminar) shear flows with non-equilibrium chemistry, i.e., implicit differences are used in the solution of the species conservation equations and explicit differences are used for the momentum and erergy equations. This mixed implicit/explicit scheme eliminates the instability problems which might otherwise arise.

The gas dynamic model assumes parallel mixing between the rocket exhaust products and surrounding air (either quiescent or moving), and allows for non-uniform initial conditions at the nozzle exit plane.

Lewis and Prandtl numbers are assumed to be constant, and pressure is

allowed to vary parallel to the plume axis. Turbulent transport is described via an appropriate eddy viscosity model and Sutherland's law is used to calculate the viscosity for laminar flow. The program will allow any chemical reaction mechanism (and associated rate coefficients) to be used as long as thermodynamic data are available for all species. Thermodynamic data, taken directly from the JANNAF Tables, 2 are input in tabular form.

This appendix presents governing partial differential equations, their finite difference formulations, the various eddy viscosity models which may be input to the program, and a description of the input data. The computer output gives detailed axial and radial distributions of velocity, temperature, density and species mole fractions. These results are used to calculate electron and ion densities and collision frequencies with neutral particles, which, in turn, are used to determine the electrical constitutive parameters.

AII. GOVERNING BOUATIONS

A. Conservation Equations and Boundary Conditions

The following equations describe the free-shear layer turbulent or laminar mixing of co-flowing axisymmetric streams undergoing chemical reactions. For turbulent flow all properties are interpreted to be the mean (time-averaged) values.

Global Continuity

$$\frac{\partial}{\partial x} (\rho u) + \frac{1}{r} \frac{\partial}{\partial r} (\rho v r) = 0$$
 (A1)

Conservation of Species

$$\rho u \frac{\partial F_{i}}{\partial x} + \rho v \frac{\partial F_{i}}{\partial r} = \frac{1}{r} \frac{\partial}{\partial r} (\frac{Le}{Pr} \mu r \frac{\partial F_{i}}{\partial r}) + \dot{v}_{i}$$
 (A2)

Conservation of Momentum

$$\rho u \frac{\partial u}{\partial x} + \rho v \frac{\partial u}{\partial r} = -\frac{dp}{dx} + \frac{1}{r} \frac{\partial}{\partial r} (\mu r \frac{\partial u}{\partial r})$$
 (A3)

Conservation of Energy

$$\rho c_{\mathbf{p}} \left[\mathbf{u} \frac{\partial \mathbf{T}}{\partial \mathbf{x}} + \mathbf{v} \frac{\partial \mathbf{T}}{\partial \mathbf{r}} \right] = \mathbf{u} \frac{d\mathbf{p}}{d\mathbf{x}} + \mu \left(\frac{\partial \mathbf{u}}{\partial \mathbf{r}} \right)^2 + \frac{1}{r} \frac{\partial}{\partial \mathbf{r}} \left(\frac{c_{\mathbf{p}}}{\mathbf{p}\mathbf{r}} \mathbf{u} \mathbf{r} \frac{\partial \mathbf{T}}{\partial \mathbf{r}} \right) +$$

$$\mu \stackrel{\underline{Le}}{\underline{Pr}} \stackrel{\underline{\partial T}}{\underline{\partial r}} \stackrel{\underline{\Gamma}}{\underline{i}} c_{F_{\underline{i}}} \stackrel{\underline{\partial F}_{\underline{i}}}{\underline{\partial r}} - \stackrel{\underline{\Gamma}}{\underline{i}} \stackrel{\underline{\dot{w}}_{\underline{i}}}{\underline{\dot{h}}_{\underline{i}}}$$
(A4)

State

$$\rho = \frac{pW}{RT} \tag{A5}$$

c = specific heat of mixture

c = specific heat of ith species

 \mathbf{F}_{i} = defined as $\mathbf{X}_{i}/\mathbf{W} (= \mathbf{Y}_{i}/\mathbf{W}_{i})$

h, = enthalpy of ith species

Le = Lewis number (laminar or turbulent)

p = static pressure

Pr = Prandtl number (laminar or turbulent)

r = coordinate normal to jet centerline

R = universal gas constant

T = static temperature

u = x component of velocity

v = r component of velocity

w, = molar rate of production of ith species

W = molecular weight of mixture

W, = molecular weight of ith species

x = coordinate parallel to jet centerline

X, = mole fraction of ith species

Y, * mass fraction of ith species

u = viscosity (or eddy viscosity for turbulent flow)

The conservation equations are solved subject to initial and boundary conditions at the nozzle of the rocket and at the free-stream boundary:

$$x = 0: \quad u = u(r), \quad F_{i} = F_{i}(r), \quad T = T(r)$$

$$r = 0: \quad \frac{\partial u}{\partial r} = \frac{\partial T}{\partial r} = \frac{\partial F_{i}}{\partial r} = 0 \tag{A6}$$

$$r \to \infty: \quad u \to u_{e}, \quad F_{i} \to (F_{i})_{e}, \quad T \to T_{e}$$

Pressure is allowed to vary in the axial direction according to,

$$p = c_0 + c_1 x + c_2 x^2 + c_3 x^3$$
 (A7)

where c_0 , c_1 , c_2 and c_3 are input coefficients.

B. Transformation to Stream Function Coordinates

It is convenient to transform the equations into a streamline coordinate system and utilize the stream function, Ψ , as the radial coordinate. The transformation from cartesian (\mathbf{x},\mathbf{r}) coordinates to streamline (\mathbf{x},Ψ) coordinates (which automatically satisfies global continuity) is defined by:

$$\Psi \frac{\partial \Psi}{\partial \mathbf{r}} = \rho \mathbf{u} \mathbf{r} \tag{A8a}$$

$$\Psi \frac{\partial \Psi}{\partial \mathbf{x}} = -\rho \mathbf{v} \mathbf{r} \tag{A8b}$$

The governing equations, then take the form:

Species

$$\frac{\partial F_{i}}{\partial x} = \frac{1}{\Psi} \frac{\partial}{\partial \Psi} \left[\left(\frac{Le}{Pr} \right) \frac{\mu \rho u r^{2}}{\Psi} \frac{\partial F_{i}}{\partial \psi} \right] + \frac{w_{i}}{u \rho}$$
(A9a)

and, on the axis of symmetry, $r = \Psi = 0$

$$\frac{\partial \mathbf{F_i}}{\partial \mathbf{x}} = 2\mu \left(\frac{\mathbf{Le}}{\mathbf{Pr}}\right) \frac{\partial^2 \mathbf{F_i}}{\partial \psi^2} + \frac{\mathbf{w_i}}{\mathbf{up}}$$
(A9b)

Momentum

$$\frac{\partial u}{\partial x} = -\frac{1}{\rho u} \frac{dp}{dx} + \frac{1}{\Psi} \frac{\partial}{\partial \Psi} \left[\frac{\mu \rho u r^2}{\Psi} \frac{\partial u}{\partial \Psi} \right]$$
 (A10a)

and, on the axis of symmetry, $r = \Psi = 0$

$$\frac{\partial \mathbf{u}}{\partial \mathbf{x}} = -\frac{1}{\rho \mathbf{u}} \frac{\mathrm{d} \mathbf{p}}{\mathrm{d} \mathbf{x}} + 2\mu \frac{\partial^2 \mathbf{u}}{\partial \mathbf{y}^2} \tag{A10b}$$

Energy

$$c_{\mathbf{p}} \frac{\partial \mathbf{T}}{\partial \mathbf{x}} = \frac{1}{\rho} \frac{d\mathbf{p}}{d\mathbf{x}} - \frac{1}{\rho \mathbf{u}} \sum_{i} \mathbf{h}_{i} \dot{\mathbf{w}}_{i} + \frac{1}{\Psi} \frac{\partial}{\partial \Psi} \left[\frac{c_{\mathbf{p}}}{\mathbf{pr}} \frac{\mu \rho \mathbf{u} \mathbf{r}^{2}}{\Psi} \frac{\partial \mathbf{T}}{\partial \Psi} \right] + \frac{\mu \rho \mathbf{u} \mathbf{r}^{2}}{\Psi^{2}} \left[\left(\frac{\partial \mathbf{u}}{\partial \Psi} \right)^{2} + \frac{\mathbf{Le}}{\mathbf{pr}} \frac{\partial \mathbf{T}}{\partial \Psi} \sum_{i} c_{\mathbf{p}_{i}} \frac{\partial \mathbf{F}_{i}}{\partial \Psi} \right]$$
(Alla)

and, on the axis of symmetry, $r = \Psi = 0$

$$c_{\mathbf{p}} \frac{\partial \mathbf{T}}{\partial \mathbf{x}} = \frac{1}{\rho} \frac{d\mathbf{p}}{d\mathbf{x}} + 2\mu \left(\frac{c_{\mathbf{p}}}{\mathbf{p_r}}\right) \frac{\partial^2 \mathbf{T}}{\partial \psi^2} - \frac{1}{\rho \mathbf{u}} \sum_{\mathbf{i}} \mathbf{h_i \dot{w_i}}$$
 (A11b)

C. Finite-Difference Formulation

The governing set of parabolic partial differential equations, are first rewritten in finite difference form and then solved using a forward marching technique. The chemistry terms, $\mathbf{w}_{\mathbf{i}}$, in the species continuity equations are evaluated via implicit-differences; the diffusion terms in the species continuity equations and the complete energy and momentum equations are evaluated via explicit-differences.

AIII. SOLUTION OF FINITE DIFFERENCE EQUATIONS

A. Integration Step Size

Should the computed species mole fraction at any radial point become negative (typically, because the chemistry is "fast," and one or more reactions are near-equilibrium), the step size is repeatedly halved until either the species mole fraction becomes positive or the step size becomes less than some minimum step size. In the latter case, the program terminates.

The number of grid points cannot be allowed to expand without bounds because of the limited storage capacity of the computer.

Therefore, the number of points is halved either when the mesh increases to twice its original size or the number of points exceeds 26. The computer prints all output at the station at which halving occurs.

AIV. CHEMICAL REACTION RATE EQUATIONS

A maximum of 25 possible reactions are included in the programs with rate coefficients \mathbf{k}_r expressed in the form*

$$k_r = NT^{-N} \exp(B/RT)$$

For the Redeye missile the reactions listed the following table are considered.

In the reactions, M is an arbitrary third body. In this program, all species are assumed to have equal third body efficiencies.

Rate coefficient data for typical rocket plume reactions may be found in the JANNAF Thermochemical Tables. 2

			REA	CTIO	NS				A	N	В
KCL	+	н			32	ĸ	+	HCL	7.0x10 ⁻¹¹	0	-1000
0	+	0	+	M	=	02	+	M	3.8x10 ⁻³⁰	1	- 340
Н	+	н	+	M	=	H ₂	+	M	2.8x10 ⁻³⁰	1	0
0	+	н	+	M	=	OH	+	M	2.0x10 ⁻³²	0	0
н	+	ОН	+	M	C.EE	н ₂ 0	+	M	6.1x10 ⁻²⁶	2	0
со	+	0	+	M	=	co ₂	+	M	2.0x10 ⁻³³	o	-4000
ОН	+	ОН			=	н ₂ 0	÷	0	1.0×10 ⁻¹¹	-o ·	-1100
ОН	+	H ₂			=	H ₂ 0	+	Н	1.0x10 ⁻¹⁷	-2	-2900
ОН	+	H			#	H ₂	+	0	1.4x10 ⁻¹⁴	-1	-7000
ОН	+	02			=	H	+	02	4.0x10 ⁻¹¹	0	0
со	+	ОН			=	co ₂	+	Н	1.1x10 ⁻¹⁹	-2	1600
Cl	+	n ₂			=	HCL	+	н	8.0x10 ⁻¹¹	0	-5260
HCl	+	ОН			=	H ₂ 0	+	CL	1.0×10 ⁻¹⁴	-1	-1900
0	+	HCL			=	ОН	+	CL	2,0x10 ⁻¹²	0	-4500
Н	+	Cl	+	M	=	HCL	+	M	3.0x10 ⁻³⁰	1	0
ĸ	+	Cl	+	M	=	KCL	+	M	1.0x10 ⁻²⁹	1	0
NaCL	+	н			=	Na	+	нся	8.0x10 ⁻¹¹	0	- 800
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Cl	+	e _	+	M	=	Cl-	/+	M	6.0x10 ⁻²⁹	ì	0
cl ⁻	+	н			=	HCL	*	e -	9.6x10 ⁻¹⁰	0	0
Na ⁺	+	e¯	+	M	=	Na	+	M	2.0x10 ⁻²⁰	2	0
Na ^{†.}	+	Cl-			■:	Na	+	Cl	8.0x10 ⁻¹⁰	0	0
Na ⁺	+	ĸ			=	Na	+	K +	1.0x10 ⁻⁹	0	0

AND THE RESERVE OF THE PROPERTY OF THE PROPERT

AV. TRANSPORT PROPERTIES

A. Turbulent Eddy Viscosity Models

The following eddy viscosity models are incorporated into the program.

(Ting/Libby)

Initial region,

$$\mu = \rho \epsilon = 0.00137 \times \left| \mathbf{u}_{j} - \mathbf{u}_{e} \right| \rho \left(\frac{\rho_{j}}{\rho} \right)$$
 (A12)

Developed region,

$$\mu = \rho \epsilon = K \overline{r_1} | u_0 - u_e | \rho (\frac{\rho_0}{\rho})^2 (\frac{\eta}{r})^2$$
(A13)

where

$$n = \sqrt{2 \int_0^r (\rho_0/\rho) r' dr'}$$

(Donaldson/Gray)

Initial region

$$\mu = \rho \epsilon = \overline{K}(r_{\underline{1}} - r_{\underline{i}})\rho |u_{\underline{0}} - u_{\underline{e}}|/2$$
 (A14)

Developed region,

$$\mu = \rho \epsilon = \overline{K} r_{1} \rho | u_{0} - u_{e} | /2$$
 (A15)

where

 $\rho = density$

 ϵ = eddy diffusivity for turbulent flow

K = eddy viscosity coefficient (for Ting/Libby model)

K = eddy viscosity coefficient (for Donaldson/Gray model)

Specifically,

K = 0.025

and

$$\overline{K} = 0.0468 + M_{\frac{1}{2}}[-0.0460 M_{\frac{1}{2}} + 0.0256 M_{\frac{1}{2}}^{2}] \qquad (M_{\frac{1}{2}} \le 1.2)$$

where M_1 is the value of the Mach number at the half radius r_1 (i.e., at the value of r where $u = (u_0 + u_1)/2$).

 $r_{\frac{1}{2}}$ is the value of η where $u=(u_0+u_e)/2$. r_i is the inner mixing zone radius and is defined as the value of r where $(u_0-u_e)/(u_1-u_e)=0.75$.

In the above equations

 u_0 = velocity at the axis of symmetry, r=0

 \mathbf{u}_{e} = velocity at the edge of the mixing layer (free stream)

 u_i = velocity at the nozzle (jet) exit plane

and

 r_{i} = radius at the nozzle (jet) exit plane

and

 ρ_{O} = density at the axis of symmetry, r=0

 ρ_{j} = density at the nozzle (jet) exit plane.

B. Laminar Flow

Sutherland's Law is used to describe the viscosity as a function

of temperature.

$$\mu = 9.8 \times 10^{-7} \text{T}^{3/2} / (\text{T} + 111)$$
 (A17)

AVI. PLUME ELECTRICAL PROPERTIES

Electron density and electron-neutral collision frequency are computed at all radial points for each axial print-out station.

A. <u>Electron Density</u>

$$n_e = 0.733(10^{22}) x_e pT^{-1}$$
 ml⁻¹ (A18)

where p is in atm and T in degrees K.

B. Collision Frequency

$$v_e = 4.57(10^{27}) p_{\tau}^{-\frac{1}{2}} \sum_{i} x_{i} Q_{e_i} \quad \text{sec}^{-1}$$
 (A19)

where p is in atm, T in degrees K and Q_{e_i} in cm². The electron-neutral collision cross-sections used in the calculations and given in the following table are those which characterize typical solid propellant exhaust plumes. Similar expressions are used to calculate the densities and collision frequencies for the ions considered.

	Ω _e (cm ²)
SPECIES	
со	2.08 $(10^{-23})v_e^{\dagger} + 2.46(10^{-16})$
co ₂	$4.7(10^{-8})v_e^{-1}$
.н ₂ о	5.9v _e ⁻²
HC1	1.85v _e ⁻²
N ₂	3.29(10 ⁻²³)v _e
H ₂	$1.45(10^{-23})v_e + 8.9(10^{-16})$

 $v_e = 6.21(10^5)T^{\frac{1}{2}}$ cm/sec

AVII. THERMODYNAMIC DATA

The thermodynamic properties (specific heat, Gibbs free energy and enthalpy) for each species are taken directly from the JANNAF Thermochemical Tables, and input to the program in tabular form as a function of temperature. Linear interpolation is used to define thermodynamic properties at the local temperature.

APPENDIX B

LAPP computer code output for the Redeye Missile (unequally-spaced data).

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	31	#	1.20				_	-		.81E-12#
	32		1.24	• • 12	#	1.105+17+	2.53E+11#	2.975+09#	1.226-02* 6	8.81E-12#
	3 5	4	1.26	• •02	#	1.106+17*	2.53E+11#	2.37E+09#	1.226-02* 6	1. 41E-124
•	34	#	1.32	• • • • •	#	1.136 +174	2.53E+11#	2.376+03#	1.22F-02* 9	. 81E-12#
	15	ø	1.36							. 51E-12¢
	36	4	1.40							. 51E-12#
	37		1.44	• • • • • •	#					11E-12#
	3.4		- - ·	+ .02					1.22E-02* 5	
ő	33			* .03			1.092+11#	C		.55E-12#
= =		- 			: :				*******	

(MAZIMUM CONDUCTIVITY + 1.828-02 (MHOS/M)

	POINT 3 •10 (4)		E-02	#FOCKET #POSITION #PPESSURE	# REDEYE # 5000(FT)/ # 0.032 (AT			**
	PATOAR XBUNI				*COL: ISION# *FREQUENCY# * (1/S) #			
	**************************************	######################################	G.00 .00 .00 .00 .00 .01 .01 .01 .01 .01	# 1.46E+17 # 1.46E+17 # 1.46E+17 # 1.46E+17 # 1.46E+17 # 1.46E+17 # 1.46F+17 # 1.46E+17	7* 2.53E + 11#	3.43E+09#	1.63E-02* 3.79E-1 1.63E-02* 3.79E-1 1.63E-02* 8.79E-1 1.63E-02* 8.79E-1	
*****	16 17 19 19 20 21 22	# 1.20 # # 1.20 # # 1.36 # # 1.56 # # 1.76 # # 2.40 #	.02 .02 .02 .02 .03	# 1.46E+17 # 1.47E+17 # 1.74E+17 # 5.44E+17 # 2.88E+18 # 2.3cE+18	7* 2.53E+11# 7* 2.53E+11# 7* 2.53E+11# 7* 2.63E+11# 3* 3.39E+11#	3.43E+09# 3.44E+09# 3.75E+09# 6.62E+09# 1.52E+10# 1.38E+10#	1.63E-02* 8.79E-1 1.64E-02* 8.79E-1 1.94E-02* 8.78E-1 5.82E-02* 8.63E-1 24 * 8.15E-1 1.23 * 8.06E-1	2# 2# 2# 2# 2#

MAXIMUM CONDUCTIVITY: .24 (MHOS/P)

#F(:2=== :INT 4 .30 (M)		ZZLE 1.48 (M		# 6	OCK OSI	Tic	ON I	5		FT)	_	111111 0 (FT/S 052HER			E+08 #
	RADIAL		TIVE*	AESCLUTY RACIUS (M)		DEN	SIT		FR		NCY		PLASM REQUEN (1/S)	CY#		EPSILON # (FO/M) #
************	==== 1234567490 11123 145	· · · · · · · · · · · · · · · · · · ·	100 + + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100 + 100	0.00 .00 .00 .00 .01 .01 .01 .02 .02 .03 .03	***	1	7E 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	174 1174 1174 1174 1174 1174 1174 1184 118	=== 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	• 526 • 516 • 516 • 516 • 506 • 506 • 506	+11 +11 +11 +11 +11 +11 +11 +11 +11 +11	***	******* 3.59E+ 3.64E+ 3.78E+	 09# 09# 09# 09# 09# 10# 10# 10#	1.79E-02+ 1.84E-02+ 1.99E-02+ 2.27E-02+ 3.41E-02+ 4.47E-02+ 4.47E-02+ 4.16E-02+ 1.15 1.15 1.14 1.16	# # # # # # # # # # # # # # # # # # #
* * * * * * * * * * * * * * * * * * * *	16 17 18 19 20 21 22	# 4. # 5. # 6.	25 * 60 * 60 * 42 * 41 * 466 * 42 * 4	.06 .97 .04 .09 .11 .13	#	1.0 8.2 6.1 4.3 2.6	6E -	+174	2 2 2 4 1	.386 .136 .866	+11 +11 +11 +11	# # # #	1.03E+ 9.24E+ 8.16E+ 7.06E+ 5.92E+ 4.63E+ 2.87E+	100 100 100 100 100 100 100 100 100 100	* .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12 * .12	5.41E-12# 6.44E-12# 8.47E-12# 3.50E-12# 8.56E-12#

MAXIMUM CONDUCTIVITY : .16 (NHOS/F)

=	======	=======================================	********	********		========		*******
•	FOINT 5				REDEYE		FREGUE	NCY #
	•69	1.40		#POSITION #			2.508	+06 #
#	(H)	# (M	•	#FRESSURE +	G.832 (AT	MOSPHERES	(47	()
Ξ				*********	* = * = * = * = * = *	========	********	=========
#				# ELECTRON*			SIGMA +	EPSILON #
•	XACNI	RACIUS *		# SENSITY *		FREQUENCY#	*	#
		•	(M)	# (1/M3) *	(1/5) #	(1/5) #	(MHQ/M) *	(FO/M) #
=	*****						*========	********
	1	• 0.00 +		# 4.53E+17+				
	_	.19 *		# 4.61E+17#				
	3	.38 *		# 4.85E+17*				•
	4	.58 *			2.49E+11#			
	5	.78 +		# 5.95E+174				
	6 7	# .99 * # 1.21 *		# 6.69E+17*				
	•			# M.14E+17*			9.13E-02+	8.49E-12#
	6 9	# 1.44 * # 1.69 *			2.53E+11#			8.43E-12#
	10	/ 1.69 * / 1.96 *		# 1.09E+18* # 1.15E+18*	2.57E+11#	9.39E+09#		8.38E=12#
-	11	* 2.26 *		# 1.11E+18*		9.446+09#		8.36E-12# 8.39E-12#
- 4	12	2.58		# 9.31E+17*		8.94E+09#		8.44E-12#
-	13	2.92		# 8.845+17*				
-	14	# 3.30 *			2.67E+11#			8.525-12#
ä	15	# 3.70 *		# F. 98E+17+				9.51E-12#
	16	# 4.12 *		# 1.0 dE+18*		9.33E+09#		3.45E-12#
	17	4.57 *			2.75E+11#			8.37E-12#
ě	18	# 5.05 *		# 1.39E+18+		1.068+10#		8.33E-12#
	19	# 5.54 ¥		# 1.37F+18*	_	1.056+10#		8.345-12#
	20	# 6.07 #		# 1.28E+18*		1.01E+10#		8.36E-12#
	21	# 6.62 *		# 1.16E+18*		9.68E+09#		8.38E=12#
	2.2	# 7.20 ¥	•11	# 1.04E+18*	2.56E+11#	9.17E+09#	•11 *	8.41E-12#
	23	# 7.81 *	•12	# 9.20F+17*	2.48E+11#	3.61E+09#	•10 *	8.43E-12#
#	24	# 3.47 #	•12	# 7.94E+17#	2.39E+11#	8.00E+09#	9.36E-02*	8.46E-12#
	25	# 9 .1 7 *	.14	# 6.67E+17*	2.29E+11#	7.33E+09#	4.22E-024	8.49E-12#
	26	# 9.92 *	•15	# 5.510+17+	2.17E+11#	6.66E+09#	7.14E-02*	9.535-12#
	27	# 10.74 #	•15	# 4.77E+17*	2.05E+11#	6.206+33#	6.55E-02*	9.54E-12#
#	29	# 11.63 *	.17	# 4.07E+17*	1.93E+11#	5.73E+09#	5.95E-02*	8.556-12#
#	29	* 12.62 *	•19	# 3.59E+17#	1.3JE+11#	5.23F+09#		8.56E-12#
#	30	# 13.73 +	• • •	* 2.73E+17*		4.69E+09#		A.58E-12#
#	31	# 14.99 *		# 2.0 af. +17+	1.54E+11#	4.10E+09#	3.82E-02*	8.61E-12#
#	32	# 16.4E #		# 1.44E+17#			2.90E-02#	3.65E-12#
F	33	# 18.27 ¥	• 27	# 7.05E+16*	1.26E+11#	2.525+09#	1.76E-02*	8.71E-12#
₹	======	==========		=======================================	========		# # = = = = = = = = :	========

MAXIMUM CURCUCTEVITY: .14 (MHOS/M)

######################################			***************
#POINT 6#	HOZZLE RACIUS	#FOCKET # REDEVE #	FPEGUENCY #
* 65. *	1.486-02	*POSITION * 5003(FT)/10(FT/S) *	2.50E+05 #
# (M) #	(M)	#PRESSURE : 0.832 (ATMOSPHERES)	(42) #
2222222	**************		31222222222222
# RADIAL#	RELATIVE* ABSCLUT	EF ELECTRON*COLLISION# PLASMA #	SIGMA # EPSILON #
# INDEX #		# DENSITY *FREQUENCY#FREQUENCY#	*
	+ (4)		(HHO/H) + (FD/H) #
*******	***************	************************	
# 1 #	3.00 * 0.00	# 7.81E+17# 2.50E+11# 7.94E+09#	8.82E-02+ 8.50E-12#
# 2 #	.23 * .00	# 7.46E+17# 2.50E+11# 7.96E+09#	
# 3 #	.46 * .01	# 8.00E+17+ 2.50E+11# 8.03E+09#	
# 4 #	.65 * .01	# A.21E+17* 2.5CE+11# 8.13E+09#	
. 5 #	.93 * .01	# 8.46E+17# 2.50E+11# 8.26E+09#	
6 6	1.19 * .02	# 8.69E+17# 2.51E+11# 3.37E+09#	
6 7 4	1.43 * .02	# 8.31E+17* 2.51E+11# 6.45E+03#	
# 3 #	1.69 * .02	# 8.71E+17* 2.52E+11# d.38E+09#	
# 3 #	1.97 * .03		9.31E-02* 8.48E-12#
# 10 #	2.26 * .03	# 7.70E+17* 2.53E+11# 7.38E+03#	
# 11 #	2.57 * .04	# 6.35E+17* 2.53E+11# 7.496+09#	
# 12 #	2.89 * .04	# 6.21E+17* 2.55E+11# 7.07E+09#	
# 15 #	3.23 * .05	# 5.59E+17# 2.56E+11# 6.71E+09#	
# 14 #	3.58 * .05	# 5.22E+17# 2.58E+11# 6.46E+09#	
# 15 #	3.96 * .06	# 5.14E+17# 2.61E+11# 6.44E+09#	
# 16 #	4.35 * .05	# 5.43E+17* 2.63E+11# 6.65E+09#	
# 17 #	4.75 * .07	# 6.38E+17* 2.65E+11# 7.17E+09#	
# 13 #	5.17 * .0 *	# 7.93E+17+ 2.67E+11# 7.39E+09#	
# 19 #	5.61 * .08	# 9.84E+17* 2.68E+11# 8.91E+09#	.10 + 8.47E-12#
# 20 #	6.07 * .09	# 1.14E+18* 2.68E+11# 9.61E+09#	.12 * 3.41E-12#
# 21 #	6.54 * .10	# 1.23F+18* 2.68E+11# 3.97E+09#	.13 # 8.375-12#
# 22 #	7.02 * .10	# 1.24E+18* 2.66E+11# 1.00E+10#	.13 * d.36E-12#
# 23 #	7.53 * .11	# 1.21E+18# 2.64E+11# 9.85E+09#	.13 * 3.37E-12#
# 24 #	8.05 * .12	# 1.14E+15* 2.61E+11# 9.59E+09#	.12 + 3.39E-12#
# 25 #	8.59 * .13	# 1.06E+16* 2.57E+11# 9.24E+09#	.12 # 8.405-12#
# 26 #	9.16 * .14	# 9.67E+17* 2.53E+11# 8.33E+03#	.11 * 8.43E-12#
# 27 #	3.75 * .14	# 8.62E+17# 2.47E+11# 9.34E+09#	9.82E-92* 3.46E-12#
# 28 #	10.36 * .15	# 7.44E+17# 2.41E+11# 7.75E+09#	1.69E-02* 8.49E-12#
# 29 #	11.00 * .16	# 6.15F+17* 2.35E+11# 7.04E+09#	7.38E-02* 8.54E-12#
# 30 #	11.56 * .17	# 4.32E+17* 2.27E+11# 6.23E+03#	5.97F-02* 3.59E-12#
# 31 #	12.40 + .18	# 3.64E+17* 2.20E+11# 5.41E+09#	4.66E-02* 8.64E-12#
# 32 #	13.15 * .19	# 2.31E+17+ 2.11E+11# 4.76E+09#	3.74E-02* 8.68E-12#
# 35 #	13.36 + .21	# 2.53E+17* 2.03E+11# 4.57E+09#	3.60E-02* 3.68E-12#
# 34 #	14.92 + .22	# 2.37E+17+ 1.94E+11# 4.37E+09#	3.45E-02+ 9.58E-12#
# 35 #	15.76 * ,23	# 2-135+17* 1-846+11# 4-146+09#	J. 26E-02* 8.68E-12#
# 35 #	16.77 * .25	# 1.37E+17# 1.74E+11# 3.88E+89#	3.02E-02+ 8.63E-12#
# 37 #	17.89 + .26	# 1.586+17# 1.646+11# 3.576+09#	2.725-02+ 8.695-12#
# 3 4 #	13.14 * .28	# 1.27E+17# 1.55E+11# 3.20E+09#	2.55E-02* 3.70E-12#
# 59 #	20.57 * .30	# 9.42F+16+ 1.42E+11# 2.76E+03#	1.88F-32* 6.72F-12#
# 43 #	22.28 * .33	# 5.37E+16* 1.30E+11# 2.13E+03#	1.30E-02* 4.75E-12#
# 41 #	24.40 * .55	# 2.69E+16+ 1.13E+11# 1.47E+09#	6.42E-03* 3.50E-12#

MAXIMUM CUNCUCTIVITY : .13 (MHOSZE)

z =	===	= 7 =	=:	=======	= = :	:::::::::::	===	==:	: 2 :	===	= =:	3 2 3	= 22:		===	==	===	===	*********	*******
#6	CIN	7 7	#	NCZZLI	E i	RACILS	# :	0.04	EI	7		×1	E DE1	Æ					# FREGUE	NCY #
#	1.	14	#	1.0	438	E-32	# 5	051	17.	CN	٤	5	000	(FT	/1	0 (FT/	'S)	# 2.50E	+03 #
₽	(M)	#		(M))	# F	?F:	St	JRF	3	Û.	. 932	: (/	1TM	105	PHE	FES	# (H2	2) #
= =	===	I I I	# :	*******	= = :	*******	===	===		32	6 3 :	3 = 3	2 ¥ 2:	. = = :	* * =	==	===	:		22222222
#	PAD	IAL	#	RELATIVE	E#	ABSCLUTE	_								•			MA		EPSILON #
	IND	EX	#	RACIUS	*	RACIUS	#	CEN	151	117	*	F٦١	E QUE	101	/#F	RE	JUE	NCY		#
#			#		*	(M)	#	(1	. /1	13)	•		(1/9	;)	#	(1/5	.)	# (MNOHM) #	(FD/M) #
2 2	===	z = =	Ξ.	2======	==:		= = =	===	: 2 :	222	* = :	= = :	¥ # #:	===	122	==	= = =	===	*********	********
		1	#	0.00	*	0.00				_	•	_		+11				+03		8.52E-12#
		2	#	•50	#	•01				_	•	_		+1				+09		5.52E-12#
#		4	#	1.01	#	.01	#			_		_		+11	_	-		+09		8.52E-12#
		4	#	1.54	*	•35	#					_		+1	_			+09		4.54E-12#
		5	#	2.11	*	•03	#					-		+1:	-			+09		8.58E-12#
		5	#	2.72	•	• 0 4		5.1		_		_		+11	-			+03		3.62E-12#
#		7	#	3.39	*	.05				_		-		+11	-			+09		8.67E-12#
		#	#	4-11		•05	#					_		+1				+09		8.68E-12#
#		4	#	4.59		.07	#			-		_		+11				+09		8.655-12#
*	1		*	5.72	*	•08			_	_		_		+1:	_			+03		8.56E-12#
#	1	-	*	5.61	-	.10	#			_	-	_		+1	_			+04		8.43E-12#
	1		*	7.55	•	•11			-	_	-	_		+1:	_			+69		8.37E-12#
	1		#	8.56	*	•13	#			_	-			+11	-			+09		8.38E-12#
	1	•	#	3.63	•	•14	*			_	•	_		+1:		•		+03		8.42E-12#
#	1		#	10.79	•	•16				_		_		+11	-			+13		8.49E-12#
	1		77	12.04	•	•18						_		+11	-			+04		8.59E-12#
	1		#	13.41	•	•50		2.5				_		+11	-			+03		5.69E-12#
	1		#	14.93	-	•22		1.		_		_		+11	_			+03		3.73E-12#
7	1		#	16.65	•	.25	#			_		_		+11	_			+03		8.73F-12#
#	2		#	10.65	•	•28	#			-		_		+1				+83		8.74E-12#
#	2.		#	21.07	-	•31	F	-		_				+1	_		-	+09		3.75E-12#
7	2	د 	# 	24.34	.	.36		3.5	1:	+11	- -	1 .	• 2 bt	+11	. # 	1.	りょと	+04	4 7.63E-03 +	8.79E-12#

MAXIMUM CONCUCTIVITY # .13 (MHOSZM)

The first of the second of the

2		=		= = :	=======	==	===	= #	===	==	==	== =	223	:==	==:	== =	===	==	# # # # # # # # # # # # # # # # # # #	====	======	
	FCINT F	#	NOZZL	E i	RACILS	# =	OCK	ET		2	ŖΕ	DEY	£					#	F	REQU	ENCY	
	1.44	#	1.	4 3	E•ù2	# F	OSI	TI	ON		5 Q	00(FTI	/1		FT/	S)	#		2.50	E+08	
	(M)	#		(M)	#F	RES	su	RE		0.	8 32	(A	\TH	US	PHE	FES	ŧ		(H	Z)	#
2	=======	=	======	# # #	*******	==	===	= =	= = =	= =	==	==4	Z = =	= =	==	3	===	==	2 = 2 = 2	====	======	2222
#			RELATIV			-		-		_							MA		SIGM	A #	EPSIL	3 AC
#	INDEX	#	PACILS	#	RACIUS	Ç								#F						#		
		#		*	(4)	#	(1	/M	3)	*	(1/5		#	(1/5	;)	#	(MHO/	4) +	(FD/	M) #
3	*****	2	222222	# #	=======================================	# # # 	===	==	===	= =	==	# 22	223	==	==:	===	===	= =	*****		*****	2222
	1		0.00	•	0.60		3.6		-								+09				8.68F	
#	2		•57		.01		3.5							_	-	_	+09		4.10E			
	3	#	1.16	•	.02		3.3	-					+11	_			+09		3.87E		3.69E	
	4	#	1.76		.33	4	3.0						+11				+09		3.51E			
	5 6	#	2.3A 3.04	*	.04 .04	*	2.7						+11	-	• -		+09		3.12E			
	7	#	3.72	_	.05	#	2.3		_				+1:				+09		2.59E		-	
	á	*	4.45	*	•07	*	2.4		-				+1:	-			+09		2.69E			
-	9	*	5.22	-	.08	-	3.0						+1	-			+03		3.26E			
7	10	-	5.02	*	.09	-	4.4						+11				+09		4.78E			
	11	-	6.96	٠	.10	-	6.9	-				-	+1	_	_		+09		7.43E			
-	12	*	7.75		.11	#	9.5		_				+1	_			+09		•10			
-	13		5.58	#	.13	ā	1.4						+1	_			+04		•12	4	8.41E	
-	14		9.66	*	.14	4	1.0	_	_				+1	-			+09		.12			
	15		10.69	#	.16		9.4						+1	_			+09		.10	#		
	15	*	11.79	*	.17		7.5	-	_				+11	_	7.	50 E	+09	#	8.60E	-02#	8.51E	-12#
	17	#	12.96	#	.19	#	5.0	7€	+17	74	2.	39E	+1	. #	6.	198	+09		5.97E			-12#
	19	#	14.21		.21	Ġ.	2.7	11	+17	7 =	2.	30E	+1	1#	4.	68E	+03	#	3.32E	-02*	9.71E	-12#
#	19	#	15.56	#	.23	#	1.2	4E	+17	7 *	2.	1 9E	+1:	L#	3.	17E	+04	#	1.60E	-02*	5.75E	-12#
	5.0	#	17.03	#	.25	#	6.4	3E	+16	5#	2.	û eE	+1	L#	2.	28E	+09	#	8.71E	-03*	3.81E	-12#
	21	#	16.64	#	.27	#	7.0	9E	+16	5 *	1.	96E	+1:	1#	2.	396	+03	#	1.02E	-02+	8.50E	-12#
#	52	#	20.42	*	.30	#	7.1	٥E	+15	بەر	1.	8 3E	+1:	L#	2.	39F	+09		1.09E			
#	2.3	#	22.41	*	• 33	#	6.4	3E	+16								+09	-	1.075			
#	24	#	24.66	#	•36	#	5.3										+09		9.56E	-	-	_
	25	#	27.26	#	.46	#			-				+1:				+09		7.89E			
	26	#	30.31	#	.45	#		-	_		-		+1:			_	+03		5. EOE			
#	27	#	34.01	*	•5 C	#	1.4	11	+16	, 	1.	215	+11	L#	1.	07E	+09	#	3.28E	-03*	9.83E	-12#

MAXIMUM CONCUCTIVITY : .12 (MHUSZF)

# :	****	==:		:===	1222	======	==:	===	===:	2 2 2 2	====	====	===	*******		******
#1	POINT	91	NO.	ZZL	E F.	ACIUS		OCK		-	RED			•	FREGUI	
	1.7	5 1	1	1.	495	-02								0(FT/S) (
#	(H)	- 4	ł		(H)		# 5	DES	SUFE		0 . 8	32 (ATM	OSPHEPES) (H)	Z) #
= :		= = :	====	===	222	#######	# = :	2525	===;	===:	= = = =	2222	###	********	::::::::::::::::::::::::::::::::::::::	
	PATT	ALI			_	ABSCLUT			_					FLASHA (EPSILJN #
•			PA!	TUS	*		#				,		Y#F	REQUENCY		# #
		ŧ				(K)	- 4	(1	/M3		(1.	/S)		(1/5)	# (MHG/M) *	(FD/M) #
= :		28:	:::::::::		===:	0 00	==:			= = = : . 7=	2228	#### ####	= = = 4 =		# 1.51E-02*	8 70F-124
•	1	•		30		0.00									# 1.49F-02*	
	2	1		.64	*	.01 .02	#								# 1.49E-02*	8.79E-12#
7	3		_	28	*	.03	7	-	9E+:	_	_				1.39E-02+	
	5		_	61	*	.04	-		EE+	-	-				# 1.35E-02*	
-	9		_	31	*	•05	7		7E+	_			_		1.35E-02*	8.50E-12#
-	7	,	_	15	*	.06							-		1.44E-02+	
7	9	1		76	*	.07			8F+						# 1.66E-02+	5.79E-12#
ä	9	ì		53	*	.08	ä		SE+:						# 2.16E-02*	3.77E-12#
-	10	i		.33		.09		2.8	HE+	17*		7E +1	_		# 3.16E-02#	3.735-12#
	11			16	#	.11		4.4	AE+	17*	2.5	9E +1	1#	6.01E+09	# 4.88E-02#	8.67E-12#
	12			02	*	.12	#	6.5	eE+	17*					# 7.14E-32+	8.58E-12#
	13	-	4	.42	*	.13	#	8.4	9E+	17*	2.6	ũĒ + 1	1#	3.272+09	# 3.21F-02*	8.50E-12#
	14	1	9.	85	*	•15	#	9.4	5E'+:	17*	2.5	5E > 1	1#	3.73E+09	# .10 *	8.45E-12#
	15	1	10	• 13	*	.16	#	9.3	168.+	17*	2.5	5E +1	1#	8.64E+09	# •10 *	8.45E-12#
#	16		11	. ძ5	*	.17	#	3.0	2E+					8.04E+09		
#	17	+	12	.93	*	•19	#	5•)4E+:	17*					# 6.80E-U2+	3.58E-12#
#	18	4	14	.06	#	.21	#		7E+		-		-		# 4.19E-32*	8.68E-12#
	19	+	15	•27	#	•23	#		4E+		2.3		_	1.75E+04	· · · · · · · · · · · · · · · · · · ·	3.76E-12#
	23			.54	*	.24			; ≒ <u> </u>	_			_	2.47E+09		8.815-12#
#	21		_	. 91	*	•26	#		+7E+			6E + 1	_			8.95E-12#
	2.2		_	.37	*	•29	#		JF+					1.30E+09		8.942-12#
#	23			. 45	*	. 31			5£ +			5E + 1		1.45E+09		8.43E-12#
#	24			.57	*	.33			14F +			6E + 1	_		# 4.31E-J3*	8.83E-12#
	25			•55	*	• 36			776+	_		5E + 1			# 4.47E-33* # 4.33E-03*	8.93E-12#
	26			.63	•	.39	# #		53E+					1.45E+09		3.83F-12#
	27		_	.94	*	.43	#		198+ 178+			4E +1	_		# 3.47E-03*	
#	24			.55 .52	-	.47 .51	7		3 4 E +		-	4E +1			# 2.50E-03*	
#	50			96.	*	•51	# H		3 7 C + 3 5 E +			4C + 1 5E + 1	_		# 2.00E=03*	
#	3 U		-	.96		•55	,	•	295.∓ 44E+	_		7E +1	_		# 1.0-E=03*	
-	31		. 47	· 77) 4==:		•776 =======	7 :::	7•' ::::	 	 			- " = = =	31012.0,	=	==========

MAXIMUM CONDUCTIVITY # .10 (MHOS/M)

**	* = = = =	# =		: 3		= = :	2223	===	==	111	3 2 2	3 2 3	E	= = :	===	2 3 1 1		22222222
#P(DINT10		NOZZLE	١ :	RACIUS	#1	FOCKE	T	1	RE	DEY	E					FREGU	ENCY #
#	2.06	#	1.4	8	·-02	#1	POSIT	ION		50	000	FT)	/1	0 (FT/	5) 4	2.50	E+08 #
#	(H)	#		M)	#!	PPESS	URE		0.	832	(A	TM	CS	PHE	PESI) (H	?) #
22:		F :		: =:		# # #	2222	===	= =	===	3 23	===	22	==:	225	===:	. = 2 2 2 2 2 2 2 2 2	22222222
# 6	JAIGAS	#	RELATIVE	*	AESCLUT	E#	ELEC	TRO	۱,*	COL	LIS	ION	i#	استا	LAS	MA A	SIGHA +	EPSILON #
# 1	INDEX	#	PACIUS	*	RACIUS	#	DENS	ITY	*	FRE	QUE	NCY	# F	RE'	JUE	NCY	, *	
#		#		4	(M)	#	(1/	M3)	#	• (1/5)	#	- (:	1/5) (F (MHG/M) *	(FD/M) #
3 3 3	32225	= =		: 3:		3 Z :	====							-			: = = = = = = = = = = = = = = = = = = =	
#	1	#	0.00	•	0.00			-	_				-				6.29E-03*	
#	2	#	•69	#	٠ 0 1												6.31E-U3*	
#	3	#	1.36	*	• 0 2												6.40E-03+	
#	4	#	2.06	•	•03												# 6 30E+03*	
#	5	#	2.90	#	• 9 4												7.01E-03+	
#	6	#	3.5?	4	•05												7.78E-034	
#	7	#	4.26	•	.36												9.13E-03*	
#	9	#	5.02	*	.07												1.158-02*	
#	9	#	5.80	•	•99									_		-	1.59E-02*	
#	19	#	6∙61	#	•10												2.29E-02*	
#	11	#	7.44	*	•11												3.44E-024	
#	13	*	3. 29	*	•12			_					-	_	-		4.99F-02*	
#	13	#	9.17	*	•14			_					_			-	6.71E-02*	•
#	14	#	10.09	*	.15												8.07E-02*	
#	15	#	11.34	*	•16												# 6.65E-02#	
	16	#	12.03		18												8.04E-32*	
#	17	#	13.05	*	•13												6.318-02*	
¢	1.9	#	14.13	•	.21												4.03E-02*	
#	19	#	15.26	*	.23												2.09E-02+	
#	5.0	#	16.44	*	.24												9.43E=03*	
#	21	#	17.69	#	.26			-									4.12E-03*	
	55	#	19.01	*	•28												1.99F-03*	
#	23	*	20.41		• 30												1.26E-03*	
#	24	#	21.36	*	.32												1.435-03*	
#	25	#	23.51	-	.35												1.60F-03*	
#	26	#	25.23	*	.37												1.746-03*	
#	27	#	27.10		• 4 3					-	_						# 1.83E-J3*	
•	29	#	24.13	*	.43			-		_							1.86E-03*	
	23	#	31.36	*	.46								_		-		1.82E-03*	
	30	#	33.37	-	•50		-								_		1.716-03+	
#	31	#	36.55	•	•54			-									1.526-03*	
#	32	#	33.61	*	.58		-							_			1.25E+03*	
	33	#	43.09	-	.64					_	_						# 9.20E=04*	
#	54 55	# #	47.05		•69			_			_	-	-				5.36E-04*	
* * * *)7 ::::::	# ===	51.66 =======	* ==:	.76 =======												# 1.34E-04* =======	

MAXIMUM CUNDUCTIVITY # A+65E+02 (MHOS/M)

# :	======	ŧ #	******	325		===	******	= = :	*** = = = =		********		*********	2
#1	FOINT1	1#	NOZZL	EF	ACIUS	#5	ROCKET	1	REDEYE	:	•	FREGL	ENCY (•
	2.36	#	1.	486	~02	# 5	POSITION		5000(F	TII	19(FT/S) #	2.50	E+08	#
	(H)			(H)		# 5	FRESSURE		0.832	(AT	MOSPHERES	(H	(Z)	#
3	*****	2 3		===	******	= = :	=======================================	= = 1		222		********	********	=
	RADIA	L#	RELATIV	EF	ARSCLUT	E#	ELECTRO	h+ (COLLIS	ON	PLASMA #	SIGMA •	EPSILON (#
	INDEX	#	RACIUS	*	PACIUS		CENSITY	# (FREQUE	ICY J	FREQUENCY#	•	•	#
				4	(P)		(1/M3)		(1/5)		(1/5)	(HNOHM)	(FD/H)	
=		= =		===	******	Z	88233225	===	======	====	**========		*********	z
	1	#	0.00	#	0.00	#	_9,79£ +1 (6#	2.36E	11#	1.582+89#	3.69E-034	. 8.84E-12	ŧ
	2	#	.73	*	• છે ≱	é	3 a 1 NE +1	6*	2.36E	11#	1.57E+89#	3.75E-034	4.84E-12	•
#	3	*	1.46	*	50 •	*	3.81E+1	6*	2.37E	114	1.63E+09#	3.93E+034	8.54E-12	•
#	4	#	2.19	*	•0.≛	ĸ	₫ a 51E +1 !	€*	2.345	111	1.71E+09#	4.27E-054	8.84E-12	#
	5	#	2.93	*	-04	•	-4.10E+1	6*	2.40E	11#	1.82E+0+#	4.81E-034	8.835-12	#
	6	#	3.60	*	.05	#	4. 11E+1	6*	2.45E	11#	1.99E+09#	5.7CE-034	8.83E-12	#
#	7	#	4.45	#	.07	#	6.17E+1	6*	2.45E	114	2.23E+094	7.09E-334	6.83E-12	#
	8	*	5.23	*	.08	#	8.20E+1	6#	2.43E+	114	2.57E+09#	9.33E-034	1.82E-12	ŧ
#	9	#	5.03	#	• 39	#	1.148+1	7*	2.50E+	114	: 3.03E+09#	1.28E-024	9.80E-12	#
#	10		5.54	#	-10	#	1.636+1	7+	2.52E	114	; 3.53E+09#	1.83E-024	8.795-12	#
#	11	#	7.57	•	.11	#	2.34E+1	7#	2.53E	-114	4.35E+094	2.61E-02	8.75E-12	•
#	12	#	3.53	*	.13	#	3.28E+1	7+	2.54E	-116	5 - 14E+09#	3.64E-024	6.71E-12	#
	1.3	#	4.41	#	.14	#	4.36F+1	7#	2.54E	111	, 23E+09#	4.83E-024	6.66E-12	•
#	14	4	10.32		•15	#	5.32E+1	7+	2.54E	-114	₿ 6.55E+09¢	5.91E-024	3.62E-12	#
#	15	#	11.2€	*	•17	#	5.49E+1	7#	2.53E	111	6.99E+094	6.57E-024	8.595-12	#
#	15	#	12.23	#	•15	#	5.42E+1	7*	2.51E	111	₽ 6.73E+091	6.32E-02	9.60E-12	#
	17	#	13.23	#	•20		4.42E+1	7*	2.48E	114	\$ 5.97E+09#	5.03E-024	8.65E-12	#
#	18	#	15.36	+	•23	#	1.44E+1	7+	2.40E	111	\$ 3.41E+09#	1.69E+02	9.78E-12	#
#	19	4	15.49	•	.24	#	6.39E+1				F 2.27E+094		8.32E-12	2
#	23	#	17.67	#	• 56		2.686.+1	6#	2.30E	114	1.47E+094	3.28E-034	6.84E-12	#
	21	#	18.92	*	.28		1.16E+1	6*	2.24E	111	F 4.68E+084	1.46E-03		
#	5.5		20.22	•	.30	#	5.148+1	5+	2.13E	111	/ 6.86E+081	7.575-044	4.85E-12	#
#	23		21.60	•	•32	#	3.73E+1	5+	2.11E	-114	\$ 5.48E+08f	1 4.49E-04	9.85E-12	#
#	24	#	23.35	*	• 3 4	#	3.19E+1				# 5.07E+03/			
#	25	#	24.00	*	• 36	#	· · · · -				6.06E+034			-
#	26	#	25.25	*	•39	#	5.240+1	-			6.50E+084			
#	27	#	23.02		.41	#	5.52F+1				# 6.67E+08			
#	24	#	29.91	*	• 4.4	#	5.565+1				# 6.69E+031			
#	23	#	31.96	•	•47	#	5.41c+1			_	F 6.61E+03			
#	30	#	34.19	*	•50	#	5.11E+1	5+	1.56E	+114	# 6.42E+C81			
#	31	Ħ	36.61	*	•54	#	4.65E+1				P 6.12E+036			
#	32	*	34.27	*	•58	#	4.05t +1				# 5.72E+036			
#	53	#	42.20	*	• 62	#					# 5.20E+016			
	34	#	45.45	•	.67	#					# 4.58£+08 <i>6</i>			
#	35	#	49.35	•	.72	#		-			# 3.95E+050			
#	36	#	53.13	-	.78	#	1.05E+1				# 2.32C+091			
f	37		57.64	#	• 6 5		4.34E+1	4*	1.11E	+114	# 1.98E+09	1.11E-J4	• 9.85E-12	#
3	======	= #		===		==	======	==	22222	===:	*********	*********	*********	=

MAXIMUM CONDUCTIVITY : 6.575-02 (MHOS/M)

```
NOZZLE MACIUS
                          #ROCKET
                                    * REDEYE
                                                             FREQUENCY
#FOINT12#
                          #FGSITION : 5000(FT)/10(FT/5) #
  2.67 #
              1.48E-02
                                                              2.50E+08
  (M)
                (H)
                           #PRESSURE 1 0.832 (ATMOSPHERES#
                                                                (HZ)
RADIALO RELATIVES APSCLUTED FLECTRONSCOLLISIONS PLASMA & SIGMA * EPSILON S
 INDEX # FACIUS *
                   FACIUS # DENSITY *FREQUENCY#FREQUENCY#
                          # (1/M3) * (1/S) # (1/S)
                                                       # (MHC/M) *
                     (+)
0.00 *
                     0.00
                          # 2.63E+16* 2.39E+11# 1.46E+09# 3.10E-03* 6.84E-12#
                          # 2.6 9E+16* 2.3 3E+11# 1.47E+03# 3.16E-03* 8.84E-12#
            .75
                      .01
           1.51
                      .02
                           # 2.87E+16# 2.40E+11# 1.52E+09# 3.37E-03# 8.94E-12#
           2.27
                      . 63
                          # 3.200+16+ 2.410+11# 1.610+09# 3.746-03+ 5.840-12#
    5
       #
           3.04
                      .04
                          # 3.72E+16* 2.43E+11# 1.73E+09# 4.32E-03* 8.54E-12#
                           # 4.53E+16+ 2.44E+11# 1.91E+09# 5.22E-03+ 8.83E-12#
           3.91
                      .06
                      .07
    7
                          # 5.75L+16+ 2.46E+11# 2.15E+09# 6.59E-03+ 5.83E-12#
       .
           4.60
           5.40
                      .09
                            7.52E+16# 2.48E+11# 2.46E+39# 8.56E-03# 8.82E-12#
                      .09
                          # 1.02E+17" 2.49E+11# 2.86E+09# 1.15E-02" 8.81E-12#
           6.21
                      .10
                          # 1.39E+17* 2.51E+11# 3.34E+09# 1.56E-02* 8.79E-12#
           7.03
           7.85
                      .12
                          # 1.87F+17* 2.52E+11# 3.89E+09# 2.15E-02* 8.77E-12#
   11
                          # 2.496+17* 2.52E+11# 4.48E>09# 2.79E-02* 8.74E-12#
   12
       #
           3.74
                      .13
   13
           9.63
                      .14
                          # 3.176+17* 2.526+11# 5.06E>09# 3.54E-02* 8.715-12#
                          # 3.00E+174 2.52E+11# 5.53E+09# 4.25E+02# 8.69E+12#
                      .16
   14
          10.54
   15
          11.47
                      .17
                           # 4.19E+17* 2.51E+11# 5.81E+09# 4.71E-02* 8.67E-12#
                          # 3.99E+17* 2.49E+11# 5.67E+09# 4.51E-02* 5.67E-12#
    16
       #
          12.43
                      .18
                      .20
                          # 3.12E+17# 2.47E+11# 5.02E+39# 3.56E-92# 8.71E-12#
   17
          13.43
                          # 1.96F+17# 2.44E+11# 3.9dE+09# 2.27E-02# 8.76E-12#
          14.45
   18
       #
                      . 21
          15.51
                          # 1.42E+17# 2.41E+11# 2.46E+09# 1.19E-02# 8.40E+12#
    19
       .
                      .23
                          # 4.58E+16* 2.37E+11# 1.92E+09# 5.45E-03* 8.83E-12#
    20
          16.51
                      . 25
                      .26
                          # 1.92F+16* 2.32E+11# 1.25E+09# 2.33E-03* 6.84E-12#
    21
          17.76
                      • Z 8
                          # 8.09E+15* 2.27E+11# 8.07E+05# 1.00F-03* 5.85E-12#
    23
          18.35
                      .30
       #
          23.26
                          # 3.70E+15* 2.22E+11# 5.46E+03# 4.70E-04* 8.85E-12#
    23
                      .32
                          # 2.02E+15# 2.16E+11# 4.03E+34# 2.63E+04# 8.85E-12#
          21.50
   24
                          # 1.39E+15* 2.10E+11# 3.35E+03# 1.07E-04* 8.05E-12#
    25
          35.55
                      . 34
          24.32
                      .36
                           # 1.29E+15# 2.03E+11# 3.21E+03# 1.77E-04# 9.35E-12#
    25
                          # 1.47F+15* 1.96E+11# 3.48E+P3# 2.68E-04* 8.85E-12#
    27
       .
          25.34
                      . 33
   23
          27.45
                      .40
                           # 2.54E+15+ 1.89E-11# 4.55E+03# 3.49E-04+ 8.85E-12#
                          # 2.578+15* 1.925+11# 4.646+00# 4.146-04* 8.856-12#
    29
       .
          29.17
                      .43
                           # 2.96E+15* 1.75E+11# 4.81E+09# 4.61E-04* 8.85E-12#
    30
       #
          33.99
                      .45
                          # 2.33E+15* 1.63E+11# 4.46E+08# 4.92E-04* 3.85E-12#
                      . 49
          32.34
    31
                           # 2.39E+15* 1.61E+11# 4.83E+J6# 5.07E+34* 8.85E-12#
           35.04
                      .52
    32
                           # 2.76E+15# 1.54E+11# 4.72E+03# 5.06E-04# 3.85E-12#
    33
       #
           37.50
                      .55
                           # 2.55°+15* 1.47E+11# 4.53E+08# 4.3UE-04* 8.35E-12#
    54
       .
          39.75
                      .59
                           # 2.27E+15* 1.4WE+11# 4.28E+06# 4.57E-04* 8.85E-12#
    35
          42.40
                      -63
                           # 1.3 T+15* 1.34E+11# 3.96E+04# 4.09E-04# 3.85E-12#
    36
          45.30
                      . 67
                           # 1.5 tE+15* 1.28E+11# 5.57E+03# 5.47E+04* 8.85E+12#
    37
          49.47
                      .72
                           # 1.19E+15# 1.23E+11# 3.10E+03# 2.74E-04# 8.85E-12#
    39
           51.95
                      .77
                           # 8.02E+14* 1.18E+11# 2.54E+08# 1.92E-34* 8.85E-12#
    39
          55.7€
                      . 32
                           # 4.16E+14* 1.13E+11# 1.83E+J8# 1.03E-04* 8.85E-12#
        #
           60.01
                      . 99
    40
                           # 9.53E+13* 1.10E+11# 9.31E+07# 2.43E-05* 8.85E-12#
    41
       .
          64.65
                      • 35
```

MAXIMUM CONGUCTIVITY : 4.715-02 (MHCS/F)

=	******		*******************	
	POINT13		#FGCKET # REDEYE	• FREQUENCY #
	2.97		#FOSITION : 5000(FT)/10(FT/	
	(H)	# (M)	#PRESSURE # 0.832 (ATMOSPHE	
3				
	RADIAL			MA # SIGMA * EPSILON #
7	XACNI	F RACIUS * RACIUS F (M)	# DENSITY *FREQUENCY#FREQUE # (1/M3) * (1/S) # (1/S) # (MHC/M) * (FD/M) #
•	,			
-	1	# 0.0C + 0.00	# 2.90E+16+ 2.42E+11# 1.53E	
•	2	# .74 + .91	# 2.76F+16* 2.43E+11# 1.55E	
ï	3	1.56 • .02	# 3.156+16+ 2.43E+11# 1.6VE	
	4	# 2.34 + .G3	# 3.32E+16* 2.44E+11# 1.66E	
•	5	# 3.12 * .05	# 4.06E+16* 2.45E+11# 1.81E	+03# 4.60E-03* 8.84E-12#
#	6	# 3.92 * .06	# 4.35C+16* 2.46E+11# 1.98E	+09# 5.56E=03* d.83E=12#
	7	# 4.72 * .07	# 6.000+16# 2.47E+11# 2.20L	+09# 5.84E-03* 8.83F-12#
	9	# 5.54 * .08	# 7.59E+16+ 2.43E+11# 2.47E	
୍ୟ) j	# 5.36 * .09	# 9.70E+16* 2.49E+11# 2.80E	
•	19	# 7.20 * .11	# 1.24E+17* 2.50E+11# 3.16E	
	11	# 3.06 * .12	# 1.58E+17* 2.50F+11# 3.57E	
		4.93 * .13	# 1.455+174 2.515+11# 4.006	
		4 4.43 4 .14	# 2.39E+17* 2.50E+11# 4.59E	
-	14	# 10.74 * .16	# 2.7nt+17* 2.50E+11# 4.71E	
- 7	15	# 11.67 * .17 # 12.63 * .19	# 2.926+17+ 2.496+11# 4.556 # 2.696+17+ 2.476+11# 4.566	+03# 3.06E-02* 3.73E-12#
7	15 17	# 13.62 * .20	# 2.35E+17" 2.46E+11# 4.36E	
-	14	# 14.64 * .22	# 1.27E+17* 2.43E+11# 3.20E	
-	19	# 15.69 * .23	# 5.61F+16* 2.40E+11# 2.316	
	20	# 16.77 * .25	# 3.04t +16* 2.37E +11# 1.57E	
	21	£ 17.49 * .26	# 1.30F+16* 2.33E+11# 1.02E	
1	22	# 19.06 * .2A	# 5.49E+19# 2.29E+11# 6.53E	
4	2.3	# 20.27 * .30	# 2.40E+15* 2.24E+11# 4.40E	+03# 3.01E-04* 8.45F-12#
4	24	# 21.55 * .3 2	# 1.20E+15* 2.13E+11# 3.11E	◆03# 1.54E-04* 8.85E-12#
	25	# 22.34 # .34	# 7.43E+14* 2.14E+11# 2.456	+04# 9.20E-35* 8.35E-12#
	26	# 24.22 * .35	# 5.90c+14* 2.09E+11# 2.18E	
•	27	# 25.66 * .38	# 6.12E+14+ 2.02E+11# 2.22E	
4	24	# 27.17 * .40	# 9.7eF+14* 1.36E+11# 2.d1E	
-	23	# 23.77 • .42	# 1.275+15+ 1.39E+11# 5.20E	
	30	# 30.46 * .45		+01# 2.27E-04+ 3.45E-12#
	31	# 32,24 * .48	# 1.618+15* 1.768+11# 3.608 # 1.686+15* 1.708+11# 3.688	
-) 32) 3 3	# 34.14 * .50 # 36.17 * .53	# 1.70++15+ 1.63E+11# 3.70E	
7	3 1	* 30.54 + .57	# 1.646 +15* 1.576 +11# 3.936	
-	35	# 40.66 * .60	# 1.6uf+15# 1.50F+11# 3.60E	
4	36	• 43.16 • .64	# 1.43E+15* 1.44E+1;# 3.47E	
î	37	# 45.45 + .64	# 1.34E+15* 1.39E+11# 3.29E	
•	19	* 43.77 * .72	# 1.175+15* 1.34E+11# 4.J6E	
	39	# 51.94 ^ .77	# 9.59E+14* 1.20E+11# 2.79E	+03# 2.13F-04# A.95E-12#
4	40	# 55.37 * .42	# 7.535 +14* 1.236 +11# 2.486	
•	41	# 54.19 * .97	# 5.57E+14+ 1.13E+11# 2.12E	
4	42	# 63.14 *3	# 3.5%E+14* 1.15E+11# 1.705	
4	4 4	# 57.50 * 1.00	# 1.76f +14* 1.12E+11# 1.19E	
1				

MAXIMUL SUNCUSTIVATY & 3.315-02 (MH03/M)

3		3		3 2 3	11555	I F	2==	Z = :		2 2	2 3	2 T 3:	===	22	2 2 2	1 2 3	= = = :	*********	********
	FCINT14	4	NCZZL	E I	F. A C I US		FOC	KET	r	1	R	EDE	/ E					● FREQUE	NCY #
	3.01	#	1.	431	E-05		PCS	IT	LON		5	000	(FT)	/1	ij (F	1/	SI	c 2.50E	E+08 #
	(H)			(#)		FRE	SSI	JRE	1	0	. 8 32	? (A	ITH	056	HE	FES	₽ (H2	(1)
		.	22432322	23	******	3 #	T = E	3 8 2	. = 3	3 # :	# =	2 2 2 3		23	2 3 3	* = =	Z Z Z	*********	********
•	RADIAL	. #	RELATIV	E#	AESCLUT	E#		-									MA .		EPSILON #
	INDEX	#	RACIUS	•	FACIUS		DE	115	YT1	•	FR	EQU	NCA	#F	PEG	iUE	NCY	• •	
4	1	*		*	(M)	#	(1/1	43)	*		(1/9	;)	•	(1	./\$)	* (HYOHH) *	(FD/H) #
3		3	*****	# 2 :	======	T B	3 E #	* = :	* * * *	8 X	= =	2 2 3 3	3 2 2 3	23	3 Z I	* * *	3 # 2	**********	*******
•	1	*	0.00	*	u.00		2.	976	E+1	6+	2	. 4 从	+11		1.5	55E	+09	# 3.45E-03+	1.84E-12#
1	2	#	1.56	#	• 0 Z	#	3.	241	+1	5*	2	. 43	+11		1.8	356	+99	# 3.75E-03*	8.84F-12#
4	3	#	3.14	•	•05		4.	1 46	+3	6+	_		+11	-	•••		+09		5.83C+12#
4	4	*	4.74	*	.07	#	6.	078	+1	5*	2	. 476	+11	_			+03		8.83F-12#
	5	#	6.38	•	.09	•	4.	671	+1	6+	_		+11	-				# 1.09E+32*	8.61E-12#
4	6	#	9.00	•	.12	•	1.	561	E + 1	7+	2	. 566	E+11		3.5	54E	+49	# 1.75E-02*	8.76E-12#
1	7	#	9.85	*	•15	#	2.	310	*:	-	_		+11		4.3	SSE	+09	# 2.60E-02*	8.75E-12#
4	9	#	11.70	*	-17		5.	798	E+1	7*			+11				+09		5.73E-12#
4	9	#	13.65	#	.20	#	1.	331	+1	7#	2	• 456	+11	, #	3.9	34E	+09	# 2.22E-02#	8.765-12#
1	10	#	15.71	*	.23	4	6.	5 36	+1	6=	2	• 40t	+11	# 1	2 . 2	4E	+03	# 7.31E-03*	5.52E-12#
	11	#	17.91	*	•26		1.	236	+1	64	2	. 336	+11	-			t 0 +		8.85E-12#
4	12	#	20.28	*	.30		2.	278	+1	5+	2	. 246	+11		4.2	7E	t 0 +	# 2.85E-04*	8.85E-12#
4	13		22.94	•	.34	#	6.	778	E+1	4=	2	. 14	+11		2.3	14E	+09	# 9.91E-05*	8.85E-12#
4	14	#	25.64	*	.38	#	5.	366	+1	4#	_		+11				+05		8.855-12#
	15	#	23.74	•	•42	#	1.	106	.+1	5*	1	. 306	+11				+0 8		8.85E-12#
	15	#	32.16	*	.47	•	_		+1				+11				+ U 9		8.85E-12#
#	17	#	36.06	#	•53	#	1.	606	1 + 1	5*	_		+11	-			t 0 +		8.55E-12#
4	1.3	#	40.49	#	.60	#	1.	536	+1	5*	1	.526	+11	.#	3.5	31E	+03	# 2.94E-04+	8.85E-12#
4	70	•	45.60	*	.67	#	1.	301	+1	5*	-		+11				£ 0 +		8.85E-12#
1	05	#	51.57	*	.76	#	۹.	61	E + 1	4#			+11				+03		a.a5E-12#
	21		54.58	*	. 36	#	5.	75	-+1	4*	1	. 206	+11	# .	2.1	.5E	+03		8.85E-12#
4	22	#	56.35	•	.99	#	1.	316	+1	4#	1	. 1 26	+11		1.3	4E	+ 0 ¤	# .79E-05+	3.85E-12#
		3		2 2	22335732	= =	===	223	= = =	2 2	3 3	332	1333	35	2 E :	: 3 2	222	**==**==	22222223

MAXIMUM CONCUCTIVITY : 3.16E-02 (MHOS/M)

#PCINTIS# NOZZLE RACTLS #PCCKET 1 REDEVE # FR	
ALCOMITY A MOTERE WASTED ALCOMAN A MEDICAL	EQUENCY #
6 3.32 # 1.43€-02 #PDSITION # 5000(FT)/10(FT/S) # 2	.50 €+00
# (M) # (M) #PRESSURE # 0.832 (ATMOSPHERES#	(HZ) #
- 医黑色素性含含染 医电影 医克兰氏 计多点 不是 医皮肤 医皮肤 医皮肤 医皮肤 医生物 医皮肤 医皮肤 医皮肤 化二氯甲基甲基苯甲基甲基	**********
# RADIAL# RELATIVE+ AESCLUTE# ELECTRON#COLLISION# PLASMA # SIGMA	+ EPSILUN #
# INDEX # RACILS # RACIUS # DENSITY #FREQUENCY#FREQUENCY#	•
# # # (MHC/M	i) * (FD/H) #
***************************************	2222272222
# 1 # 0.00 # 0.00 # 3.58E+16* 2.44E+11# 1.70E+09# 4.14E*	13* 6.84F-12#
# 2 # 1.61 * .02 # 3.A7E+16* 2.44E+11# 1.77E+09# 4.46E*	03+ 4.84E-12#
# 3 # 3.22 # .05 # 4.79E+16# 2.46E+11# 1.37E+0+# 5.43E-	• • • • • • •
# 4 # 4.86 * .07 * 6.55E+16* 2.47E+11# 2.3UE+39# 7.47E*	034 8.82E-12#
# 5 # 6.53 * .10 # 9.43E+16* 2.44E+11# 2.76E+09# 1.07E	102 0.01E-12#
# 6 # 8.26 * .12 # 1.36E+17* 2.43E+11# 3.31E+09# 1.54E-	124 6.795-12#
# 7 # 10.04 * .15 # 1.11E+17* 2.4至+11# 3.42E+09# 2.05E*	
# 1 # 11.90 # .1# # 1.96E+17* 2.47E+11# 3.97E+09# 2.23E-	
# 3 # 13.85 * .20 # 1.24E+17* 2.44E+11# 3.16E+09# 1.43E*	
# 10 # 15.31 * .23 # 4.04E+16* 2.39E+11# 1.90E+09# 4.75E-	
# 11 # 18.08 * .27 # 8.83E+15* 2.53E+11# 8.44E+0## 1.07E	
A TO A CITAL SOUND A TAILORING CATALOGUE AND	1044 9.85E-124
# 13 # 22.90 * .34 # 4.42E+14+ 2.16E+11# 1.39E+0d# 5.76E-	
# 14 # 25.61 * .34 # 2.50E+14* 2.06E+11# 1.45E+08# 3.56E	-05- 8.95E-12-
# 15 # 23.56 * .42 # 5.55E+14* 1.95E+11# 2.12E+08# 3.02E	
# 15 # 31.81 * .47 # 7.35E+14* 1.85E+11# 2.53E+08# 1.22E	
# 17 # 35.42 * .52 # 9.49E+14* 1.71E+11# 2.77E+09# 1.56E-	
# 18 # 39.46 # .58 # 1.JOE+15# 1.6GE+11# 2.94E+03# 1.775	-04# 8.85E-12#
# 19 # 44:05 + .65 # 9.56F+14* 1.4 E+11# 2.78E+09# 1.32E	-04# 8-35E-12#
# 20 # 43.25 + .73 # 8.26F+14* 1.38E+11# 2.58E+0## 1.69E	
# 21 # 55.26 * .82 # 6.418+14* 1.29E+11# 2.27E+09# 1.4GE-	
# 22 # 62.13 * .92 # 4.39E+14* 1.21E+11# 1.86E+09# 1.02E	-04+ 5.85E-12#
# 25 # 63.31 * 1.03 # 2.56E+14* 1.15E+11# 1.44E+08# 6.26E	-954 8.85E-128
# 24 # 73.19 * 1.15 # 1.12E+14* 1.11E+11# 9.52E+37# 2.35E-	-05+ 3.555-12#

MAXIMUM CUNCUCTIVITY : 2.23E-02 (MHCS/F)

=		3	*****	2 2 2	*******	# # :	***	1 3 1		==	3 \$	32	221			* * 1	*********	*********
	FCINT16	#	NOZZL	Ē.	ACIUS	# 1	FOCE	EŢ		1	ŔΕ	DEY	Έ			- (FREGUE	NCY .
	3.65	#	1.	486	-02	# (PO 5	[1]	CN	1	5.	L0(FTI	/1	L0(FT/S) (₹ 2.50€	+06
	(M)	ø		(4)	ı		ac E ?	SSU	RE		٥.	9 32		\TP	10SPHER	ESI) (HZ	•
2		8	*******	* * 2	********	2 2 2	EST	123	===	= =	* *	3 2 3				== 1		*******
	RADIAL		RELATIV	€*	AESCLUT	E #	EL	CI	RON	, * C	OF	LIS	ION	1#	PLASM	A 4	SIGHA *	EPSILON #
	INDEX	#	FACIUS	*	RACIUS		OF	15 I	TY	+ F	ĸΕ	QUE	NCY	#F	REQUEN	CY	•	•
				*	(M)	•	(:	L/H	5)	#	(1/5)	•	(1/5)	- 4	* (MHO/M) *	(FO/H) #
8	****	=	* * * * * * * *	Z Z 1	******	## :		: 2 :	# # #	* =	= 3	* * *	321	21	*****	= = :	*********	*******
•	1	٠	0.00	4	0.00		4.								1.94E+			
	2		1.64	*	.02	#	4 .	32E	+16	*	۶.	46E	+11		1.995+	-		6.93E-12#
	3	#	3.29	+	.05	•	5.	35	+16				+11		2.155+			
	4	#	4.97	•	.07		7.0			-			+11		2.412+			8.82E-12#
	5	#	6.67	*	.10		9.0			-			+11		2.76E+			5.81E-12#
	6	#	8.42	*	.12	#	1.6	?1E	+17				+11		3.12E+	•	• •	6.90E-12#
	7	*	10.23	*	.15		1.4	+5E	+17	•	г.	47E	+11	L#	3.410+	691	1.656-024	8.798-12#
	8		12.10	*	•18	•	1.3	5 S E	+17	*	۶.	465	+11	#	3.30£+			8.79E-12#
•	9	#	14.06	+	.21	#	7.9	3E	+16	*	2.	43E	+11		2.46E+	046	8.74E-03*	4.822-12#
#	10	#	16,11	4	. 24	#	2.4	11	+16	*	۶.	3 BE	+11	ļ 🗘	1.33E+	031	2.85E-03*	8.84E-12#
•	11		19.27	*	•27		5.	5 S E	+13				+11	-	6.69E+			8.85E-12#
	7.5	#	20.57	#	.30	#	1.1	50	+15	#	2٠	2 6E	+11		3.04E+	0 31	1.43E-34*	8.855-12#
¢	1.3	#	23.02	•	. 34		2.	30E	+14	, .	2.	1 3E	+11		1.536+	0 .		3.85E-12#
	14	#	25.65	#	.35	#	1.5	3E	+14	,*	2.	9 JE	+11		1.15E+	091	2.20E-05*	5.35E-12#
,	15	#	28.5C	*	.42	#	3.	95	+1.4	*	1.	38€	+11	#	1.68E+	081	4.95E-05+	9.85E-12#
	15	#	31.61	*	•47	#	5.1) Y F	4:4	۲,	1.	8 5E	+11	l #	2.02E+	3 44	7.63E-05*	C.85E-12#
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	19	ü	43.02	*	•63	#	7.) SE	+14	-		–	+11	-	2.386+			A.45E-12#
	20	#	47.75	*	.70	#			+14		_			-	2.30E+	-		8.35E-12#
	21	#	53.10	*	.78	#	5.7	11	+14	•	-			-	2.15E+			8.65E-12#
	22	٠	5).14	•	.67	#	4.5	65	+14	+	1.	2 8E	+11	#	1.925+	081	1.00E-04*	5.85E-12#
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	25	•	61.52	•	1.20	#	1.1	13E	+14	•	1.	1 2E	+11		9.54E+	076	2.83E-05*	8.856-12#
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MAXIMUM CONCUCTIVITY # 1.65E-02 (MHOS/M)

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MAXIMUM CONCULTIVITY : 1.32E-C2 (MHOS/M)

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# 4 # 5.16 + .0A # 8.11E+16* 2.47E+11# 2.56E+09# 3.26E-03* 8.82E-129 # 5 # 6.92 * .10 # A.92E+16* 2.47E+11# 2.68E+09# 1.02E-02* 4.81E-12# # 6 # 3. 2 * .13 # 9.48E+16* 2.46E+11# 2.77E+09# 1.09E-02* 4.81E-12# # 7 # 10.7 * .16 # 8.77E+16* 2.45E+11# 2.65E+03# 1.09E-02* 4.81E-12# # 8 # 12.48 * .19 # 5.36E*16* 2.45E+11# 2.17E+09# 3.06E-02* 3.31E-12# # 9 # 14.4E * .21 # 2.62E+16* 2.40E+11# 1.45E+09# 3.06E-03* 8.94E-12# # 10 # 16.52 * .24 # 8.29E+15* 2.36E+11# 5.18E+08# 9.91E-04* 9.85E-12# # 11 # 18.68 * .28 # 2.14E+15* 2.31E+11# 4.15E+08# 2.61E-04* 8.85E-12# # 12 # 20.95 * .31 # 5.11E+14* 2.29E+11# 1.04E+08# 1.75E+05* 8.85E-12# # 13 # 25.34 * .34 # 1.54E+14* 2.19E+11# 1.04E+08# 1.75E+05* 8.85E-12# # 14 # 25.89 * .35 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E-06* 8.85E-12# # 15 * 28.61 * .42 # 5.23E+13* 2.03E+11# 6.49E+07# 7.21E-06* 8.85E-12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E-05* 8.85E-12# # 17 # 34.66 * .56 # 3.31E+14* 1.34E+11# 1.44E+08# 3.91E-05* 3.95E-12# # 18 # 38.13 * .56 # 3.31E+14* 1.34E+11# 1.63E+08# 5.33E-05* 3.95E-12# # 19 # 41.89 * .62 # 3.30E+14* 1.75E+08# 5.33E-05* 3.95E-12# # 20 # 46.03 * .68 # 4.00E+14* 1.55E+11# 1.63E+08# 7.23E-05* 8.85E-12# # 21 # 50.60 * .75 # 3.33E+14* 1.55E+11# 1.71E+08# 7.32E-05* 8.85E-12# # 22 # 55.67 * .92 # 3.31E+14* 1.32E+11# 1.71E+08# 7.32E-05* 8.85E-12# # 22 # 55.67 * .92 # 3.31E+14* 1.32E+11# 1.75E+08# 7.32E-05* 8.85E-12# # 23 # 61.3C * .99 # 3.12E+14* 1.32E+11# 1.75E+08# 7.32E-05* 8.85E-12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.32E+11# 1.59E+08# 6.67E-05* 8.85E-12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.25E+11# 1.54E+08# 4.44E-05* 8.85E-12#	-				
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# 10.7	•				
# 0 # 12.48 * .18 # 5.86E + 16* 2.43E + 11# 2.17E + 05# 5.81E - 12* # 2.62E + 16* 2.40E + 11# 1.45E + 05# 3.06E - 03* 8.34E - 12* # 10 # 16.52 * .24 # 6.29E + 15* 2.36E + 11# 3.18E + 08# 9.91E - 04* 9.85E - 12* # 18.66 * .28 # 2.14E + 15* 2.31E + 11# 4.15E + 08# 2.61E - 04* 8.85E - 12* # 12 # 20.95 * .31 # 5.11E + 14* 2.24E + 11# 1.04E + 05# 2.61E - 04* 8.85E - 12* # 13 # 25.34 * .34 # 1.54E + 14* 2.12E + 11# 1.04E + 05* 1.75E - 05* 8.85E - 12* # 14 # 25.88 * .35 # 5.40E + 13* 2.11E + 11# 6.60E + 07* 7.21E - 05* 8.85E - 12* # 14 # 25.88 * .47 # 1.60E + 14* 1.34E + 11# 1.14E + 08# 3.91E - 05* 8.85E - 12* # 16 # 31.53 * .47 # 1.60E + 14* 1.34E + 11# 1.44E + 08# 3.91E - 05* 8.85E - 12* # 17 # 34.69 * .51 # 2.76E + 14* 1.34E + 11# 1.44E + 08# 3.91E - 05* 8.85E - 12* # 18 # 38.13 * .56 # 3.31E + 14* 1.75E + 11# 1.63E + 08# 5.33E - 05* 8.85E - 12* # 18 # 38.13 * .56 # 3.31E + 14* 1.75E + 11# 1.63E + 08# 5.33E - 05* 8.85E - 12* # 19 # 41.89 * .62 # 3.90E + 14* 1.65E + 11# 1.75E + 08# 6.47E < 05* 8.85E - 12# 8					
# 9 # 14.46 * .21 # 2.62E+16" 2.40E+11# 1.45E+09# 3.06E-03* 8.94E-12# 10 # 16.52 * .24 # E.29E+15* 2.36E+11# 8.18E+08# 9.91E-04* 8.85E-12# 11 # 18.68 * .28 # 2.14E+15* 2.31E+11# 4.15E+08# 2.61E-04* 8.85E-12# 12 # 20.95 * .31 # 5.11E+14* 2.29E+11# 2.03E+00# 6.40E+05* 8.85E-12# 13 # 25.34 * .34 # 1.54E+14* 2.13E+11# 1.04E+09# 1.75E+05* 8.85E-12# 14 # 25.89 * .38 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E-06* 8.85E-12# 15 # 24.61 * .42 # 5.23E+13* 2.03E+11# 6.49E+07# 7.28E-06* 3.85E-12# 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E-05* 8.85E-12# 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E-05* 3.95E-12# 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E-05* 8.85E-12# 20 # 46.03 * .62 # 3.60E+14* 1.56E+11# 1.75E+08# 6.47E-05* 8.85E-12# 21 # 50.60 * 75 # 3.43E+14* 1.56E+11# 1.70E+08# 7.23E-05* 8.85E-12# 22 # 55.67 * .82 # 3.31E+14* 1.39E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 55.67 * .82 # 3.31E+14* 1.32E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 55.67 * .82 # 3.31E+14* 1.32E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 57.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E-05* d.85E-12# 24 # 67.53 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E-05* 8.85E-12#					
# 10 # 16.52 # .24 # E.29E+15* 2.35E+11# 5.16E+08# 9.91E-04* 9.05E-12# 11 # 18.68 * .28 # 2.14E+15* 2.31E+11# 4.15E+08# 2.61E-04* 8.85E-12# 12 # 20.95 * .31 # 5.11E+14* 2.29E+11# 2.03E+00# 6.40E-05* 8.85E-12# 13 # 25.34 * .34 # 1.54E+14* 2.14E+11# 1.04E+08# 1.75E+05* 0.85E-12# 14 # 25.89 * .35 # 5.4UE+13* 2.11E+11# 6.60E+07# 7.21E-06* 0.85E-12# 15 # 24.61 * .42 # 5.23E+13* 2.03E+11# 6.49E+07# 7.28E-06* 3.85E-12# 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E-05* 8.05E-12# 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E-05* 8.95E-12# 18 # 39.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E-05* 8.85E-12# 19 # 41.89 * .62 # 3.60E+14* 1.65E+11# 1.75E+08# 6.47E-05* 8.85E-12# 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.70E+08# 7.23E-05* 8.85E-12# 21 # 50.60 * 75 # 3.43E+14* 1.47E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 55.67 * .82 # 3.31E+14* 1.39E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 55.67 * .82 # 3.31E+14* 1.39E+11# 1.71E+08# 7.32E-05* 8.85E-12# 22 # 57.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E-05* d.85E-12# 24 # 67.53 * 1.10 # 1.89E+14* 1.25E+11# 1.24E+08# 4.44E-05* 8.85E-12#					_
# 11 # 18.68 * .28 # 2.14E+15* 2.31E+11# 4.15E+08# 2.61E=04* 8.85E=12# # 12 # 20.95 * .31 # 5.11E+14* 2.29E+11# 2.03E+00# 6.40E=05* 8.85E=12# # 13 # 25.34 * .34 # 1.54E+14* 2.13E+11# 1.04E+08# 1.75E=05* 8.85E=12# # 14 # 25.85 * .38 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E=06* 8.85E=12# # 15 # 24.61 * .42 # 5.23F+13* 2.03E+11# 6.49E+07# 7.28E=06* 3.85E=12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E=05* 8.85E=12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E=05* 8.95E=12# # 18 # 38.13 * .56 # 3.31E+14* 1.34E+11# 1.44E+08# 3.91E=05* 8.95E=12# # 19 # 41.85 * .62 # 3.60E+14* 1.65E+11# 1.75E+08# 6.47E=05* 8.85E=12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.70E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.43E+14* 1.56E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 22 # 55.67 * .82 # 3.51E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.30 * .90 # 3.12E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 8.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#				•	
# 12 # 20.95 * .31 # 5.11E+14* 2.29E+11# 2.03E+03# 6.40E=05* 8.85E=12# # 13 # 25.34 * .34 # 1.54E+14* 2.13E+11# 1.04E+05# 1.75E=05* 8.85E=12# # 14 # 25.85 * .35 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E=06* 8.85E=12# # 15 # 24.61 * .42 # 5.23E+13* 2.03E+11# 6.49E+07# 7.28E=06* 3.85E=12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E=05* 8.85E=12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E=05* 3.95E=12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E=05* 8.85E=12# # 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+08# 6.47E=05* 8.85E=12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.75E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.33E+14* 1.67E+11# 1.71E+08# 7.52E=05* 8.85E=12# # 22 # 55.67 * .82 # 3.31E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.3C * .90 # 3.12E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 8.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#					
# 13 # 23.34 * .34 # 1.54E+14* 2.14E+11# 1.04E+03# 1.73E+05* 0.05E-12# # 14 # 25.05 * .35 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E+06* 0.05E-12# # 15 # 24.61 * .42 # 5.23F+13* 2.03E+11# 6.49E+07# 7.20E+06* 3.05E-12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+00# 2.33E+05* 8.05E-12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E-05* 8.05E-12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E+05* 8.05E-12# # 19 # 41.89 * .62 # 3.00E+14* 1.65E+11# 1.75E+08# 6.47E+05* 8.05E-12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E+05* 8.05E-12# # 21 # 50.60 * 75 # 3.33E+14* 1.47E+11# 1.71E+08# 7.52E+05* 8.05E-12# # 22 # 55.67 * .92 # 3.31E+14* 1.39E+11# 1.71E+08# 7.32E+05* 8.05E-12# # 23 # 61.3C * .90 # 3.12E+14* 1.32E+11# 1.71E+08# 7.32E+05* 8.05E-12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+00# 5.67E+05* 0.05E-12# # 25 # 74.37 * 1.10 # 1.09E+14* 1.20E+11# 1.24E+08# 4.44E-05* 8.05E-12#					
# 14 # 25.85 # .38 # 5.40E+13* 2.11E+11# 6.60E+07# 7.21E-06* 8.85E-12# # 15 # 24.61 * .42 # 5.23F+13* 2.03E+11# 6.49E+07# 7.28E-06* 3.85E-12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E-05* 8.85E-12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E-05* 3.95E-12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E-05* 8.85E-12# # 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+08# 6.47E-05* 8.85E-12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E-05* 8.85E-12# # 21 # 50.60 * 75 # 3.33E+14* 1.47E+11# 1.71E+08# 7.32E-05* 8.85E-12# # 22 # 55.67 * .82 # 3.61E+14* 1.39E+11# 1.71E+08# 7.32E-05* 8.85E-12# # 23 # 61.3C * .90 # 3.12E+14* 1.32E+11# 1.71E+08# 7.32E-05* 8.85E-12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E-05* 0.85E-12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E-05* 8.85E-12#					
# 15 # 24.61 * .42 # 5.23F+13* 2.03E+11# 6.49E+07# 7.28E=06* 3.85E=12# # 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E=05* 8.85E=12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E=05* 3.95E=12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E=05* 8.85E=12# # 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+08# 6.47E=05* 8.85E=12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.33E+14* 1.47E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 22 # 55.67 * .82 # 3.61E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.3C * .90 # 3.12E+14* 1.32E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 0.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#					
# 16 # 31.53 * .47 # 1.60E+14* 1.34E+11# 1.14E+08# 2.33E=05* 8.85E=12# # 17 # 34.69 * .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E=05* 3.95E=12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E=05* 8.85E=12# # 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+05# 6.47E=05* 8.85E=12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.33E+14* 1.47E+11# 1.70E+08# 7.52E=05* 8.85E=12# # 22 # 55.67 * .82 # 3.61E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.30 * .90 # 3.12E+14* 1.32E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 0.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#			· · · · · · · · · · · · · · · · · · ·		
# 17 # 34.69 # .51 # 2.76E+14* 1.34E+11# 1.44E+08# 3.91E=05* 3.95E=12# # 18 # 38.13 * .56 # 3.31E+14* 1.75E+11# 1.63E+08# 5.33E=05* 9.95E=12# # 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+08# 6.47E=05* 8.85E=12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.43E+14* 1.47E+11# 1.70E+08# 7.52E=05* 8.85E=12# # 22 # 55.67 * .92 # 3.61E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.30 * .90 # 3.12E+14* 1.32E+11# 1.59E+09# 6.6dE=05* 3.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 8.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#					
# 18 # 38.13 * .56 # 3.315.+14* 1.75E.+11# 1.63E.+08# 5.33E.+05* 8.95E12# # 19 # 41.89 * .62 # 3.80E.+14* 1.65E.+11# 1.75E.+05# 6.47E.05* 8.85E12# # 20 # 46.03 * .68 # 4.00E.+14* 1.56E.+11# 1.80E.+08# 7.23E05* 8.85E12# # 21 # 50.60 * 75 # 3.43E.+14* 1.47E.+11# 1.70E.+08# 7.52E05* 8.85E12# # 22 # 55.67 * .82 # 3.51E.+14* 1.39E.+11# 1.71E.+08# 7.32E.+05* 8.85E12# # 23 # 61.30 * .90 # 3.12E.+14* 1.32E.+11# 1.59E.+09# 6.68E.+05* 3.85E12# # 24 # 67.53 * 1.00 # 2.52E.+14* 1.25E.+11# 1.43E.+06# 5.67E.+05* 8.85E12# # 25 # 74.37 * 1.10 # 1.89E.+14* 1.20E.+11# 1.24E.+08# 4.44E05* 8.85E12#	_				
# 19 # 41.89 * .62 # 3.80E+14* 1.65E+11# 1.75E+05# 6.47E < 05* 8.85E-12# # 20 # 46.03 * .68 # 4.00E+14* 1.56E+11# 1.80E+08# 7.23E < 05* 8.85E-12# # 50.60 * 75 # 3.43E+14* 1.47E < 11# 1.70E+08# 7.52E < 05* 8.85E-12# # 22 # 55.67 * .92 # 3.51E+14* 1.39E+11# 1.71E+08# 7.32E < 05* 8.85E-12# # 23 # 61.30 * .90 # 3.12E+14* 1.32E+11# 1.59E+09# 6.6dE < 05* 3.85E-12# # 24 # 67.53 * 1.00 # 2.52E + 14* 1.25E + 11# 1.43E + 06# 5.67E < 05* 8.85E-12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E + 11# 1.24E + 08# 4.44E < 05* 8.85E-12#		• • • • • • • • • • • • • • • • • • • •			
# 20 # 46.03 # .68 # 4.005+14* 1.566+11# 1.80E+08# 7.23E=05* 8.85E=12# # 21 # 50.60 * 75 # 3.43E+14* 1.47E+11# 1.70E+08# 7.52E=05* 8.45E=12# # 22 # 55.67 * .92 # 3.51E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.30 * .90 # 3.12E+14* 1.32E+11# 1.59E+09# 6.68E=05* 3.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 8.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#		· · · · · · · · · · · · · · · ·			
# 21 # 50.60 * 75 # 3.43E+14* 1.47E+11# 1.73E+03# 7.52E=05* 8.45E=12# # 22 # 55.67 * .82 # 3.51E+14* 1.39E+11# 1.71E+08# 7.32E=05* 8.85E=12# # 23 # 61.30 * .93 # 3.12E+14* 1.32E+11# 1.59E+09# 6.68E=05* 3.85E=12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E=05* 8.85E=12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E=05* 8.85E=12#	_	· — · · · · · · · · · · · · · · · · · ·			
# 22 # 55.67 * .82 # 3.51E+14* 1.39E+11# 1.71E+08# 7.32E*05* 8.85E-12# # 23 # 61.30 * .93 # 3.12E+14* 1.32E+11# 1.59E+09# 6.6dE*05* 3.85E-12# # 24 # 67.53 * 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E*05* d.85E-12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E*05* 8.85E-12#					
# 23 # 61.30 # .90 # 3.12E+14* 1.32E+11* 1.59E+09# 6.6dE+05* 3.85E-12# # 20 # 67.53 # 1.00 # 2.52E+14* 1.25E+11# 1.43E+00# 5.67E+05* d.85E-12# # 25 # 74.37 # 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E+05* 8.95E-12#					
# 20 # 67.53 # 1.00 # 2.52E+14* 1.25E+11# 1.43E+06# 5.67E+05* 0.85E-12# # 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E-05* 8.85E-12#					
# 25 # 74.37 * 1.10 # 1.89E+14* 1.20E+11# 1.24E+08# 4.44E-05* 8.85E-12#					
	. –				
# 26 # M1.79 # 1.21 # 1.50E#12# 1.16E#11# 1.82E#4## 5.16E#49# A.60E#12#	# 26 #	61.79 + 1.21		# 1.02E+0## 3.16E=05# 8.85E-12	
# 27 # 89.69 # 1.32 # 7.848+13* 1.13E+11# 7.95E+07# 1.96E-05* 8.85E-12#					
# 28 # 97.95 # 1.45 # 3.505+13* 1.10E+11# 5.59E+07# 9.18E-66* 3.85E-12#			· · · · · · · · · · · · · · · · · · ·		
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MAXIMUM CUNCUCTIVITY # 1.098+02 (MHOS/M)

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# 1	FOINT19				RACILS		POCK		-	RE		_				#	FREQUE	
#	4.55	#	1.4	+ 31	E-02	# 5	PCSI	TIO	1 1						/ S)		2.516	
#	(M)	#	((4))	# £	FFS	SURE	1	0.	8 32	(A	THO)SPH	ERES	; #	(H2	<u>(</u>) #
# 1		#	********	= :	========	= = =	====	# # # # ;	===	::==	===	= ==	==:	====	===:	*	********	
#			RELATIVE			_		-							SMA		SIGMA *	EPSILON #
#	INDEX	#	RACIUS	*	RACIUS										_		•	
		#		•	(F)		(1	/M31	•	, (1/5)	#	(1/	S)	#	(MHC/M; *	(FD/M) #
=:		= :		= = :		==:						- 4 4	===		C.O.	= :		
7	1	7	0.00	_	0.00												8.32E-03*	8.82E-12#
7	2 3	#	1.74 3.43	*	•03 •05	-	7.3	• • •	_			+11			E+0:		3.43E-03+ 8.72E-03+	8.82E-12#
I	4	•	5.25	#	•04		7.9				–	+11			_		9.12E-03+	8.82E-12#
7		*	7.04		_		6.1		_					- • • •			9.398-034	
7	5 5		3.87	-	•13		7.7									•	8.93E-03+	8.925-12#
7	7	# #	10.74		. 16	-		DE+:									7.86E-33+	· · ·
7	8	#	12.67		.19	7		5E+1	_			+11			-	_	4.15E-03*	
7	o y	#	14.6F	*	.22	#	1.4					+11			F + 0 -		1.75E-03*	d.85E-12#
-	10	-	16.73	*	• 25	-		7E+:									5.73E-04	8.35E+12#
-	11	-	13.89	#	.28	#	1.3								E+0		1.61E-04*	
-	12	-	21.15	4	.31		3.4		_			+11					4 · 32E - 05*	8.35E-12#
7	13	7	23.53		•35		9.7		_	_		+11			E+0		1.266-05*	8.85E-12#
7	14	*	26.05		.39	7											5.26F-06*	
7	15	-	21.73	*	•42	7	3.7								E+07		5.15E-06*	
ā	15		31.59	*	•47			4E+	-			+11		-	E+1		1.645-05*	3.85E-12#
-	17	•	34.67	+	•51			46+	_			+11			E+0			8-855-124
ä	19	ž	37.59	#	•56	ï	2.4					+11			E+0		3.64E-05+	8.85E-12#
ï	13	*	41.50	•	.61		2.8					+11					4.758-35+	8.858-124
	20	#	45.54	•	.67	#		0E+	_			+11				-	5.45E-05*	6.35E-12#
	21	#	49.87		.74	#		6E+				+11					5.87E-35*	8.85E-12#
	22	#	54.61		.81	#		4E+	- '			+11	-		-		5.96E-35*	8.85E-12#
	23	#	53.84	#	• B e.	#		5E+				+11		1.49	E+0	4 #	5.72E-05*	8.85E-126
#	24	#	65.66	•	.97	#	2.3	7E+	144	١.	SJE	+11	# 1	1.39	E+0	9#	5.16E-95*	8.45E-12#
	25	#	72.02	#	1.05	#	1.9	2E+	144	1.	2 4E	+11	# :	1.24	E+0	3#	4.37E-05#	8.45E-12#
#	25	#	73.93	+	1.16	#	1.4	5E+	44	. 1.	1 95	+11			E+0		3.45F-35*	8.95=-12#
#	27	#	66.37	*	1.27	#	1.6	1E+	144	1.	155	+11	# 3	9.02	E+0	7 #	2.46E-05*	9.55E-12#
#	28	#	94.24	*	1.39	#	6.2	DE+:	1 34	1.	1 36	+11		7.07	E+0	7#	1.556-05*	8.855-12#
#	23	#	102.45	*	1.51	#	2.9	2E+:	1.34	1.	100	+11	# /	4.95	E+0	7#	7.45E-06+	8.355-124
#	30	#	110.39	#	1.64	#	4.1	9E+:	12	1.	0 3E	+11	# :	1.94	E+0	7#	1.09E+05#	8.85E-124
=:		=	=======	= .		==:	====	===	= = :	====	===	::::	==:	===:	====	= =		========

MAXIMUM CONDUCTIVITY # 9.39E-03 (MHG5/M)

=	22222	: 3	2222222	# E :		==:	====	====	:::	===	2 = =	===	===	= 3	==:	= = = :	===:	====		= =	z z z		1 # Z
	POINTE) #	NOZZL	E	RACIUS	#1	ROCK	ET	:	₹E	DEY	E					•	F	RELI	IJĘ	NCY	,	#
	4.85	#	1.	49	S-0S	#	F051	TION	1 1	53	00(FT)	/10	(F	T/	S) 1	į.		2.5	OΕ	+08	1	•
	(H)			(M))	# (PRES	SURE	: 8	0.	8 32	(A	THO	SF	HE	ES	•		(+	HΖ	ţ.		#
I	======	: =	========	==:	. 4 2 2 2 3 2 2	==	====	===:	: 2 2	= 4 =	= ==	===	#==	==	==:	I	===	= = = :	:222:	E E	z = x	===	# # #
	RADIA	.ŧ	RELATIV	E+	ABSCLUT	E#									_	MA I		4 D I 2	14	p.	EPS	ILO	N #
	INDEX	#	RACIUS	*	RACIUS	#	DEN	SITY	*	FRE	GNE	NCY	#FR	EG	IUE	NCY	į.		•	•			#
#	1	#		•	(4)	#	(1	/M31	*	• (1/5)	#	(1	./S) (# (1	MHC/	/H) '		(F	C/M	*
=	:======:	:	=======	==:	******	==:	====	===:	:==	===	= ==	332	## I	==	==:	= = = ;	===	#221	222	= = -	# = =	# # # # # # # # # # # # # # # # # # #	222
#	1	#	0.00	•	0.00		7.2											-					_
	2	#	1.77		•03		7.3															2E-	
	3	*	3.55	*	•05		7.3						_						-03			2E-:	
	4		5.34	*	.08		7.2												-03			2E-	
1	5	#	7.16	#	•11		6.8	-		_		+11							-03			2E-	
-	6	#	9.01	*	•13 •16		5.7			-				_		- 6 a .			-03' -03'		_	3E	
7	8	7	10.91 12.85	_	.19		2.0												E-03			4E=	
7	9	#	_		.22		8.1						-			+ 0 a:	_		-34			5E-	
	10	ø			.25		2.7					+11	-			+03			-04		-	5E-	
-	11		13.34		.28		8.1						-			+03		-	-04			5E-	
7	12	4	21.37		.32		2.3						_				_		-05°			5E-	
7	13			-	.35		7.2		-	_	_							-	E-06			5E-	
-	14			*	.39	4		5E +1								+07	_		-06			5E-	
-	15		:	+	.43		2.3									+07			-06			5E-	
4	16			#	.47	#		5E+1				+11	-			+07			-05			5E-	
•	17		1.7.1	#	.51		1.4						-			+08	_		-05			5E-	
i	18	#	37.95	*	.56		1.3		-							+ 0 ĉ			-05			5E-	-
4	19	#	41.44	#	.61	#	2.2	3F +1	44	1.	7 2E	+11	# 1		HE.	+09	# 3	. 65	-05	¥	6.6	5E-	12#
	20	#	45.22	#	.67		2.4	76 +1	44	1.	646	+11	# 1	. 4	1E	+ 13 15	# 4	.25	E-05	*	8.8	SE-	12#
4	21	#	49.35	*	.73	#	2.5	75 +1	44	1.	55E	+41	# 1		4E	+00	# 4	.676	-05	#	8.6	35E-	12#
#	22	#	53.86	#	.79	#	2.5	5E+1	44	1.	47E	+11	# 1	. 4	3t.	+C i	4	.876	-15	•	8.6	5E-	12#
4	23	ű	55.41	#	.87	#	2.4	9E+1	4+	1.	4 JE	+11	# 1	l • :	39E	+ 8 8	# 4	. 836	E-05	#	8.4	15E-	12#
4	24	8	64.24	#	•35	#	2.1	6E +1	4*	1.	3 SE	+11	.# 1	. 3	SE.	+ 0 8	# 4	• 55 (E-05	•	8.8	15E-	12#
4	25	#	70.19	#	1.04	#	1.3	4E+1	4	1.	2 9E	+11	.# 1	l • č	SSE.	+08	F 4	. 066	-05	*	8.4	15E-	12#
4	25	#	76.58	#	1.13	#	1.4	<u> 45</u> +1	4*			+11	_			+08			-15			5E-	
4	27	#		*	1.23	#	1.1	2E +1	4*			+11		-					-05			SE-	
4	24	Ħ	91.15	*	1.34	#	7.3			_									-05		-	SE-	
4	23	#	93.01	#	1.46	#		7E+1		_			_		-		_		-05			SE-	
4	30	#		#	1.54	#		0E.+1					_			-			- \$6		-	15E-	
4	31	#	115.52	7	1.70	#	りょり	2E +1	24	1.	0 3E	+11	.# 2	2 • 3	1E	+07	* 1	.718	-06	•	3.5	15E-	154
=	:2:5522	2 2	*****	:==:	======	==	2 2 2 2	322:	:::	::::	===	:===	::::	: = :	22:	= = = :	2 2 2	222:	====	= =	322	222	2 2 2

MAXIMUM CONCUCTIVITY # 8.43E-03 (MHOSZM)

=		==		= = = =	======	= = :	===	22:	===	# # ,#		====		* *			********
	POINT2	1*	N072	Lii P	ACILS	# 2	oc	KE1	7	1	๊	DEV	Έ			FREQU	ENCY #
#	5.17	#	1	. 489	-92	61	05	ITI	LON	t	50	100	FT)	/1	O(FT/S)	2.50	E+08 #
	(H)	#		(H)		#1	PRE	SSU	JřE		0.	532	. (A	TM	OSPHERES) (H	Z) #
z	======	= =	======	====	222222	= = :	= =	Z = :	::::	= = =	33	= = =	322	==	*******	********	
	RADIA	L#	PELATI	VE#	AESCLUT	E#	EL	ECI	140	N# C	OL	L 15	ION	#	PLASKA	# SIGMA *	EPSILON #
	INDEX	#	RACIU	5 *	FACIUS		Ct	451	TY	4 5	RE	QUE	NCY	#F	REQUENCY		
					(M)	#	(1/1	13)	. #	(1/5	;)	#	(1/5)	# (MHO/M) #	(FD/H) #
=	======	I Z	======	3335	=======	= = :	* = #	22:	===	: : :	: 2 :	===	***	E 2	******		********
	1		0.00		0.00	#	6.	626	+10	€*	2.	456	+11		2.31E+09	7.61E-03+	4.92E-12#
	2		1.30	4	.03		6.	5 7 F	+11	6*	2.	4 56	+11		2.30E+09	# 7.56E-93*	8.82E-12#
#	3	#	3.61	4	.95	#	6.	376	-1	5#	2.	45E	÷11		2.27E+09	# 7.34E-33*	5.92E-12#
	4	#	5.43	*	.09	#	5.	916	+11	6*	2.	446	+11		2.16E+03	6.825-03+	9.83E-12#
	5	#	7.27	•	.11		5.	U 4E	+1	6#	2.	438	+11		2.01E+09	# 5.64E-03+	8.35E-12#
	6	#	9.15	*	•13	#	3.	738	+10	6#	2.	4 25	+11	ø	1.736+09	# 4.345-03#	5.54E-12#
	7	#	11.07	#	.16		2.	278	E+1(6#	2.	4 98	+11		1.35E+09	# 2.66E-03+	5.84E-12#
#	5	*	13.54	*	.19	#	1.	116	+10	6	2.	3 86	+11	#	9.47E+88	# 1.32E-03+	8.35E-12#
#	4	#	15.06	4	•55	#	4.	526	+15	5#	Ž.	356	+11		6.03E+0#	# 5.41E-04#	4.55E-12#
#	10		17.15	*	•25	#	1.	5 98	+1	5+	2.	325	+11	#	3.586+93	# 1.94E-04#	8.855-12#
	11		19.32	#	.29	#	5.	176	+14	4#	2.	2 86	+11		2.045+38	# 6.4úE-05#	€.85F-124
#	12	#	21.59	•	•32		1.	645	+14	4	2.	2 SE	+11	#	1.15E+05	# 2.07E-J5+	8.95E-12#
	13		23.95	*	.35		5.	526	+1	3#	2.	178	+11		6.67E+07	7.15E-06*	3.856-12#
	14	#	25.44	#	•39	*	2.	43E	+1	3*	2.	115	+11	#	4.43E+07	# 3.24F-36*	8.358-12#
#	15	#	24.06	*	.43	#	2.	278	+1	3#	2.	, Q 5E	+11	. #	4.28E+G7	# 3.12E-36+	6.85E-12#
#	16	#	31.34	#	.47	#	6.	866	+1	37	1.	906	+11	#	7.448+37	# 9.78E-06+	8.856-12#
	17	#	34.96	•	•51		1.	126	+1	4#	1.	305	+11		9.485+07	# 1.65E-05*	9.956-12#
	14		37.96	4	•56	#	1.	4 9 E	+14	47	1.	328	+11	#	1.10E+G5	# 2.31E-05#	8.95E-12#
#	19	#	41.56	•	- 51		1.	306	+1	4*	1.	7 4E	+11	#	1.20E+09	# 2.9GE-85+	8. 956-12#
	20	#	45.02	*	•66	#	2.	3 26	+1	4*	1.	665	+11		1.27E+05	# 3.41E-05*	8.35E-12#
	21	Ħ	49.00	*	•72	#	2.	148	E+14	, *	1.	5 5€	+11	#	1.31E+08	# 3.80E-05+	8.55E-12#
	22	#	55.31	4	.79	#	2.	168	41	4#	_			_		# 4.04E-35*	
	2.3	#	53.12	#	. 36				+1							# 4.10F-05#	
	24	#	63.17	4	.93	#	1.	436	+14	4 -						# 3.9HE-05+	
#	25	#		*	1.01	#			41	-				-		# 3.68E-05#	
	26	#	74.90	*	1.10	#	1.	445	>1	4=	1.	. S 6F	+11	. #	1.056+03	# 3.245-05*	0.95E-12#
#	27	#	91.52	•	1.20				+1	-	_				· · · · •	# 2.69E-05+	
	23	#	43.61	*	1.31	#	6.	7 25	+1		_	_		_		# 2.07E-954	·
	53	#	76.14	*	1.42	#	6.	1 3	+1		_	-				# 1.50E-35#	
#	30	#	144.00	•	1.53	#	5.	300	+1.	j=	1.	125	+1:		5.545+97	# 9.575-36*	5.95E-12#
#	31	#	112.13	*	1.65		1.	90H	+1.	3*	1 .	1 JE	+11	#	3.92E+37	# 4.87E-06*	5.35E-12A
	32	#	122.41	*	1.79	ø	5.	315	+1	5=	1.	0 3 t	+11		2.16E+07	# 1.50E-36+	J. 95E-12#
Ŧ	=====	==	======	= = = =		==	===	Z = :	= = = :	===	= 3	122	===	# # F		*****	********

MAXIMUM CONDUCTIVITY & 7.618-65 (MHUSZM)

#	****	= =	*****			32:			######	3 2 3 2	********	********	********
	POINTE	-		.E +	RACILS	# 1	FOCKET		PEDEY	Ε	•	FREGU	ENCY #
#	5.47	*	1.	438	E-02						10(FT/S) #		E+05 #
	(M)	#		(i4))	#1	PRESSUPE	1	0.932	(AT	MOSPHERESF	(H)	Z) #
8	*****	33	3222222	1321	******	==:	*******	2	****	2 2 E E	*******	*********	********
							ELECTADE						EPSILON #
•	INDEX	#	RACIUS	•	RACIUS	#	DENSITY	+F			FREQUENCY#	•	*
•		*		•	(F)	•	(1/H3)	•	(1/5) #	(1/5)	(MHG/H) +	(FD/H) #
=		==	24121	333		3.2 :	******	# # #	2122	===	*******	***********	********
	1		0.00	•	0.00							6.05E-03+	
•	2	#		•	• 0 3							5.93E-034	
	3	#	3.66	*	.05							5.53L-03*	• - •
	4	#	5.51	•	• 6 9							4.80E-33*	
	5		7.39	#	•11							3.76E-03*	
	6		9.29	•	•14							2.35E-03+	
	7		11.23	•	.17							1.46E-33*	
	8	*	13.22		.19							7.11E-34+	
	9		15.26	*	•23							3.00E-044	
	18		17.36	•	.26			-				1.15E-34*	
	11		13.54	•	•29							4-13E-05+	
	12	#		•	.32							1.47E-05+	
	13	*		•	•36							5.51E-06+	
	14			•	•39			_				2.63E-06*	
	15			•	.43							2.56E-06*	
	15				.47							7.96F-06*	
	17		_ ,,,,	*	•52			-				1.36E-05+	
	19		34.03	*	•56							1.68E-05+	
	13		41.35		.61							2.37E-05*	
	20	F	44.91	*	•66							2.00E-05	
7	21	7	48.76	*	.72							3.15E-05+	
#	23 23	#		*	.75							3.39E-054	
-	23 24	*			.85 .92							3.50E+05+	
*	25	4	67.67	*	1.00				_	-	_	3,47E-05+ 5.305-05+	
77	25							-					
7	27	-	73.47 79.75		1.03 1.18							3.015-05*	
	23	دم عم	55.50		1.25		1.15F+1					2.61E-05+	8.65E-12# 8.65E-12#
#	29	-	43.68	•	1.38		6.85E+1	-				1.66E-05+	
4	311	*	141.25	#	1.49	-	4.79E+1					1.00E-05+	
*	31		101.25		1.61	#	2.386+1					7.525-36*	
g.	31		117.23		1.75							3.61E-06*	
*	33	<i>"</i>	125.45		1.95			-				1.156-06*	
**	J; =====	==		===:		==		_				. T.T.E 10.	

MAXIMUM GUNEUCTIVITY # 6.05E-03 (MHOS/M)

# :		: 2 :	= = = = = = = = =	= = :		==:	====	==		: 3 =	, R = 3	22	3 Z Z Z	===	====	====		
# 1	POINT23		NOZZL	E F	ACILS	#	FUCH	ET		ŧ	RED	EY	Ε				FREGU	ENCY #
#	5.78	#	1.0	485	20-2	#	POSI	ITI	NC	ŧ	500	0 (FT)	/10	(FT/	S) (2.51	E+08 #
	(H)	#		(4))		_					-			SPHE		•	Z) #
	*****	: = :		3 2 3				28					323			222		*******
	RADIAL		RELATIV	-	ASSCLUT	F#	FLE	CT	201	.+ 0	OLL	ıs	ION		PLAS	M A #	SIGMA .	EPSILON #
	INDEX		RACIUS															4
•	•1152	ī			(۲)	-			3)			/S					(MHC/M) *	(FD/H) ¢
*			* = = = = = = =	= = 1		* 2 2 :			-				•				. (1400)41	7 (11(07)
•	1		0.00		0.00		2.	36									4.11E-03*	9.94E-120
-	Ş	ĭ	1.86		.03		_							_		_	3.97E-034	
7	3	Z	3.72		• 45												3.57E-03*	
7	-	•			-													
	4	-	5.60	*	.06						-			_		-	2.935-034	
	5	•	7.50	*	•11						-			_			2.165-03+	
	6		9.42		•14								_				1.396-03+	
	7	#	11.39	*	.17							-				_	7.80E-04*	
	3	#	13.39	#	.20						_						3.84E-04+	
	9	#	15.45	#	.23	#	1.4	OE	+15	•	2.3	SE	+11	F 3	. 36E	+09#	1.70E-04*	8.85E-12#
#	10	#	17.57	•	.26	#	5.6	6E	+14	•	2.2	Æ	+11(# 2.	. 14E	+0 4#	6.97E-05+	e.35F-12#
	11	#	19.77	#	.29	#	2.1	. 6E	+14	•	2.2	Æ	+11(1 1.	. 32E	+ J 3,¢	. 2.725-35+	3.35E-12#
	12	#	22.34	*	.33	#	0 . 3	4E	+13	•	2.2	1E	+11(₽ 8.	. 1 5E	+07#	1.U5F-05*	9.95E-12#
#	13	#	24.40	•	.36	#	3 . 2	36	+13	5 *	2.1	6E	+114	¥ 5.	. 10E	+ 47#	4.21E-06*	9.858-12#
#	14		25.88	*	.40		1.4	6E	+13	5#	2.1	ĮΕ	+11(1 3	. 43E	+37#	1.95E-064	3.858-12#
	15		23.47		.43	#	9.7	2E	+12	2#	2.0	эE	+11	# 2.	. BOE	+07#	1.34E-36*	3.45E-12#
#	15		32.20	•	.47	#	1.3	SE	+13	5*	1.9	ЭE	+114	# 3.	. 30E	+97#	1.92E-06*	8.85E-12#
	17	#	35.08		•52		5 .	JUE	+13	5#	1.9	ŚΕ	+11	# 6.	. 54E	+07#	7.78E-06+	8.85E-12#
	19		39.14		•56		8.	35	+13	5#	1.5	5E	+11	8 8	. 44E	+07#	1.355-05+	8.85E-12#
	19		41.39	•	.61		1.1										1.86E-35*	
	20		44.76	*	•65		1.	_									2.295-05+	
	21	#	45.01	*	.72		1.		_		_	_		_			2.636-05+	
	22	ä	52.64	•	.78		1.5		_		-		_	_			2.67E-05*	-
	23		56.33	•	.84		1.6	-			_			_			3.01E-05#	
Ā	24		61.76	-	. 71		1.9	-	-				-				3.04E-35+	
Ä	25	•	55.00		.99		1.		_					-			2.95F-05+	
-	26	ï	72.34		1.07		1.2		_			-		_			2.76L-05*	
-	27	-	73.32		1.15		1.1				-					-	2.47E-05*	
7	23	-	34.75		1.25		9.		_								2.12E-05*	
-		#	34.73		1.35				_							-		
-	53	Ŧ			1.45		7		_							-	1.72E-15*	
7	30	-	33.90				5.	-									1.325-05*	
#	31	₹.	100.51	-	1.57		3 - 7										3.36E-06*	
	32		114.39	*	1.53		2.		_								5.905-06*	
#	3,5	#	122.47	-	1.81		1 •		_								2.89E-06*	
	34	#	130.67	*	1.93	#	2.4	12t	• 1.3	•	1.0	9Ē	+11	1	. 40E	+37#	5.38E-07*	d.85E-12#
=	***===:	3	======	==:	=======	==	= = = :	===	==:	= = 1	===	23	3 3 2 E	===	2 2 2 2	====	:::::::::::::::::::::::::::::::::::::::	22222222

MAXIMUM CONCUCTIVITY # 4.11E-03 (MHOS/M)

1		= =	=======	222	*******	== :		Z Z Z			3 = =		*****	********
1	POINT2	4#	HOZZL	ER	ACILS	45	OCKET	t	REDI	EYE			FRECU	ENCY #
- (6.09	#	1.	48E	-02	# 5	POSITIO	N I	5000	(FT	1/1	0(FT/S) #	2.50	E+08 #
-	(H)	#		(M)		# 5	PRESSUR	E ŧ	0 . 4	32 (ATP	OSPHEFES#	(4)	Z) 🖠
:		= #	*****	3 2 2	2522223	E E :		2 2 2	1 2 2 2 :	* * *	Z Z Z	********	******	**::::::
(RADIA	L#	RELATIV	E#	ABSCLUTE	#	ELECTR	44C	COLL	1510	N#	PLASMA #	SIGMA +	EPSILON #
1	INDEX	#	RACIUS	#	RACIUS	#	CENSIT	Y *	FREQ	JE NC	Y#F	REQUENCY#	•	•
- ()	#		•	(4)	#	(1/H3	, *		/ S)		(1/5)		(FD/H) ●
1	******	3 4	*****	222				2 3 £		12 22				*******
1	1		0.00	•	0.00			_			_		2.42E-03+	8.54E-12#
•	, 5	#	1.59	#	.03			_	-		-		2.32E-03+	
•	3	#	3,.77	*	•06			-			_		2.04E-03*	
1	4		5.66	*	.09			_			_		1.62E-03#	
- 1	5	*	7.60	•	•11		9.77E+				_		1.15E-03+	
- (6		9.55	•	.14						_		7.33E-04#	
1	7			•	•17				_		_		4.15E-04+	
•	8			*	.20			-			_		2.12E-04#	
•	9		15.65	*	.23						_		9-905-05+	
1	10	#		#	• 26			-		_	_		4.35E-05*	
•	11	#		•	•29		1.46E+	_			-		1.84E-05+	
1	12	#		*	. 33						_		7.63F-J6+	
•	1.5	*			•36		2.43E+				-		3.25E-06*	
•	14	*		*	• 40		1.16E+	_			_	3.06E+07#		
•	15			4	.44						_		1.05E-06*	-
1	15			*	. 4 9			-			_	2.89E+07#		
1	17	#		•	•52			_			_		5.93E-06*	
•	14			-	•56								1.04E-05#	
1	19	#		#	.61						_	8.65E+07#		
1	20			*	•66		1.130+						1.85E-05+	
	21	*		₽	•72								2.17E-05*	
- 1	22	#			.77								2.42E-15+ 2.58E-05+	
	23	#			.64 .30			- •			_		2.66E-05*	• • • • •
	25	*		•	.98		1.37E+				_		2.63E-05*	
7	26				1.05			_			-		2.518-05+	-
	27	ï			1.14		_ , _ ,						2.31E-05*	8.85E-12#
	, 24 , 24	-	33.31		1.23						-		2.04E-05*	
1	2 2			•	1.33		7.396+	-			_		1.73E-05*	
	30			•	1.43						_		1.39E-05+	
1	31	ï		•	1.54								1.055-05*	
1	32	ï		•	1.65						-		7.41E-06*	
1	33	i		*	1.77		1.835						4.64E-06-	
1	34		127.83	•	1.89		5.55E+					2.63E+07#		_
	. , , , , , , , , , , , , , , , , , , ,	- -		: 2 = 5	 :===:==:	- 32:					_		*******	
					- - ·					_		_		

MAXIMUM CONCUCTIVITY # 2.42E-03 (MHOS/M)

*		=	2223232	33		==			= = = = =	***	=======================================		22222
	POINTES		いことフレ	E f	ACILS	#1	FOCKET	ŧ	REDEY	Ε		FREGUENCY	
	6.39	#	1.	48	20-		FOSITION	1	50000	FT1/	10(F7/S) #	2.50E+08	•
	(M)			(M))		PRESSURE	1	0.832	(AT	MOSPHERES	(HZ)	
=	******	: 3		= = :		: #	*******		3	3222			SEEEE
#	FADIAL		RELATIV	==	ASSCLUT	E#	ELECTPOI	N# C	OLLIS	ION#	PLASMA #	SIGMA + EPSI	LON #
	INDEX		RACIUS	-		_		-			FREQUENCY		
					(*)	ě	(17M5)		(1/5			(MHC/M) + (F3	/H) #
	*****	: 32		1 2 :		**	*******		######################################		3832232323		2222
	1		3.30	#	6.00	4	1.10F+16		2.39	-112	3.42F+08#	1.30E-03+ 5.55	F-12#
•	2	ì	1.31		.03			_				1.24E-03* 3.35	-
-	3	-	3.83		•06			-			=		E-12#
Ĭ	ú	-	5.76		.08								E-12#
-	5	-	7.71		-							6.03E-04+ 3.85	
7	. 6	Ξ	7.68		•11		_						E-12+
7	7	7		_		ł						2.258-04# 8.39	-
-		*	11.69	_	.17								
	•	₩.	13.74	*	.50							1.20E-04# 8.85	
	9		15.84	#	.23						1.97E+03#		
	10		17.99	*	.27							2.79E-15# 8.99	-
	11	#	20.21	•	.30								E-12#
8	12	#	22.50	*	.33								-12#
•	13	#	24.87	•	.37						3.95£+07#		E-12#
	14	#	27.34		• 4 4			_			2.76E+07#		E-12#
	15	#	83.45	•	. 44						2.25E+U7#		E-12#
#	16	*	32.61	#	. 4 8			_			2.62E+07#		E-12#
	17	#	35.45	*	•52						5.16E+07#		E-12#
#	1 3		33.44	*	.57	•	5.61t+1	3 *	1.05E	+11#	6.725+07#	*.45E-JE+ 6.89	E-12#
	19		41.60	*	. 61	#	7.67E+1	3*	1.30E	+11#	7.86E+07#	1.20E-354 8.49	E-12#
	នរា	#	44.95	*	• 66		9.415+1	3*	1.73E	+11#	8.71E+87#		E-12#
#	21		48.53	#	.72	#	1.08E+1	4#	1.67E	+11#	9.31E+07#	1.52E-05* 4.35	E-12#
	22		52.35		.77		1.175+14	4	1.6JE	+11#	9.722+07#	2.05E-05* 4.85	E-12#
	23		50.45	•	- 63	#	,21E+1	4 *	1.54E	+11#	9.436+07#	2.22E-054 5.45	F-12#
	24		60.15	•	• 90		1.216+1	4.	1 . 4 SE	+11#	9.39E+07#	2.32F-05# 4.85	E-12#
	25	#	65.59	*	• 37	#	1.18E+1	4*	1.42E	+11#	9.73E+07#	2.34E-05* 8.85	E-12#
	25	#	70.76	•	1.04		1.180+1	4#	1.365	+11#	9.42E+07#	2.2cE-054 6.65	E-12#
	27	#	75.25	*	1.12		9.465+1	5*	1.31E	+11#	8.96E+37#	2.142-054 9.95	F-12#
	2 }		11.56	•	1.21		8.72E+1	5*	1.27E	+11#	8.58E+U7#	1.94E-754 8.85	E-12#
	24		49.43		1.30		7.36E+1	3*	1 . 2 3E	+11#	7.70E+07#	1.695-35* 0.99	*51-3
	39		35.16	•	1.40		-					1.41F-05" 8.85	E-12#
	31		162.27	•	1.51		4.64E+1	3#	1.16E	+11#	6.11E+07#	1.12E-05* 8.89	E-12#
	32		139.73	#	1.62								E-12#
	33	ï	117.39		1.75			-				5.87E-06* 4.35	E-12#
	34		125.2c		1.85								E-12#
	35		133.25	•	1.97			-					E-12#
=	*****	: =	=======	E 3		E 3	=======================================	-	2222	2223	********		

MAXIMUM CONGUSTIVITY # 1.80E-03 (MHGS/M)

*	=====		******	= 3 1		3 2 E	===	2222	2 2 2			****	*****	********	********
	POINTE	5#	NUZZL	E A	ACILS	# 5	ROCK	ΕT		REDE	YE		(FREGU	ENCY #
	6.70		_	_	-02	#1	120°	TICH		5000	(FT)	/10 (F	T/S) (2.50	+03
	(M)			(M)			FES	SURE		0.63	2 (A	THOSE	HERESI) (H	Z) #
	222223	= = :		323		==:		2222	2 2 1	2222	3322	Z 2 2 2 2	*****		******
	RADIA	. #	RELATIV	E*	ASSCLUT	E#	ELE	CTPO	.+(COLLI	SION	. PL	ASMA (SIGNA *	EPSILON #
ě	INDEX	_	FACIUS	-	RACIUS							_	_		
•	•			*	(M)		_	/H3 A		(1/			/S) ((F0/H) #
	233323	3 28 3		323		231	***	****	*=:		* * * *			********	********
	1		0.00	-	0.00		5.6	SF+1	5#	2.37	E+11	6.7	'5E+051	6.72E-04*	8.85E-12#
	2		1.94		•03	•							9E+086		6.85E-12#
ä	3		3.36		•06			£E +1						5.57E-04*	8.85E=12#
i	ú	•	5.34		.09	-							5E+08		8-85E-12#
4	5	-	7.31	*	•12	4		4E+1			_	-	1E+09		8.85E-12#
Ĭ	6	ï	3.51		.14			2E+1					3E+06		3.45E-12#
-	7	Ä	11.54	•	•17		_	3E+1					34E+08		8.85E-12#
-	8	-	13.91	•	.21			1E+1						7.015-05*	8.85E-12#
-	9	Ξ	16.03	•	.24			7E+1					55E+031		8.85E-12#
-	10	-	19.20		.27			60+1		2.24			196 +031		3.55E-12#
-		-	20.43		.30			5E+1					AE+07		8.35E-12#
-	11 12	ï	22.73		.34				_					4.18E-06*	
7	13	-		-	.37			16+1	-				9E+U7		8.85E-12#
-		*	25.11						-	_					
	14	-	27.56	•	• 41			4E+1	_				50E+07(3.55E-12#
•	15	•	30.15	*	.44			9F.+1	_				-	7.32E-074	9.852-12#
	16		32.84	*	•48			6E+1	_				0E+07		8.85E-12#
*	17	•	35.66	-	•53			9E+1					736+071		8.95E-12#
	18		38.62	#	.57			3E+1	-			_	-	7.13E-06*	3.85E-12#
	19		41.75	#	•62			9E+1	-				35+07		8.35E-12#
•	53		45.05	*	•66			15+1					14E+G7(8.85E-12#
	15		48.57	•	.72			3E+1						1.55E-05*	8.35E-12#
•	22		52.31	*	•77			1E+1	-				3E+07		8.85E-12#
•	23		56.31	*	.83	•		6E+1					6E+07		8.35E-12#
	24		60.59	*	• 9 •	7		8E+1		-		-	S2E+074		9.85E-12#
	25		65.18	•	• 36	#		6E.+1					24E+071		8-85E-12#
•	25		70.12	#	1.03			1E+1					1E+07		3.85E-12#
	27		75.42	•	1.11			1F+1	-	-			6E+07		8.85E-12#
	85		61.11	•	1.20				-				19E+071		8.856-12#
	24		a7.20		1.29			16+1					2£ + 07		8.85F-12#
	30	#	93.69		1.36	•		3E +1					37E+07		8.45F-12#
	31		103.55	*	1.48	#	-	5E+1	-				?5E+07(8.85E-12#
•	32		107.75	#	1.59			3E+1	-					9.10E-06*	8.85E-12#
	53	*	115.25	•	1.70			1E+1	-			- •	58E+07		8.35E-12#
•	54		122.97		1.81			46+1		_			35E+07		8.35E-12#
•	35		130.36		1.93	#		1E+1						2.84E-06*	9.35E-12#
	35	#	133.34	*	2.05	4	5.1	4E+1	2*				14E+07	1.32E-06+	8.455-12#
3	**=**=	= = :	# 2 2 2 2 2 2 2 2	==:	*****	T = :	===	====	* * :	: = : : :	2 2 2 2	****		*********	********

MAXIMUM CONSUCTIVITY : 6.72E-84 (MHGS/M)

#FOINT27	NOZZLE RACILS	#FOCKET # REDEVE # FREQUENCY	
# 7.00	1.43E-C2	#FOSITION : 5000(FT)/10(FT/S) # 2.50E+08	•
# (H) ((H)	#FRESSURE 1 0.832 (ATMOSPHERES# (HZ)	
*******	*************	:=====================================	
# RADIAL	FRELATIVE* ARSCLUTE	E# ELECTRON*COLLISION# PLASHA # SIGHA * EPSILU	A 4
# INDEX	HACIUS + RACIUS	# DENSITY *FREQUENCY#FREQUENCY# *	•
•	* (*)	# (1/M3) * (1/S) # (1/S) # (MHQ/M) * (FD/M	1) #
*******	***********	***********************************	: # 7 %
# 1 +	0.00 + 0.00	# 2.4GE+15* 2.35E+11# 4.34E+88# 3.48E-04* 8.85E-	.12#
# 2	1.95 * .03	# 2.78E+15* 2.35E+11# 4.73E+0## 3.33E-04* 6.85E-	.12#
# 3	3,93 * .06	# 2.42E+15* 2.35E+11# 4.42E+08# 2.91E-04* 8.85E-	.12#
# 4 :	5.92 * .09	# 1.930 +15* 2.34E +11# 3.95E+08# 2.33E-14* 8.85E-	120
# 5 (7.91 * .12	# 1.41F+15* 2.33E+11# 3.37E+08# 1.71E-64* 5.85F-	.120
# 6	<i>y</i> 9.94 * .15	# 9.49E+14* 2.32E+11# 2.77E+08# 1.15E-04* 8.85E-	-12#
. 7	11.59 * .18	# 5.90E+14* 2.30E+11# 2.18E+08# 7.23E-05* 8.85E-	-120
# 8	14.08 4 .21	# 3.43E+14# 2.23E+11# 1.66E+03# 4.24E-05* 8.35E-	.12#
9 9	16.22 * .24	# 1.88E+14* 2.26E+11# 1.23E+06# 2.34E-07* 8.85E-	-12#
# 10	1 19.40 + .27	# 9.78E+13* 2.23E+11# 8.38E+07# 1.24E-05* 8.85E-	-120
# 11	20.65 * .30	# 4.91E+13* 2.20E+11# 5.29E+07# 6.30E-06* 8.85E-	-124
• 12	22,96 * .34	# 2.41F+13+ 2.16E+11# 4.41E+07# 3.14E-06+ 8.85E-	-12#
# 13	25.35 + .37	# 1.19F+13+ 2.12E+11# 3.10E+07# 1.50E-06+ 8.85E-	-12#
# 14	27.82 4 .41	# E.3PF+12* 2.09E+11# 2.27E+07# 8.65F+07* 3.85E-	-12#
# 15	P 30.46 9 .45	# 4,46E+12# 2.03E+11# 1.90E+07# 6.22E+07# 8.85E<	-12#
# 15	# 33.G# + .49	# 6.11E+12# 1,98E+11# 2.22E+07# 8.70E+07# 8.85E+	-12#
# 17	/ 35,ee + .53	# 2.38E+13* 1.93E+11# 4.38E+07# 5.48E-06* 8.89E-	-124
# 13	1 34.62 + .57	# 4.65E+13* 1.67E+11# 5.72E+07# 6.11E-06* 3.45E-	-12#
# 19	62 * 56.14	# 5.5AE+13* 1.31E+11# 6.71E+07# 5.68E-06* 8.85E-	-12#
# 23	45.19 * .67	# 6.42F+13* 1.73E+11# 7.47E+07# 1.11E-05* 8.85E-	-12#
21	45.6472	# 8.02F +13# 1.69E+11# 8.04E+07# 1.335-05# 8.85E-	-
# 25	52,32 + .77	# #.84E+13* 1.63E+11# 4.44E+C7# 1.53E+05* 6.85E=	-12#
2 3	£ 55.23 * .A3	# 9.39F+13* 1.57E+11# 8.69E+07# 1.66E-05* 8.85E-	
# 24	60.41 4 .89	# 9.61++13* 1.51E+11# 8.8NE+07# 1.79E-05* 9.85E-	
# 25	₽ 64.87 ♥ .96	# 9.55L+13* 1.46E+11# 8.73E+U7# 1.85E-05* 8.85E*	
• 26	# 63.66 * 1. 03	# 9.22F +13* 1.40E +11# 3.62E + 07# 1.85E - 05* 8.85E -	
# 27	₽ 74.79 ₽ 1.10	# A.65E.+13* 1.35E+11# 8.35E+07# 1.80E-05* 9.85F-	
# 28	# 20.29 * 1.1A	# 7.88E+13* 1.31E+11# 7.97E+07# 1.70E-05* 8.55E-	_
# 29	# 85.17 * 1.27	# 6.47E+13* 1.26E+11# 7.50E+07# 1.55E-05* 8.85E-	
• 30	1 42.45 4 1.36	# 5.47E+13* 1.23E+11# 6.94E+07# 1.37E-05* 3.95E-	
# 31	× 43.06 ← 1.46	# 4.94F+13* 1.19E+11# 6.31E+07# 1.17F-05* 8.85F-	_
# 32	106.04 + 1.56	# 3.94E+13* 1.17E+11# 5.64E+07# 9.50E-06* 8.55E-	
# 33	111.33 + 1.67	# 3.005+13* 1.14E+11* 4.32E+07# 7.3PE-06* 8.85E-	
# 34	# 120.ee * 1.75	# 2.16E+13* 1.13E+11# 4.17E+07# 5.40E-Jo* 5.35E-	
	123.63 * 1.90	# 1.44F+13* 1.11E+11# 3.41E+07# 3.65E-06* 9.85E-	
	136.51 * 2.01	# 8.53E.+12* 1.1UE+11# 2.62E+07# 2.18E-06* 8.95E-	
	1 144.47 • 2.13	# 3.97E+12* 1.09E+11# 1.77E+07# 9.97E-07* 3.45E-	
******	22222222222222		2222

MAXIMUM CONDUCTIVITY # 3.45E-04 (MHOSZM)

==	*****		2222222		******	8 Z 2				===	2 2 Z	===	##			*************
# F	STRID	•	NOZZL	ER	AGILS	# 5	OCK	ET	ı	RE	DEY	Ε				FREQUENCY (
•	7.31		1.	4 BE	-02	# F	120	TION	1	50	80(FT)	/1	O (FT	/S)	# 2.50E+88 (
•	(H)			(M)		# 6	RES	SURE		0.	8 32	/A	TH	OS PH	ERES	9 (HZ) (
38	*****	2	******				***	***			===		==		***	**************
•	RADIA	. #	RELATIV	E+	AESOLUTI	E#	ELE	CTRO	N#	COL	LIS	ION	#	PLA	SHA	# SIGHA * EPSILON (
•	INDEX		RACIUS		RACIUS	•	DEN	SITY		FRE	QUE	NCY	#F	REQU	ENCY	• • •
٠					(M)		(1	/H3)		(1/5)	•	(1/	SI	# (MHO/M) * (FO/M) (
81	*****	8	******	***	******	321		***	==	===	22	782	==	***	***	************
	1	#	0.00	•	0.00		1.5	4E+1	5+	2.	3 3E	+11		3.52	E+08	# 1.26E-04# 3.85E-124
	2		1.99	•	.03		1.4	8E+1	5+	2.	3 3 E	+11		3.45	E+48	# 1.78E-844 8.85E-124
	3		3.93	•	.06		1.5	0E+1	5+	2.	3 3E	+11		3.24	E+08	0 1.57E-04* 8.85E-126
	4		5.99	*	.09	•	1.0	5E+1	5#	ς.	32E	+11		2.91	E+08	# 1.20E-04* 8.85E-126
	5	•	8.01	•	•12		7.4	7E+1	4+	2.	3 1E	+11		2.52	E+98	# 9.59E-85* #.85E-126
	6		10.06		.15		5.4	5E +1	4.	2.	3 0E	+11		2.10	E+0 5	# 6.6EE-35* 8.85E-126
•	7		12,14	•	.18		3.5	2E+1	4*	2.	2 SE	+11		1.64	E+06	# 4,34E-05+ 6.45E-12(
	3		14.25	#	.21		2.1	3E+1	4*	2.	26E	+11		1.51	E+0 &	# 2.66E-05* 8.85E-126
•	9	0	16.40	*	.24	•	1.2	2E+1	4.	2.	24E	+11		9.93	E+07	# 1.54E-85* 8.85E-124
•	10	,	18.61	•	.27		6.7	0E+1	3*	2.	2 1E	+11		7.55	E+07	# 3.53E-06* 4.85F-12
	11		20.67	•	.31		3.5	3E+1	3*	2.	1 8E	+11		5.54	E+07	# 4.56E-06* 8.85E-126
•	12		23.19	•	.34		1.3	2E+1	3+	2.	1 SE	+11	#	3. 33	E+07	# 2.39E-06* 6.35E-12
	1. 5		25.59	•	.38		9.4	5E+1	2*	2.	11E	+11		2.76	E+07	# 1.26E-06* 4.85E-126
•	14		23.07	45	.41		5.3	4E+1	2*	2.	0 7E	+11	3	2.07	E+07	# 7.27E-07+ 8.85E-12
	15		33.64	•	.45		4.3	7E+1	2+	2.	0 2E	+11		1.85	E+07	# 6.08E-07# 8.85E-12
	16		33.32		.49		1.3	35+1	3*	1.	9 8E	+11		2. 36	E+07	# 1.47E-06* 8.85E-12
	17		36.11		•53		2.1	7E+1	3+	1.	92E	+11		4.18	E+07	# 3.16E-06* 8.65E-12
	13		39.03	*	•58		3.5	4E+1	3*	1.	87F.	+11		5.34	E+87	# 5.33E-06+ 8.85E-12
	19	#	42.10	•	•62		4.5	7E+1	.3*	1.	82E	+11		6.27	E+07	# 7.56E-06* 8.85E-12
	20	•	45.34	*	.67		6.0	6E+1	3*	1.	76E	+11		6.99	E+07	# 9.70E-06+ 8.35E-12
Ü	21		46.75	•	.72	#	7.0	5E+1	.5*	1.	7 0E	+11	.₽	7.54	E+07	# 1.17E-95* 8.85E-12
	2.5	#	52.36	#	.77		7.5	1E+1	3*	1.	6 4E	+11		7.94	E+07	# 1.34E-35* 9.55E-12
•	23		56.20		. 43	#	8.3	4E +1	.3*	1.	5 dE	+11		8,20	E+J7	# 1.48E-05* 8.85E-12:
•	24		30.29		. 99		8.6	2E+1	.3*	1.	5 3E	+11	. #	3.34	L+07	# 1.59E-05# 8.85E-12
•	25	#	64.65	*	. 95	4	9.6	5E+1	.3*	1.	47E	+11	#	8.35	E+07	# 1.66E-05* 8.85E-126
•	26		69.31	-	1 - 02		4.6	5E + 1	3=	1.	42E	+11		8.25	E+07	# 1.68E-05+ 5.55E-12
	27		74.29	*	1.10	•	8.0	3E+1	.3*	1.	37E	+11	. 3	4.04	E+07	# 1.65E-05* 8.85E-12
•	23	#	73.62	#	1.17			3E+1			32E	+11		7.74	E+07	# 1.50E-05* 8.55E-12
	29	#	85.30	#	1.26	#	6.6	8E+1	. 3*	1.	2 9E	·11	#	7.54	E+07	# 1.47E-05+ 8.85E-12
	30	#	91.36	*	1.35		5.3	4E+1	.3*	1.	24E	+11	#	6.56	E+07	# 1.32E-05* 3.65E-12
	31		47.78		1.44		4.9	5E+1	.3*	1.	2 1E	+11		5.32	E+07	# 1.15E-05+ 8.85E-12:
•	32	#	104.55	•	1.54		4 . C	óc + 1	. 34	1.	1 6E	+11	#	5.72	E+07	# 9.68E-06+ 9.85E-12
	33		111.65	*	1.65		3.2	1E+1	.3*	1.	16E	+11		5.06	E+07	# 7.80E-06* 8.85E-12
	34		114.02	*	1.76	*	2.4	2E+1	.3*	1.	1 4E	+11	#	4.41	E+07	# 5.99E-06* #.85E-12
	35		126.61	*	1.87		1.7	15+1	. 3*	1.	1 SE	+11		3.72	E+07	# 4.31E-06+ 8.65E-12
	56		134.38	•	1.98	•	1.1	15 +1	. 3*	1.	1 1E	+11	, #	3.00	E+07	# 2.83E-06+ 8.85E-12
•	37		142.27	*	2,10	#	6,3	QE 4 1	2+	1.	1 0E	+11		2.25	E+07	# 1.62F-06* #.35E-12
	3 9		150.20	•	2.22	#	5.6	9E+1	.2*	1.	0 3E	+11		1.47	'E+07	# 6.95F-07+ 3.85E-12
= 3		4 2		.2 = 1	*******	3 2 2		1211	: 2 2		2 22	-	222	***		***************

MAXIMUM CONDUCTIVITY # 1.86E-84 (MHOS/M)

2	****	: =		2222	=======	2 : :		## E 1			====	*******	********	*******
	FUINT2	9#	NG 2.2	LE x	ACILS	45	CCK	ET	ı	ŔĔŬĔ	YE	,	# FREGU	
	7.62			.45E								/10(FT/S)		E+08 #
	(M)		_	(H)	-							THOSPHERES		Z) #
		23	*****	#2##	*35=355						_			- '
	PADIA	L#	RELATI	VE#	ABSGLUT	F #	ELE	CTRO	364	COLLI	SIGN	C PLASHA	# SIGMA *	EFSILON #
	INDEX											#FREQUENCY		•
6	0				(P)			/M31		(1/			# (MHG/M) *	(FD/H) #
	*****	2 E	*****	2222	• • •	= 2 :								*******
•	1	ŧ	0.30	•	0.00	•	8.4	5ē+1	4+	2.32	E+11	# 2.61E+08	# 1.03E-04*	8.85E-12#
	2				• 0 3								# 9.89E-05*	
	3				.06								8.91E-05*	
	4		2 7 7 2		.09	ï			_				# 7.27E-05+	
¥	5	#	8.11	*	.12								# 5.58F-05*	-
	6		10.16		.15								# 4.00E-05*	
	7		12.29		.10								# 2.69E-05+	
ä	8	*		*	.21								# 1.71E-05*	
	ą.		16.50	•	.24								# 1.03E-05*	
	10	#	18.31	*	.28						-		# 5.98E-06	
	11		21.06		.31								# 3.34E-06+	
	12	#	23.42	*	.35						_		# 1.84E-06*	
	13		25.33		.38								# 1.u3E-96*	
	14		29.51		.42								# 6.63E-37#	
4	15		30.99		.46								# 7.09t37*	
	16		33.5€		•50					_			. 2.19E-06*	_
	17	#	36.35	*	.54								# 3.73E-06*	_
	18		37.26	*	.58		3.5	6E'+3	134	1.87	E +11	# 5.36E+07	# 5.37E-16*	9.95F-12#
	19	#	42.31	•	.62		4.5	6E +1	13#	1.38	E +11	# 6.06E+07	# 7.06E-06+	9.85E-12#
	20		45.51	-	.67		5.4	35+1	L 3#	1.76	E+11	# 6.65E+07	# 8.76E-06+	9.95E-12#
	21		49.86	•	.72								. 1.64E-05*	
	22	#			.77		6.9	9E+1	13+	1.69	E+11	# 7.50E+07	# 1.19E-05+	8.855-124
	2.3		56.22	•	. 83		7.4	et +1	13+	1.6	E+11	# 7.76E+07	# 1.32E-05*	8.95F-12#
	24		ინ.23	*	. 89	#	7.7	72+1	13+	1.54	E+11	# 7.92E+07	# 1.42E-05*	5.95E-12#
	25		64.50	•	.95		7.8	6E+1	134	1.4	E +11	# 7.96E+07	# 1.49E-J5+	8.85E-12#
	26	*	63.04	*	1,02		7.7	5£ + 1	13*	1.44	E +11	# 7.306+07	# 1.52E-05*	8.85E-12#
	27	#	73.69	*	1.09		7.4	4++	13*	1.3	E+11	4 7.75E+07	# 1.51E-35*	8.855-12#
	23		79.06	•	1.17		6.9	58+1	134	1.34	E +11	# 7.5UE+07	# 1.47E-05+	8.65E-12#
	2.)		54.58	•	1.25		€ . 3	76 +1	13*	1.3	E +11	# 7.17E+07	# 1.36E-35*	8.856-124
	33		13.45	÷	1.33	#	5.6	7E+1	3.	1.26	£ +11	# 0.76E+0/	# 1.278-35*	9.45E-12#
	31	#	96.67	*	1.43		4.4	CE+1	3*	1.2	E+11	# 5.29E+07	# 1.13E-05#	5.35E-12#
	32	#	103.25	4	1.52	#	4.1	16+1	3+	1.2	F+11	# 5.76E+07	# J.69E-864	8.85E-12¢
	3.5	Ÿ	110.15	•	1.62								# 8.05E-36+	
	34	#	117.53	*	1.73								# 6.41E-06*	
	35	#	124.77	•	1.54		1.3	56+1	13*	1.1	SE + 11	* 5.96E+07	# 4.6hE-J6"	8.855-12#
	36		132.40	*	1.95	#	1.5	FE+	13*	1.1	Œ +11	# 3.32E+07	# 3.44E-06*	8.955-12#
	37		143.10	*	2.47								# 2.19E-J6#	
	5.4	#	144.65	4	2.19		4.5	3E +1	12*	1.3	E +11	# 1.47E+37	# 1.11E-06*	6.85F-12#
•	33	#	155.39	•	2.30	M	1.3	11 +1	12*	1.3)E + 1 1	# 1.63E+07	# 5.40E-37#	4.45124
=	*****	2 2		***	222171	- 2 :				====	****	2::::::::::::::::::::::::::::::::::::::		2312222222

(MNZCHM) 40-350.1 : YTTVITOUDHOD MURIXAM

3 :		2 1	*****	2 2 2	*****	==		*	===	3 2	Z # #	33 :	***	3 2 3	Z = 1		***************
	CINTS	0.	HOZZL	S R	ACILS		900	KFT		t	RED	EY (Ε				# FREGUENCY #
	7.92		1.	48E	-02	•	FOS	ITI	NC		500	011	FT).	/1 G	(F1	1/5)	# 2.50E+08 #
	(H)	#		(M)												HERES	
31		3 %			*****				222	32	222	*= :		5 × 3	3 3 1		****************
	SADIA	L#	RELATIV	£#	ABSCLUT	E#	EL	EC 7	404	* C	ÜLL	IS.	I GN:	•	PL	AHZ	# SIGMA * EPSILON #
#	INDEX		-	_	RACIUS										-		
				•	(4)				3)			15				(S)	# (NHOZN) * (FDZH) #
*		23	E = # 2 # 2 # 2 #	122		3 3		***	***	# Z	Z = 2	22 :	3 # Z :	F # #			*************
	1		3.36	•	0.00		4.	ALE	+14	٠	2.3	DE .	+11:	5 1	. 94	5E+05	# 5.94E-05+ 8.85E-12#
	ž		2.14		.03												# 5.73E-05+ 8.85E-12#
ä	3		4.08		.06				_								# 5.15E-05* 8.35E-12#
•	4		6.14		.09												# 4.31E-05* 8.85E-12#
á	5		8,21	•	.12								_		-		# 3.39E-05* 5.85E-12#
Ā	ś		10.30		•15				_			_	-	_	-	-	# 2.49E-05* 8.35E-12#
	7	•	12.42	#	.18												# 1.72E-05* 8.55E-12#
	ė	~	14.56		.22												# 1.13E-05+ 8.35E-12#
	ร		16.77		.25			_									# 7.10F-06# 8.85E-12#
-	10	-	19.01	*	•25			_									# 4.27E-06* 8.85E-12#
-	11	-	21.30	•	.31												* 2.49E-06* 8.85E-12#
-		-	23.55		.35												# 1.436-06* 8.85[-12#
-	12							-									
-	13		25.07	*	• 3 5			_				-					'# 4.416-07* A.45E-12#
	14	#	29.56	*	.42										-		# 5.73E-07* 6.85E-12#
•	15	*		*	• 46			-					-				# 6.57E-07* 4.85E-12#
	16	*			•50								_		-		# 2.135-06* 6.65E-12#
	17		35.59	*	• 54												4 3.62E-U6+ 6.95E-12#
	15			*	.58						-		_				# 5.12E-06* 8.85F-12#
•	19	•	42.52	*	•63												# 6.62E-06* 8.95E-12#
•	53			*	•67		_		_		_	. –					# 8.10E-06+ 8.45E-12#
•	51		43.04	~	•72												# 9.50E-06- 8.85E-12#
	55	#		4	.75		-		+13								# 1.08E-05+ A.35E-12#
•	53		56.28	*	.03				+13								# 1.19E-05+ 8.85E-12#
	24	#		•	• 19			_	+13		_						# 1.23E-05* 8.85E-12#
	25		64.40	•	• 95		-	-	+13								* 1.35E-05* 0.85E-12#
	6			#	1.02				+13			-	_				# 1.39E-05* 8.85E-12#
•	27	*			1.09				+13								# 1.39E-05+ A.85E-12#
	29	#	73.62	•	1.15			_	+13								# 1.36E-05+ a.35E-12#
	29		43.90	*	1.24		_		+13								# 1.30E-05# 8.95E-12#
	30	*	•	*	1.32				+13								# 1.21E-05* 8.85F-12#
	31	4		•	1.41												# 1.09E-05+ 8.95E-12+
ø	32			•	1.51		-		_			-			-		# 9.58E-064 8.85E-12#
#	3.3		100.93	•	1.61		-	-								-	* 8.15E-06* 5.55E-12+
	54	#		•	1.71												'4 6.68E-76* 8.95E-12#
	35		153.15	*	1.82								_			_	# 5.26E-06* 8.85E-12#
	35	#	133.61	4	1.43									-	-		'# J.93E-06* 6.85E-12#
	57		230.26	#	2.04												# 2.75E-06* 8.85E-12#
	3 4		146.14	•	2.15		_	_								_	# 1.72E+06+ 0.35E-12#
	3 3	*	155.90	+	2.27	*	З.	17E	+12	•	1.0	JE.	+11:	* 1	.63	3ビ+47	'# 9.17E-07º 8.35E-12#
= 1	*****	= =	=======	= = =		===	z = =	===	===	= =	= 4 =	==:	===	===	==:		

MAXIMUM CONCUCTIVITY # 5.34E-05 (MHOS/M)

=		z	******	* 3 2		# 2 :	222	3 2 2 2				**=******		
	FOINT31		NOZZ	LE	MACILS		FOCK	ET		₽'E'DE	Αï		FREGU	ENCY #
	8.23		1	.43	E-02				4 1	5000	(FT)	/10 (FT/S)		
	(M)		_	(1								1 MUSPHERES!		
		E			-						_			
	RADIAL		RELAT:	VE#	ARSCLUT	F#	FLE	CTRO	*40	COLL	SION	PLASHA	SIGMA +	EPSILON #
	THITEX											FRE DUENCY		
-				~ •	(P)			/H3					! (MHC/M) *	(FD/H) #
=		2 2		***		= 2 :			-			*********	· -	
	1												3.55E-05*	8.855-124
	ž		2.06		•03								3.43E-35*	
-	3		4.13		•06								3.11E-05*	
-	4	•	5.21										2.64E-05*	
-	5				•12		_						2.11E-05*	
7	6												1.595-35*	
-	7			•	, ,								1.136-15	
-	, , ,	-	14.74		.22								7.66E-06*	
-	9		16.95		•25								# 4.96E-06*	
-	_	7							-					
-	10		19.20		•28 70				_		_		# 3.09E+06*	
	11	-	21.51		•32								1 1.87E-36*	
-	12	#			•35								1.11E-J64	
7	13	*			•39								6.858-07*	
	14		28.91		***								4.91E-07*	
	15	, u			.46								5.32E-07*	
	16	*											1.995-06*	
	17	#	,		•54								3.59E-06*	
	13	*	39.74		•53								# 4.73E-06+	
	19	#			•63								5.15E-06*	
	84	*			•6₫								7.42E-06*	
4	8.1	4,			•73								# 9.73E-06*	
ŧ,	26	*			•7 <i>8</i>		-			_			9.87E-06*	
*	23				• 83								1.09E-05*	
	24				• 8 9								1.17E-J5*	
#	25	#	54.36		• 95								1.236-05*	
	25	#			1.01								1.278-05-	
	27	#			1.08								1.24E-05*	
#	28	#	78.25	. *	1.15								# 1.26E-05*	
	54	*	73.43	, +	,								# 1.22E-05*	
#	3.0	#	59+33	*		#							1 1.15F-05*	
٥	31	#	94.91	. *	1.40	#							* 1.u5E-05*	
	32		131.12		1.40			-	_	_	-		# 9.39E-06*	
	33		107.56	, +	1.50								# 8.14E-J6+	
	34		114:50		1.69	#	2.3	4E+	13*	1.17	E+11	# 4.79E+37	6.64E-J6+	
	35	#	121.61	. +	1.73								\$ 5.54E-J6+	
	36		124.36	•	1.90								# 4.36E-46*	
	37		135.50	j +	2.01	*	1.2	F + 1	13#	1.13	E+11	# 3.15E+07	# 3.17F-36*	d.85E-12#
	38	#	144.18	*	2.15	#	6.5	4- +	12*	1.1	E+11	# 2.52E+07	# 2.17E-36#	9.95E-12#
	39		151.55	, .	2.24								1.3:E-06*	
	40	#	159.77	*	2.36		2.4	QE +:	12*	1.0:	E +11	# 1.39E+07	6.19F-07*	3.35E-12#
3		= =	======	===		==		222	= = =		:::::	=======================================		========

MAXIMUM CONDUCTIVITY & 3.555-05 (MHOS/M)

= :		==		===	=======	==:	===	===	===	==	====	====	==		222222222	
# 6	CINTS	20	NOZZL	Ē	RACIUS	# 1	FOCI	(ET	•	1	REDE	YΕ		#	FREGU	ENCY #
#	5.54	. #	1.	48	E-02	#	FOS	ITI	JN	:	5000	(FT)	/1	LO(FT/S) #	2.50	E+98 #
	(M)	#	ŀ	(M)	#	PRE	ssu	ı≓E	t	0.83	2 (A	17	10SPHERES	(9	Z) #
= =		= =	::::::::::	= = =	======	==:	===	:::	===	==	====	222	==:		=========	22222222
#	RADIA	L#	RELATIV	15+	AESCLUT	E#	EL	CT	RCN	.+ C	OLLI	SION	4#	PLASMA #	SIGMA *	EPSILON #
	INDEX	. 4	PACIUS	*	FACIUS	#	DE	NSI	TY	* F	REQU	ENCY	/ # F	REQUENCY #	;	*
A			ŀ	#	(M)	#	(:	1/	3)	*	(1/	S }		(1/5)	(MHC/H) +	(FO/H) #
==	*****	==	::::::::::	===	=======	==:	===	===	===	= 4	====	2 7 F S	: = :	12 <u>-</u> 738286	=======================================	==========
#	1	#	0.00	*	0.00	#	1.	76E	+14	#	2.26	E+11	L#	1.19E+050	2.20E-05#	8.85E-12#
#	5	*		*	•03	ø	1.	7 1 E.	+14	*	2.26	E+11	L é.	1.17E+086	2.13E-05#	6.05E-12#
•	3	*	4.19	#	•06	#	1.	565	614	#	2.25	E+11	. #	1.12E+05#	1.95E+05*	8.85E-12#
	4	#	6.28	#	•09	#	1.	34E	+14	*	2.25	E+11	L#	1.04E+06#	1.67E-05*	8.855-12#
#	5		8.40	*	+12	#	1.	θE	+14	*	2.24	E+11	#	9.3384074	1.36E-05#	8.85E-12#
	6		19.54	*	•16	#	е.	? 5E	+13	*	2.23	E+11	L#	8.15E4076	1.04E-05+	8-65E-12#
#	7	4	12.70	*	•19	#	5.	18F	*13	#	2.21	E+11	L#	6.942+874	7.G2E-06*	8.85E-12#
#	Ą	#	14.90	#	.22	#	4.	13E	+13	}₹	2.23	E + 11	L#	5.776+974	5.30E-06*	8.85E-12#
#	9	#	17.13	*	•25	#	2.	7 3E	+33	+	2.17	E+11	Į#	4.69E+074	3.530-06*	8.35E-12#
#	10	X	19.48	*	•29	#	1.	7 3E	+13	#	2.15	£ +11	ĹĊ	3.74E+074	1 2.27E.054	8.85E-12#
*	11	#	21.72	+	.32	#	1.) 7 F	+13	*	2.13	E • 1	4	2.94E+674	1.425-064	8.85E-129
#	12	#	24.15	#	•36	#	6.	5 2 E	+1 3	#	2.10	E + 11	L#	2.29E+074	8.77E-87*	8.898-12#
#	13	#	26,54	4	•39	#	4.	116	+12	*	2.06	E+11	#	1.32E+076	5.616-074	8 a 85E-12#
#	14	4	24.35	*	.43	#	3.	3 3 E	+18	#	2.03	E+11	#	1.56E+074	4.211 -07*	8.85E-12#
#	15	Á	31.64	*	.47	#	3.	75E	+13	44	2.99	E+13		1.745+074	1 5.31 -07*	6.85E-12#
#	16	Ħ	34.52	#	.51	*	1.	285	+13	5 #	1.35	E+11	į į	3.216+074	1.84 -064	8.856-12#
#	17	#	37.10		•55	#	2 :	: 3E	+13	5 #	1. 31	E+11	L#	4,158+074	3.156-06#	8.85E-12#
G	14	#	39.98	#	•59	斧	2.	34E	+13	5 #	1.67	E+11	L#	4.875+674	4.44E-16*	8.85E-12#
#	19		42.99	*	.63	#	3.	668	+13	•	1.82	E+11	1 *	5.448+08%	5.69E+06*	8.956-12#
#	20	#	46.13	*	•58	.4	4.	3 4 E	+13	5 #	1 77	E+11	.#	5.316+074	6.9AE-06*	8.85E-12#
#	21	#	49.41	*	.73	#	4.	91F	+13	*	1.72	E+11	#	6.298+8:	9.046-06*	8.85E-12#
#	22	#	52.96	#	.78	#	5.	3 9 E	+13	5#	1.57	E +13	#	6.595+074	9.08E-06*	8.85E-12#
#	23	#	56.49	*	.83	#	5.	758	+13	*	1.62	E+11	L#	6.81E+074	9.498-36"	8.85E-12#
#	24	4	60.31	*	.33	#	6.	0 0 E	+13	5 *	1.57	E+11	. #	6.36E+074	1.062-05*	3.85E-12#
#	25	#	64.35	*	.95	#	6.	1 3 ĉ	+13	5 *	1.52	E + 11	L#	7.03E+07#	1.13F-05*	8.85F-12#
#	25		60.63	.,	1.01	#	6.	1 3 E	+13	•	1.40	E +11	L#	7.036+074	1.175-054	8.85E-12#
#	27	#	73.16	*	1.04	#	6.	0 1 E	+13	5 #	1.43	E+11	L#	6.98E+074	1.196-95*	8.558-12#
#	23	4	77.37	#	1.15	#	5.	746	+13	5*	1.38	E+11	L#	6.836+074	1 1. 18E-05#	3.85E-12#
#	23	Ħ	83.47	•	1.23	#	5.	456	+13	5 	1.34	2+11	1.7	6.63E+07#	1.148-15*	9.95E~12₫
#	30	Ħ	43.4A	*	1.31	ri	5,	333	.+13	5*	1.30	E+11	Ļ#	6.372+074	1.09E-05*	8.855-12#
F	31	#	94.21	*	1.39	#	4.	54E	+13	5 #	1.27	E + 1 i	. #	6.05E+076	1.01E-054	d.65E~12#
#	32	4	100.27	¥	1.43	#	4.	018	+13	5 *	1.24	E+11	L#	5.68E+071	9.14E-06*	8.85E-12#
#	3.3	Ħ	106.64	13.	1.57	#	3.	45E	+13	5 +	4.21	E+14	#	5.28E+07#	8.06E-J6*	6.85E-12#
#	34	#	113.31	*	1.57	#	2.)) E	:+13	5 +	1.13	E+11	L#	4. 43E+07i	6.91E-06*	8.85E-12#
#	35	1	120.26	*	1.77	Ħ	2.	3 6 E	+13	5#	1.16	E+11	L#	4.36E+07#	5.74E-06*	8.95F-12#
#	35	4	127.47	*	1.88	#	1.	36E	+1:	5#	1.14	E+11	L#	5.87E+076	# 4.59E-U6*	3.85E-12#
#	57	s,	134.87	4	1.39	#	1.	4HE	+17	*	1.13	F+11	1#	3.366+071	\$ 3.51E-06*	8.356-12#
#	38		142.45	*	2.10	#	1.	3	+13	5#	1.11	E+11	1#	2.94E+37#	1 2.54E-G6*	8.85E-12#
#	39	4	150.14	*	2.21	#	б.	598	E+i2	2*	1.10	E+11	1#	2.30E+07	1.64E-06*	8.85E-12#
#	40	ŧ	157.31	*	2.33	Ħ	ა.	8 J F	+1	2 44	1.10	E+1:	#	1.75E+07	# 9.77E-17*	5.85E-12#
έ,	61	Ĥ	165.71	*	2.44	#	1.	o 7 E	+12	2 24	1.09	F+11	Lø	1.16E+j7	4.32E-07*	8.85E-12#
= :		= :	========		222222	==	===	==:	====	: 4 =	====	====	= = :	=		========

(MN20HM) 70-205.5 . YTTVITOURICO MUMI) AM

```
FREQUENCY
           NOZZLE PACIUS
                          #HOUKET # REDEVE
#FOINT33#
  3.34 #
              1.48E-02
                          #POSITION : 5000(FT)/10(FT/S)
                                                              2.50E+03
                          #PRESSURE + 0.832 (ATMOSPHERES#
  (M) #
                (M)
                                                                (H7)
# RADIAL# RELATIVE* ABSCLUTE# ELECTRON*COLLISION# PLASMA # SIGMA * EPSILON #
         HADIUS * PACIUS # DENSITY *FREQUENCY# REQUENCY#
                          # (1/M3) * (1/S) * (1/S) # (MHC/M) *
                    (M)
  0.00 *
                    0.00 # 1.12E+14* 2.24E+11# 9.59E+07# 1.41E-05* 8.85E-12#
                 #
                          # 1.09E+14* 2.24E+11# 9.36E+07# 1.37E-05* 8.85E-12#
           2.11
                     .03
                          # 9.98E+13* 2.24E+11# 8.97E+07# 1.26E-35* 8.85E-12#
    3
           6.23
                     .06
                      .09
           6.35
                          # 6.65E+13* 2.23E+11# 4.35E+07# 1.09E+05* 8.85E+12#
           8.49
                      .13
                          # 7.09E+13+ 2.22E+11# 7.56E+07# 9.00E-06+ 8.85E-12#
                          # 5.526+13# 2.21E+11# 6.67E+07# 7.04E+06# 8.45E-12#
          10.65
                      +16
                          # 4.09F+13# 2.20E+11# 5.74E+07# 5.24F-06# 8.85F-12#
          12.84
                     .19
                          # 2.49E+13# 2.14E+11# 4.43E+07# 3.74E-06* 4.85E-12#
          15.05
                      .22
                          # 1.36F+13* 2.16E+11# 3.97E+07# 2.56E+06* 8.85F+12#
          17.30
                     .26
                          # 1.28f+13* 2.14E+11# 5.21E+07# 1.69E-06* 8.85E-12#
   10
          14,59
                      .29
                          # 8.14E+12* 2.11E+11# 2.56E+07# 1.39E-06* 8.85E-12#
          21.33
                     .32
   11
                          # 5.14E+12* 2.08E+11# 2.04E+07# 6.95E-07* 8.85E-12#
   12
          24.32
                      .36
          26.7€
                          # 3.36E+12* 2.05E+11# 1.65E+07# 4.61E+07* 8.85E+12#
   13
                      .40
                          # 2.598+12* 2.02E+11# 1.44E+07# 3.61F-07* 8.85E-12#
   14
          23.30
                      .43
          31.90
                          # 3.34E+12+ 1.98E+11# 1.64E+07# 4.75E-07* 8.85E-12#
   15
                      .47
                          # 1.17E+13* 1.95E+11# 3.08E+07# 1.70F-06* 3.95E-12#
   16
          34.50
                      .51
   17
       .
          37 35
                 *
                      .55
                          # 1.37E+13* 1.90E+11# 3.99E+07# 2.92E+06* 8.95E+12#
                          # 2.72E+13* 1.36E+11# 4.68E+07# 4.11E-06* 8.35E-12#
          49.23
                      .59
   18
       Ħ
   19
          43.23
                      .64
                          # 3.4CE+13* 1.02E+11# 5.24E+07# 5.27E+96* 8.35F-12#
                      .68
                          # 4.01E+13* 1.77E+11# 5.69E+07# 6.55E+06* 8.95E+12#
          46.35
   20
                      .73
                          # 4.54E+13* 1.72E+11# 6.05E+07# 7.42E+36* 8.85E+12#
   21
          43.62
                      .78
                          # 4.996 +13* 1.630 +11# 6.340+07# 8.346+06* 3.350-12#
          53.34
   22
       ħ
                 -
                      .84
                          # 5.33E+13* 1.63E+11# 6.55E+07# 9.22E+06* 0.85E+12#
   23
          56.63
                      . 59
                          # 5.57E+13* 1.58E+11# 6.70E+07# 3.93E-06* 8.85E-12#
          69.41
   24
   25
       #
          64.39
                     .95
                          # 5.70E+13* 1.53E+11# 6.76E+07# 1.05E-05* 8.95E-12#
                          # 5.72(+13* 1.49E+11# 6.79E+07# 1.09E-253 8.85E-12#
          65.53
                     1.01
   26
                          # 5.64E+13* 1.44E+11# 6.74E+07# 1.10E=
   27
          75.04
                     1.08
                                                                   8.35E-12#
                          # 5.456+13# 1.406+11# 6.536+07# 1.105-00 8.856-12#
   23
       12
          77.76
                     1.15
                          # 5.176+15* 1.36E+11# 6.466+07# 1.35E-35* 8.95E-12#
   23
          12.75
                     1.22
       iŧ
          59.33
                          # 4.92E+13* 1.32E+11# 6.23E+07# 1.03E-J5* 9.85E-12#
                     1.30
   3 3
                          # 4.396+13* 1.28E+11# 5.95E+07# 9.67E-96* 8.85E-12#
       ıŧ
          33.52
                     1.30
                     1.47
                          # 3.420+13* 1.250+11# 5.620+67# d.650-06* 8.950-12#
   32
          99.53
                          # 3.430+13* 1.22E+11# 5.26E+07# 7.93E+06* 8.95E-12#
   3 4
       # 135.74
                     1.56
                          # 2.93E+13* 1.19E+11# 4.96E+0/# 6.91E-J6* 8.85E-12#
   54
       # 112.26
                     1.66
                          # 2.43E+13* 1.17E+11# 4.43E+07# 5.c5E-06* H.85E-12#
       # 119.65
                     1.76
    35
                          # 1.360+13# 1.150+11# 5.480+07# 4.800-06# 3.850-12#
    35
       # 126.11
                     1.86
                          # 1.53E+13* 1.13E+11# 3.51E+07# 3.80E-06* 8.85E-12#
    77
       # 137.75
                     1.97
                          # 1.14F+13* 1.12E+11# 5.03E+07# 2.d7E+06* 8.89E-12#
   38
       # 145.85
                     2.08
                          # 7.956+12* 1.11E+11# 2.54E+07# 2.03E-06* 3.95E-12#
       # 142.45
    37
                     2.13
    40
       # 199.15
                     2.30
                          # 5.J2: +12* 1.1JE+11# 2.J1E+07# 1.29E-J6* 8.35F-12#
                          # 2.45E+12* 1.09E+11# 1.41E+07# 6.33F-07* 8.85E-12#
       # 153.92
                     2.42
                     2.53 # 5.17E+11* 1.09E+11# 6.45E+86# 1.34E=07* 8.85E=12#
                *
       # 171.73
```

MAXIMUM CONDUCTIVITY : 1.41E-05 (MHOS/M)

==	322323	: # :	=======	= = :	=======	£ ; ;	====	====	===	x==:	====	===		===	=========	*******
#6	OINT34		NOZZL	E A	RACILS	#6	OCKE	T		REDE	YE			#	FREGUE	NCY #
	9.15	#	1.	496	-02	# F	OSII	NCIT		5000	(FT)	/1	G (FT/S) #	2.506	+03 #
	(H)			(H)	t	# F	PESS	SURE		0.83	32 (<i>l</i>	TH	OSFHER	Es#	(42	(1)
= =	=====	= :		==:	:::::::::	# 2 2	===:	====	===	2==:	====	==	======	===	=========	3=======
#	FADIAL	. #	RELATIV	E+	AESCLUT	E≢	ELEC	CTROI	N≠ C	OLL.	IS I C	4.	PLASM	A #	SIGMA *	EPSILON #
#	INDEX	K	RAGIUS	#	RACIUS	#	DEN:	YTE	#F	REGI	JE NC Y	/#F	REQUEN	CY#	•	
•		#		#	(M)	#	(1/	M3)	#	(1/	/S)	#	(1/5)	#	(MHC/M) *	(FD/M) #
# =	======	=	=======	= = :		===	===:		===	===:	====	===	****	2:3	*********	*********
#	1	#	0.00	¥	0.00	#	7.30	E+1.	3#	2.2	2E+11	L#	7.71E+	07#	9.35E-06*	3.85E-12#
#	2	#	2.13	*	.03	#	7.19	9E +13	5*	2.22	2E + 1.1	L#	7.61E+	67#	9.11E-06*	8.85E-12#
	3	#	4.27	*	.06	#	6.63	3E+13	3*	2.22	2E + 1 :	L#	7 • 31E +	07#	8.42E-06*	9.85E-12#
#	4	#	6.42	#	.09	#	5.80	JE +1	3◆	2.2	LE+1:	L#	6.84E+	07#	7.38E-06+	8.85E-12#
	5	#	3.58	#	.13	#	4 . 82	2E+13	3*	2.21)E+1:	L#	6.23E+	07#	6.16E-06#	8.85E-12#
#	6	#	10.76	*	•16										4.89E-06+	
#	7	#	12.97	*	•19										3.71E-06+	
#	8	#	15.20	*	• 22										2.70E-06*	
#	9	#	17.47	*	•26									-	1.89E-06*	
#	10	#	19.75	*	•29										1.2#E-06*	
	11	#	22.13	#	• 33										8.47E-07*	
#	12	#	24.54	*	•36										5.56E-07+	
#	13	#	27.01	+	•40										3.84E-07*	
*	14	#	23.54	#	•44										3.12E-07*	
#	15	#	32.14	#	.47										4.27E-07*	
#	15	#	34.83	•	•51										1.57E-06+	
#	17	#	37.61	*	•55		_	2E +1.							2.71E-06*	
	15	#	40.48		•60			2E +1	-			-			3.825-06*	
*	19	#	43.47	*	•64			5E+1			_				4.69E-06*	
#	20	#	46.58	•	•69			25+1							5.925-06*	
#	21	#	41.83	*	•74			2E +1							6.89E-06*	
#	22	#		*	•79			si: +1							7.775-064	
#	23	#	56.78 60.52	_	.84			6E+1: 9E+1:				_			8.55E-06* 9.21E-06*	
#	24		64.45	_	•89			2E+1							9.74E-06*	
#	25 26	-	68.60	_	.95 1.01			EE + 1.							1.01E-05*	
7	27	#	72.97		1.08			DE +1							1.036-05*	
-	25	*	77.60		1.14			6E+1				_			1.03E-05*	
<u></u>	23		o2.49		1.22			2E +1							1.01E-05+	-
#	30	#	67.67	•	1.29			2E +1		-		_	5.10E+			
#	31	#		*	1.37			5E + 1							9.26E-06+	•
	32	#		*	1,46	#						_			8.58E-36*	
ä	33	#	104.96		1.55			9E +1							7,77E-16+	_
	34	#	111.35	*	1.64			3E +1				_			6.87E-06+	
#	35	#		*	1.74		_	7E+1				_			5.916-06*	
	36	#		*	1.94										4.95E-06*	
#	37	#		#	1.95			2E+1							4.01E-36*	
#	34	#		-	2.06										3.12F-06*	
#	33	#		+	2.17										2.32E-06*	
#	40	#	154.54		2.23	#	6.3	3E+1	24	1.1	1E+1:	1#	2.26E+	.07#	1.61E-06*	6.35E-12#
#	41	#	162.23		2.39	#	3.9	15 +1	2#	1.1	35+1:	1#	1.77E+	07#	1.00F-06*	8.85E-12#
#	42	#	163.97	*	2.51	#	1.3	4E+1	2*	1.0	汇+1.	1#	1 . 22E +	u7#	4.756-07+	J. 95E-12#
2 1	:::::::	= =	=======	==	======	==:	====			===	====	===	=====	: = = :		========

MAXIMUM CUNQUETIVITY : 1.03E-35 (MHOSZM)

APPENDIX C

LAPP computer code output for the Redeye Pissile (equally spaced data).

```
#FOINT 1#
       NOZZLE RACIUS
                #FOCKET ! REDEYE
                                       FREGUENCY
 0.00 #
         1.43E-02
                 #FOSITION : 5000(FT)/10(FT/S) #
                                       2.53E+08
 (H) #
          (H)
                 #PRESSURE : 0.832 (ATMOSPHERES#
                                         (HZ)
# RADIAL# RELATIVE* ABSCLUTE# ELECTRON*COLLISIGN# PLASMA # SIGMA * EPSILON #
# INDEX # RACIUS * RACIUS # DENSITY *FREQUENCY#FREQUENCY#
             (F) # (1/M5) # (1/S) # (1/S) # (MH0/M) 4
0.00 * 0.00 * 1.59E+17* 3.71E+11# 3.58E+09# 1.21E-32* 8.82E-12#
```

MAXIMUM CONCUCTIVITY : 1.21E-82 (MHOS/M)

```
#POINT 2#
        NOZZLE RACIUS
                  #FOCKET : REDEYE
                                            FREQUENCY
  .20 #
                   #FOSITION : 5000(FT)/10(FT/S) #
          1.480-02
                                             2.50E+08
  (M) #
                   #PRESSURE : 0.832 (ATMOSPHEPES#
           (M)
                                              (HZ)
# PADIAL# #ELATIVE* AGSCLUTE# FLECTHON*COLLISION# PLASMA # SIGMA * EPSILON #
       RACIUS *
              RACIUS # DENSITY *FREQUENCY#FREQUENCY#
                   # (1/M3) + (1/S) # (1/S) # (MHO/M) +
               (M)
# 1.51F+17+ 2.52E+11# 3.49E+89# 1.69E-82+ 8.79E-12#
        3.00 *
               0.00
               .05
        3.39
                   # 5.7 dE+17* 1.03E+11# 6.83E+09# .16
                                              * 7.31E-12#
        6.76
                .10
                   # 1.99E+17* 7.34E+10# 4.01E+09# 7.54E-02* 7.81E-12#
       10.17 *
                   # 4.52F+16* 4.79E+10# 1.31E+09# 2.66E+J2* 8.30E-12#
                •15
```

MAXIMUM CONDUCTIVITY : .16 (MHOS/F)

```
#PCINT 3#
         NOZZLE RACILS
                    ##OCKET
                            * REDEYE
                                               FREGUENCY
           1.486-02
  .40 #
                    #POSITION : 5000(FT)/10(FT/S) #
                                                2.505+03
                     #PRESSURE : 0.832 (ATMOSPHERES#
  (M)
            (H)
                                                  (H7)
# RADIAL# RELATIVE* ASSOLUTE# ELECTPON*COLLISION# PLASMA # SIGMA * EPSILON
               FACIUS # DENSITY *FREQUENCY#FREQUENCY#
 INUEX #
       AACIUS *
                (×)
                    # (1/M3) * (1/S) # (1/S) # (MHC/M) * (FD/M) #
3 · 00 · *
                    # 1.798 +174 2.51E+11# 3.30E+09# 2.01F-024 3.77E-12#
                0.00
                 .05
         5.30
                    # 1.556+16* 2.84E+11# 1.12E+13# .15
                                                 * 8.31E-12#
                    # 5.30E+17* 2.07E+11# 6.30E+03# 8.02E-02* 3.47E-12#
        6.73
                 .10
        10.17 *
                    # 1.52E+17* 1.38E+11# 3.5GE+09# 3.1GE+02* 8.63E-12#
                 .15
        13.56 *
                    # 1.85E+16* 1.10E+10# 1.22E+03# 4.63F=02* 4.66E=12#
                 .20
                    # 0.295+15+ 6.935+09# 8.176+00# 2.546-02* 6.016-12#
                 .25
```

MAXIMUM CONGUCTIVITY 1 .15 (MHOSZE)

the second secon

```
NOZZLE RACIUS #FOCKET # REDEYE
                                            FRECUENCY
#FOINT 4#
                   #PCSITION + 5000(FT)/10(FT/S) #
          1.48E-02
                                             2.50E+6A
  .60 #
                   #FRESSURE # 0.832 (ATMOSPHERES)
  (H) #
           (M)
# RADIAL# RELATIVE* AGSOLUTE# ELECTRON*COLLISION# PLASMA # SIGMA * EPSILON #
 INDEX # RACIUS * RACIUS # DENSITY *FREQUENCY#FREQUENCY#
              (P) # (1/H3) * (1/S) # (1/S) # (MHC/H) * (FO/H) #
0.00 # 3.71E+17* 2.49E+11# 5.47E+09# 4.20E-02* 8.69E-12#
        0.00 *
        3.39 +
               .05
                   # 1.06F+18* 2.73E+11# 3.25E+09# .11
                                              4 8.45E-12#
        6.78 *
                                              * 3.40E-12#
                   # 9.69E+174 2.45E+11# 8.84E+09# .11
               .10
       10.17 *
               .15 # 4.16F+17* 1.91E+11# 5.79E+09# 6.13F-02* 8.53E-12#
                .20 # 2.04E+17* 1.22E+11# 4.06E+09# 4.72E-02* 8.47E-12#
       13.56 *
       16.95 *
                .25 # 9.13E+164 9.84E+10# 2.71E+09# 2.61E-024 4.59E-12#
MAXIMUM CONDUCTIVITY :
                       (MHOS/P)
                 . 11
#FOINT 5# NOZZLE RACIUS #FOCKET # REDEYE #
                                            FREQUENCY
                   #POSITIJN | 5000(FT)/10(FT/S) #
   .40 #
          1.48E-02
                                             2.53E+08
  (H) #
                   #PRESSUPE # 0.832 (ATMOSPHERES#
# RADIAL# RELATIVE* AESCLUTE# ELECTRON*COLLISION# PLASHA # SIGHA * EPSILON #
# INDEX # FACIUS * FACIUS # DENSITY *FREQUENCY#FREQUENCY#
           #
               (M) # (1/M3) * (1/S) # (1/S) # (NHO/4) * (FD/M) #
1 # 0.00 *
               0.00 # 5.76E+17* 2.49E+11# 6.82E+09# 6.53E-02* 9.59E-12#
               .05 # 7.36E+17# 2.64E+11# 7.70E+09# 7.86E-02# 8.56E-12#
        3.39 *
        6.78 *
                •10
                   # 1.17E+18+ 2.64E+11# 9.71E+03# .15 * 8.38E-12#
       10.17 *
                .15 # 6.24E+17* 2.25C+11# 7.09E+09# 7.82E-02* 3.51E-12#
       13.56 *
16.95 *
20.34 *
                .20
                   # 2.78E+17* 1.83E+11# 4.73E+03# 4.28E-02* 8.62E-12#
   5 #
                .25
   6 #
                   # 1.48E+17# 1.50E+11# 3.45E+09# 2.77E-02* 8.67E-12#
                .30
                   # 3.75E+16* 5.39E+10# 1.74E+09# 1.96E-02* 8.49E-12#
       23.73 +
                .35 # 1.41E+16* 4.58E+10# 1.76E+89# 3.03E-03* 8.67E-12#
MAXIMUM CONDUCTIVITY : .13
                       (MHOS/M)
FREQUENCY
#POINT 6# NOZZLE RACILS #POCKET # REDEVE
                   #FOSITION + 5000(FT)/10(FT/S) #
                                             2.50E+08
# 1.00 #
          1.48E-02
                   #PFESSURE : 0.832 (ATMOSPHERES#
  (M) #
           (M)
# PADIAL# RELATIVE* ABSCLUTE# ELECTRON*COLLISION# PLASMA # SIGMA * EPSILON #
# INDEX # FACILS * RACIUS # DENSITY *FREQUENCY#FREQUENCY#
               (M) # (1/M3) * (1/S) # (1/S) # (MHC/M) * (FD/M) #
0.00 # 7.78F+17* 2.50E+11# 7.92E+09# 6.73E+02* 6.50F-12#
       J.00 +
                .05 # 5.35E+17* 2.57E+11# 6.57E+09# 5.86E-02* 4.63E-12#
        3.39 *
                                              + 8.37E-12#
                   # 1.23E+18* 2.67E+11# 3.95E+09# .13
        5.78 ¥
                .10
   *
     11
                   # 7.58E+17* 2.44E+11# 7.97E+03# 9.11E-02* 8.45E-12#
        10.17
                .15
                   # 2.70E+17* 2.08E+11# 4.67E+09# 3.66E=02* 8.68E+12#
                05.
        13.56 #
                   # 1.81E+17* 1.73E+11# 3.81E+09# 2.93E-02* 8.69E-12#
        16.95
                .25
   6
                   # 9.345+16* 1.44E+11# 2.83E+09# 1.94E+02* 8.72E-12#
        29.34
                • 30
                .35 # 3.7d-+16* 1.22E+11# 1.75E+09# 4.70E-03* 8.78E-12#
        23.73 *
```

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```
FREQUENCY
                     SFOCKET S REDEVE
         NOZZLE RADILS
#FOINT 7#
                     #FOSITION # 5000(FT)/10(FT/S) #
                                                  2.5JE+08
           1.48E-02
 1.20 #
                     #PRESSURE : 0.832 (ATMOSPHERES)
                                                    (HZ)
             (M)
  (M) #
# RADIAL# RELATIVE* AESCLUTE# FLECTRON*COLLISION# PLASMA # SIGMA * EPSILON
                RACIUS # DENSITY *FREQUENCY#FREQUENCY#
       RACIUS +
                     # (1/H3) * (1/S) # (1/S) # (HHG/H) *
                 (M)
   # 6.58E+17* 2.48E+11# 7.28E+09# 7.49E-02* 8.55E-12#
                 0.00
         0.00 *
                     # 3.45E+17* 2.53E+11# 5.63E+09# 4.3dE-02* 5.68E-12#
                  .05
         3.39
                     # 1.01E+18* 2.65E+11# 9.00E+03#
                                               .11
                  .10
         6.74
                                                     + 5.45F-128
                                               .10
                     # 9.11E+17* 2.51E+11# 8.57E+09#
                  .15
        13.17
                     # 2.97E+17* 2.22E+11# 4.89E+09# 3.77E-02* 8.68E-12#
                  .20
        13.56
                     # 1.36E+17* 1.91E+11# 3.31E+09# 2.015-02* 8.75E-12#
        10.95
                  .25
                     # 9.08E+16* 1.62E+11# 2.70E+09# 1.5AE-02* 3.76E-12#
                  .30
        20.34
                     # 4.70E+16* 1.37E+11# 1.95E+09# 9.64E-03* 3.78E-12#
        23.73
                  .35
    8
                     # 3.13E+15* 2.89E+10# 8.12E+08# 7.97E-03* 5.58E-12#
                  .40
    q
        27.11
                      # 5.2 PE+15* 2.62E+10# 6.52E+08# 5.66E-03* 3.64E-12#
                  .45
        34,50
   10
                     # 2.89E+15# 2.41E+10# 4.82E+08# 5.36E-03# 9.71E-12#
                  .50
         33.49 *
```

PAXIMUM CONDUCTIVITY # .11 (MHOS/M)

```
FREGUENCY
                             I REDEYE
#FCINT 9#
         NOZZLE KACIUS
                     #RCCKET
                     #FOSITION : 5000(FT)/10(FT/S) #
           1.48E-92
                                                  2.5JE+04
  1.40 #
                     #PPESSURE # 0.832 (ATNOSPHERES#
                                                    (HZ)
  (M)
             (H)
# RADIAL# RELATIVE* AESCLUTE# ELECTRON*COLLISION# FLASMA # SIGMA * EPSILON
        RACIUS * FACIUS # DENSITY *FREQUENCY#FREQUENCY#
                     # (1/M3) * (1/S) # (1/S) # (MHO/M) * (FD/M) #
                 (4)
# 4.14E+17* 2.43E+11# 5.79E+09# 4.79E-02* 8.66E-12#
         0.90
                 0.00
                     # 2.65E+17* 2.49E+11# 4.62E+09# 3.00E-02* 8.73F-12#
                  .05
         3.59
                     # 7.50E+17# 2.63E+11# 7.67E+09# 7.62E-02# 8.56E-12#
         6.78
                  .10
    3
                                                   * 8.43E-12#
                  .15
                     # 9.64E+17+ 2.55E+11# d.32E+03# .11
    4
        19.17
                     # 3.77E+17* 2.33E+11# 5.51E+09# 4.57E-02* 8.66E-12#
        13.56
   5
                  .29
                       3.02E+16* 2.05E+11# 2.54E+09# 1.10E-02* 8.80E-12#
                  .25
   6
        16.95
                     # 7.46E+16* 1.90E+11# 2.45E+09# 1.17E-02* 8.79E-12#
   7
                  .30
        20.34
                     # 5.50E+16* 1.50E+11# 2.12E+09# 9.97E=03* 8.79E-12#
                  . 35
    9
        23.73
                     # 3.52E+16* 1.24E+11# 1.69E+09# 7.93E-03* 3.79E-12#
        27.11
                  .40
                     # 2.27E+16* 1.13E+11# 1.35E+09# 5.68E-03* 8.80E-12#
                  • 45
   10
        30.56
                      # 1.24E+16# 1.04E+11# 9.09E+09# 3.57E+03# 8.92E-12#
                  .50
        33.89
```

MAXIMUM CUNDUCTIVITY 1 .11 (MHCS/M)

111 12 18

```
SPOINT 98
          NOZZLE RACILS
                        #FOCKET # REDEYE
                                                       FREQUENCY
  1.50
             1.485-02
                        #FOSITION # 5000(FT)/10(FT/S) #
                                                        2.50E+08
  (M) #
              (M)
                        *PRESSURE : 0.832 (ATMOSPHERES#
                                                          (HZ)
RADIAL RELATIVE ABSOLUTE ELECTRON-COLLISION PLASMA & SIGMA * EPSILON
 INDEX #
         * ZUICAF
                  RADIUS # DENSITY *FREQUENCY#FREQUENCY#
                        # (1/M3) * (1/S) # (1/S) # (MHC/M) *
                   (2)
                  3.00
                   0.00
                        # 2.61E+17# 2.59E+11# 4.40E+09# 2.84E-02# 8.74E-12#
          3.39
                        # 1.75E+17+ 2.46E+11# 3.76E+09# 2.02E-02+ 8.77E-12#
                    .05
                        # 5.19F+17+ 2.60E+11# 6.47E+09# 5.62E-02+ 3.64E-12#
          6.78
                    .10
                    .15
                       # 9.71E+17* 2.57E+11# 8.85E+89# .11
         17.17
         13.5€
                        # 4.30E+17# 2.3.E+11# 5.88E+09# 5.67E-02# 9.64E-12#
                    . 20
         16.95
                    .25
                        # 6.57E+16+ 2.15E+11# 2.30E+09# 3.60E-03* 3.81E-12#
                        # 4.71E+16* 1.92E+11# 1.95E+09# 6.92E-03* 6.82E-12#
         23.34
                    .30
                    . 35
                       # 4.27E+16* 1.71E+11# 1.86E+49# 7.02E-03* 8.81E-12#
         23.73
                        # 3.27E+16* 1.54E+11# 1.62E+03# 5.99E-03* 8.82E-12#
    q
         27.11
                    .40
                       # 2.29E+16* 1.40E+11# 1.36E+09# 4.61E-03* 8.82E-12#
   10
         30.50
                    .45
                        # 1.44E+16* 1.29E+11# 1.08E+09# 3.15E-03* 8.83E-12#
   11
         33.39
                    .50
                        # 4.96E+15# 6.46E+10# 6.32E+06# 2.16E-03# 0.92E-12#
   12
         37.28
                    .55
                        # 3.00E+15+ 6.08E+10# 4.32E+03# 1.39E+03+ 4.83E-12#
         44.57
                    -60
MAXIMUM CONGUCTIVITY :
                     .11
                            (MHOS/F)
#FOINT10#
          NOZZLE PACILS
                        #ROCKET : REDEYE
                                                       FREQUENCY
                        #FOSITION : 5000(FT)/10(FT/S) #
             1.48E-02
                                                        2.505+08
  1.80 #
              (M)
                        #PRESSURE & C.832 (ATMOSPHERES#
                                                          (HZ)
  (M) #
# RADIAL# RELATIVE* ARSCLUTE# ELECTRON*COLLISION# PLASMA # SIGMA * EPSILON #
 INDEX # RACIUS *
                 RACIUS # DENSITY *FREQUENCY#FREQUENCY#
                        # (1/M3) * (1/S) # (1/S) # (MHQ/M) *
                   ( M)
         0.00 # 1.14E+17* 2.35E+11# 3.03E+09# 1.37E-02* 8.80E-12#
          0.00 *
                       # 1.09E+17# 2.43E+11# 2.37E+69# 1.27E-02* 8.80E-12#
          3.39
                    .05
          5.78
                    .10
                        # 3.50E+17* 2.57E+11# 5.51E+09# 3.84E-02* 9.70E-12#
    3
                        # 9.06E+17* 2.57E+11# 8.54E+03# 9.93E-02* 8.47E-12#
         19.17
                    .15
                        # 4.62E+17* 2.43E+11# 6.11E+G9# 5.35E-02* 8.63E-12#
    5
         13.56
                    .20
                        # 6.30E+16# 2.23E+11# 2.25E+09# 7.96E+03# 8.82E-12#
         16.95
    6
                    .25
                        # 2.13E+16# 2.02E+11# 1.33E+03# 3.05E-03# 8.84E-12#
         20.34
                    .30
         23.73
                    .35
                        # 2.52E+16* 1.32E+11# 1.43E+09# 3.91E+03* 8.83E+12#
                        # 2.24E+16# 1.64E+11# 1.34E+09# 3.84E-03# 3.83E-12#
    ų,
         27.11
                    .40
                    .45
                       # 1.79E+16# 1.50E+11# 1.20E+09# 3.36E-03# 8.83E-12#
         30.50
   13
         33.89
                        # 1.34E+16* 1.39E+11# 1.34E+09# 2.73E-03* 8.83E-128
                    .50
   11
                          9.31E+15* 1.29E+11# 8.66E+08# 2.04E-03* 9.94E-12#
                    .55
   12
         37.28
                        # 5.79E+15+ 1.21E+11# 6.83E+08# 1.35E-03+ 8.84E-12#
   13
       #
         40.67
                    •60
                        # 5.93E+14* 2.01E+10# 2.19E+08# 8.26E-34* 8.81E-12#
                    .65
   14
         44.05
                        # 3.47E+14# 1.92E+10# 1.67E+03# 5.07E-04# 8.83E-12#
   15
         47.45
                    .70
         50.84
                    .75
                        # 1.64E+14# 1.85E+10# 1.15E+08# 2.46E-34# 8.84E-12#
```

MAXIMUM CONSUCTIVITY : 9.936-02 (MHOS/M)

the second secon

PPOINT1					
		_	RACIUS	PROCKET : REDEVE	• FREGUENCY
2.00			50-364	#FOSITION : 5000(FT)/10(
# (H)			(4)	#FRESSURE # 0.832 (ATMOS	PHERES# (HZ)
******	38	*******		* * * * * * * * * * * * * * * * * * * *	*************
					LASMA # SIGMA # EPSILON
B INDEX		RACIUS	* FACIUS	# DENSITY #FREQUENCY#FRE	QUENCY# -
į.	•		+ (H)		1/S) # (MHC/H) # (FD/H)
*****	323		******** * * * * * * * * * * * * * * * *	*************	****************
1		0.00	* 0.00	# 6.55E+16# 2.34E+116 2.	JE+89# 7.89E-03# 8.82E-12
2		3.39	+ ,05	7.50E+16* 2.42E+31# 2.0	
3		6.74	* .10		53E+09# 2.82E-02* 8.74E-12
4	_	10.17	* .15		305.4034
5	-	11.56		A COLDENIA COMMENTAL CO	90E+09# 8.51E-02# 8.52E-12
6	7			F 4.73E 71/7 7.45E 7119 6.1	09E+09# 5.27E-02# 9.64E-12
		16.95			20E+04# 7.44E-03+ 5.82E-12
7		20 . 34	4 .3C	1.23E+16+ 2.0dE+11# 9.4	96E+08# 1.66E-03* 8.85E-12
9		23.73	* .35	* 1.41[+16* 1.8%+11# 1.6	06E+03# 2.09E-03* 8.84E-12
, 3	#	27.11	* , ,40	# 1.37E+16+ 1.72E+11# 1.	05E+09# 2.24E-03# 8.84E-12
10		30.50	+ ,45	1.21E+16+ 1.50E+11# 4.4	86E+09# 2.15E-03* 3.84E-12
11	#	33.89	+ .50	9.89E+15+ 1.45E+11# 8.5	95E+0d: 1.92E-03+ 8.84E-12
12	#	37.28	* .55		82E+43# 1.59E-03* 5.84E-12
13	*	40.67	* .60	\$ -40E+15* 1.27E +11# 6.4	50L+08# 1.20E-03+ 8.84E-12
14	#	44.06	• .65	1 2 - 35E + 15# 1 . CRE + 11# 4	88E+03# 9.31E-04# 8.35E-12
15	#	47.45	* .70	2 4 7 15 A1 54 D 525 A 64 7	73E+08# 5.10E-04# 8.35F-12
16	-	50.84		. Telacato. Assistant 201	7314US# 7.1UE-U44 5.37F-12
70		20.04	* .75		57E+05# 2.50E-04* 8.955-12
FOINT1		=======================================	:==::::::::::::::::::::::::::::::::::::		****************
		_	E RACIUS		# FREGUENCY FIZED # 2.53F+00
2.20		1.4	8E-02	POSITION : 5000(FT)/10(FT/C) # 2.5JE+08
		1.4			FT/C) # 2.5JE+08
2.20 (H) =====	# #	1.4) =======	8E-02 M ========	PPOSITION : 5000(FT)/10(PPSESSURE : 0.832 (ATMOS EBBERRARIE	FT/C) # 2.5JE+00 FHERES# (MZ)
05+5 (M) ===== AIGAF	# # ==:	1.4) RELATIVE	08E-02 (M) ========= E* A8SGLUT	POSITION : 5000(FT)/10() PSESSURE : 0.832 (ATMOS) PSESSURE : 0.832 (ATMOS) PSESSURE : 0.832 (ATMOS)	FT/C) # 2.5JE+00 FHERES# (MZ) RECERTIFIED RECERTION LASMA # SIGMA * EPSILON
05.5 (h) ====== AIGAF	# # ==:	1.4) =======	HE-02 (M) E E- ABSGLUT ACIUS	PPOSITION : 5000(FT)/10() PPESSURE : 0.832 (ATMOSE ELECTRON*COLLISION# PI P DENSITY *FREQUENCY#FRE	FT/C) # 2.5JE+00 FHERES# (MZ) RESERVED THE STEEL LASMA # SIGMA * EPSILON QUENCY# *
05.5 (M) ===== Alda?	# # ==:	1.4) RELATIVE	08E-02 (M) ========= E* A8SGLUT	PPOSITION : 5000(FT)/10() PPESSURE : 0.832 (ATMOSE ELECTRON*COLLISION# PI P DENSITY *FREQUENCY#FRE	FT/C) # 2.5JE+00 FHERES# (MZ) RECERTIFIED RECERTION LASMA # SIGMA * EPSILON
(M) (M) PICAF XBONI XBONI	# # ==:	1.4) RELATIVE KACILS	# C C C C C C C C C C C C C C C C C C C	POSITION : 5000(FT)/10() PPESSURE : 0.832 (ATMOSE PELECTPON*COLLISION# PI PENSITY *FREQUENCY#FRE PENSITY * (1/8) # (1/8)	FT/C) # 2.5JE+0? FHERES# (MZ) SHERES# (MZ) LASMA # SIGMA * EPSILON QUENCY# * 1/S) # (MHC/M) * (FD/M)
2.20 (M) ====== = RADIA = INDEX	# # ==:	1.4 () () () RELATIVE () AGIUS	# C.00	#POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) #ELECTPON*COLLISION# OF #POENSITY *FREQUENCY#FRE # (1/M3) * (1/S) # () #################################	FT/C) # 2.5JE+0? FHERES# (MZ) ELEMENTE
2.20 (M) ====== = RADIA = INDEX	# # ==:	1.4 () () () () () () () () () () () () ()	# G.00 + 05	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) #ELECTPON+COLLISION# OF #DENSITY +FREQUENCY#FRE # (1/M3) + (1/S) # () #################################	FT/C) # 2.5JE+00 FHERES# (MZ) FHERES# (MZ) FROM # SIGMA + EPSILON QUENCY# + (FD/M) FROM # (FD/M) FROM # 5.05E-03+ 8.43E-12 13E+09# 5.56E-03+ 8.35E-12
2.20 (M) ===== RADIA INDEX ====== 1 2	# # ==:	1.4 (() RELATIVE *AGILS 	# AdSGLUT # AdSGLUT # C.00 # 05 # 10	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) # ELECTPON*COLLISION# OF # OENSITY *FREQUENCY#FRE # (1/M3) * (1/S) # (1/S) # 4.215+16* 2.35E+11# 1.6 # 5.62E+16* 2.42E+11# 2.5 # 1.36E+17* 2.53E+11# 3.	FT/C) # 2.5JE+02 FHERES# (MZ) ====================================
2.20 (A) ===== RADIA INDEX	# # ==:	1.4 () RELATIVE *ACIUS 0.00 3.19 6.76 13.17	# G.00 + 05 + 05 + 05 + 10 + 15	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) # ELECTPON*COLLISION# POESSURE : (1/M3) * (1/S) # (1/M3) * (1/M3) * (1/S) # (1/M3) * (1/M3)	FT/C) # 2.5JE+00 FHERES# (MZ) THERES# (MZ) THE THE THE THE THE THE THE THE THE THE
2.20 (M) ===== RADIA INDEX ====== 1 2 3 4 5	*************************************	1.4 () RELATIVE ACIUS 0.00 3.59 6.76 1J.17 13.56	# G.00 + G.00	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.032 (ATMOS) # ELECTPON*COLLISION# PO # DENSITY *FREQUENCY#FRE() # (1/M3) * (1/S) # () # 4.215+16* 2.355+11# 1.3 # 5.626+16* 2.426+11# 2.3 # 1.366+17* 2.556+11# 7.3 # 4.296+17* 2.466+11# 5.	FT/C) # 2.5JE+00 FHERES# (MZ) RERESE (MZ) RERESE EXECUTED A REPSILON REPRESILON REPSILON REPRESILON REPRES
2.20 (M) ===== RADIA INDEX ====== 1 2 3	*************************************	1.4 () RELATIVE *ACIUS 0.00 3.19 6.76 13.17	# G.00 + 05 + 05 + 05 + 10 + 15	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.032 (ATMOS) # ELECTPON*COLLISION# PO # DENSITY *FREQUENCY#FRE() # (1/M3) * (1/S) # () # 4.215+16* 2.355+11# 1.3 # 5.626+16* 2.426+11# 2.3 # 1.366+17* 2.556+11# 7.3 # 4.296+17* 2.466+11# 5.	FT/C) # 2.5JE+00 FHERES# (MZ) THERES# (MZ) THE THE THE THE THE THE THE THE THE THE
2.20 (M) ===== RADIA INDEX ====== 1 2 3 4 5	*************************************	1.4 () RELATIVE ACIUS 0.00 3.59 6.76 1J.17 13.56	# G.00 # 05 # 05 # 05 # 10 # 15 # 20 # 25	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) # ELECTPON*COLLISION* PO # COLUMN PREQUENCY #FREQUENCY	FT/C) # 2.5JE+00 FHENES# (MZ) RERESE (MZ) RERESE RERESE REPORT
2.20 (M) ===== RADIA INDEX ====== 1 2 3 4 6	*************************************	1.4 (() RELATIVE AGILS 0.00 3.19 6.76 1J.17 13.56 16.95 20.34	# G.00 + 0.00 + 0.00 + 0.00 + 0.00 + 0.00 + 0.00 + 0.05 + 0.00 + 0.00	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHERES# (MZ) RERESE (MZ) RERESE EXTENDED TO THE STREET TO THE STRE
2.20 (M) ====== = ADIA INDEX ====================================		1.4 () RELATIVE AGILS 0.00 3.19 6.76 1J.17 13.56 16.95 20.34 23.73	# AdSGLIUS # AdSGLIUS # (M) # G.00 # .05 # .10 # .20 # .25 # .30 # .35	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POSSURE : 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHENES# (MZ) 3====================================
2.20 (M) ====== RADIA INDEX ======1 23 456 7	*************************************	1.4 () RELATIVE AGIUS 10.00 3.19 6.76 1J.17 13.56 16.95 20.34 23.73 27.11	# AdSGLIUS # (M) # G.00 # .05 # .20 # .35 # .40	POSITION : 5000(FT)/10() PPESSURE : 0.832 (ATMOSESSURE : 0.835 (ATMOSESS	FT/C) # 2.5JE+00 FHENES# (MZ) RERESE (MZ) RERESE RERESE REPORTOR
2.20 (M) ====== ADIA INDEX ====== 1 2 3 4 5 6 7	经非工作品 医二甲基苯甲基苯甲基苯甲基	1.4 () RELATIVE AGIUS 	# AdSGLIUS # (M) # G.00 # .05 # .30 # .35 # .40 # .45	POSITION : 5000(FT)/10() PPESSURE : 0.832 (ATMOSESSEEDERS : 0.832 (ATMOSES	FT/C) # 2.5JE+00 FHENES# (MZ) RERESE (MZ) RERESE RERESE REPORTOR REPORT
2.20 (M) ===== RADIA INDEX ===== 123 456 7 3 111	金米二甲基苯甲基苯甲基苯甲基苯甲基	1.4 () RELATIVE AGIUS 	# AdSGLIUS # (M) # G.00 # .05 # .30 # .35 # .40 # .50	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POSSURE : 0.832 (ATMOS) ====================================	FT/C) # 2.5JE+00 FHENES# (MZ) SEE=###################################
2.20 (M) ====== ADIA INDEX ====== 123 456 73 111 12	*************************************	1.4 () RELATIVE ACIUS 	# AdSGLIUS # (M) # G.00 # .05 # .20 # .35 # .40 # .55	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POSSURE : 0.832 (ATMOS) ====================================	FT/C) # 2.5JE+00 FHENES# (MZ) SEE===================================
2.20 (M) ===================================	*************************************	1.4 () RELATIVE AGILS 0.00 3.59 6.76 1J.17 13.56 16.95 2J.35 27.11 30.30 35.89 37.26 40.57	## ABSGLIUS # ABSGLIUS # (M) ## G.00 # .05 # .10 # .20 # .25 # .30 # .40 # .45 # .50 # .55 # .50	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POSSURE : 0.832 (ATMOS) ====================================	FT/C) # 2.5JE+00 FHERES# (MZ) SEE===================================
2.20 (M) ===== ADIA INDEX ===== 1 2 3 4 5 6 7 3 1 1 1 1 1 1 1 1 1 1 1	*************************************	1.4 (CERTICAL SELATIVE ACIUS	## ABSGLIUT ## ABSGLIUT ## C.00 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .0	#POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POSITION : 5000(FT)/10() #POESSURE : 0.832 (ATMOS) # ELECTPON*COLLISION* PO # DENSITY *FREQUENCY#FRE() # (1/M3) * (1/S) # (3) # (1	FT/C) # 2.5JE+00 FHERES# (MZ) SEE===================================
2.20 (M) ===== = ADIA INDEX ===== 1 23 456 7 3 11 12 13 14 15	*************************************	1 • 4 () 1 • 4 () 2 = = = = = = = = = = = = = = = = = =	# 40 S G L I I I I I I I I I I I I I I I I I I	#POSITION : 5000(FT)/10() #PCESSURE : 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHERES# (MZ) SEE===================================
2.(M) = = = = = 2 (M) = = = = = = = = = = = = = = = = = = =	*************************************	1.4 (CERTICAL SELATIVE ACIUS	## ABSGLIUT ## ABSGLIUT ## C.00 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .05 ## .0	#POSITION # 5000(FT)/10() #POSITION # 5000(FT)/10() #POESSURE # 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHERES# (MZ) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/SE+09# 5.05E-03* 8.35E-12 3.5E+09# 5.56E-03* 8.35E-12 3.5E+09# 1.34E-03* 8.35E-12 3.5E+09# 1.34E-03* 8.35E-12 3.5E+09# 1.32E-03* 8.35E-12 3.5E-04* 8.35E-12 3.5E-04* 8.35E-12
2.20 (M) ====== ADIA X	*************************************	1.4 4 4 22222222222222222222222222222222	# 40 S G L I I I I I I I I I I I I I I I I I I	#POSITION # 5000(FT)/10() #POSITION # 5000(FT)/10() #POESSURE # 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHERES# (MZ) SEE===================================
2.20 (M) ===================================	*************************************	1 • 4 () 1 • 4 () 2 = 2 = 2 = 2 = 2 = 2 = 2 = 2 = 2 = 2 =	# ABSGLIUTS # ABSGLIUTS # (M) # C .00 # .05 # .15 # .20 # .35 # .45 # .50 # .50 # .75	#POSITION # 5000(FT)/10() #POSITION # 5000(FT)/10() #POESSURE # 0.832 (ATMOS) ####################################	FT/C) # 2.5JE+00 FHERES# (MZ) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/S) # (MHC/M) * (FD/M) RESERVE STGMA * EPSILON QUENCY# 1/SE+09# 5.05E-03* 8.35E-12 3.5E+09# 5.56E-03* 8.35E-12 3.5E+09# 1.34E-03* 8.35E-12 3.5E+09# 1.34E-03* 8.35E-12 3.5E+09# 1.32E-03* 8.35E-12 3.5E-04* 8.35E-12 3.5E-04* 8.35E-12

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MAYIMUM CONDUCTIVITY : 6.99%-02 (MHUS/M) 87

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#FCENT13	NOZZLE RA	CIUS	#ROCKET !	REDEVE		FREGUENCY	
# 2.40				5000(FT)/16	ALETISE A	2.50E+08	
Ø (M)	(M)	-	*PRESSURE			(HZ)	
• (4)	, , , , , , , , , , , , , , , , , , , ,	. 	**************************************	U1036 (417)	03-NEKE3#	1761	-
*******		341288	**********	******	*******	********	=
# RADIAL	-		# ELECTRON		PLASMA #	SIGMA * EPSILON	•
# INDEX	* KACIUS *	RACIUS	# DENSITY	FREQUENCY#F	REQUENCY#	•	
•	•	(4)	# (1/H3) 4		(1/S) #	(HHC/H) * (FD/H)	
	, 			*****			-
4			* * ^ * * * * * * * * * * * * * * * * *				_
. 1	• 0.00 *	0.00	# 3.03E+164			3.62E-33+ 8.94E-12	
2 :	3.39 *	.05	# 4.53E+164	2.426+11# 1	1. 31E+09#	5.27E-03* 8.83E-12	#
# 3	6.78 *	.10	# 1.55£+174	2.51E+11#	3.54E+09#	1.74E-02* 8.78E-12	
• 4	10-17 *	.15	# 4.955+174			5.50F-02* 8.64E-12	
# 5	13.56 +	•50	# 3.846+374		5.56E+09#	4.38E-02* 8.68E-12	
# 5	16.95 +	.25	# 4.81E+16"	2.34E+11# :	1.97E+09#	5.80E-03+ 8.83E-12	#
# 7	20.54	.30	# 5.39E+154	2.19E+11# (6.59E+08#	6.98E-04* 8.85E-12	
	23.73 4	.35	4 3.466+154		. —	4.86E-04* 8.85E-12	
		-					
		.40	# 4.97E+15				
# 13	# 30.50 *	.45	# 5.17E+154			8.54E-04* 8.85E-12	
# 11	33.89 *	.50	# 4.86E+154	1.58E +11# (6.26E+08#	8.67E-04* C.85E-12	
# 12	37.28 *	.55	# 4,27E+154	1.47E+11#	5.87E+08#	8.17E-04* 8.85E-12	
# 13	40.67 *	.60	# 3.56E+15				
# 14	44.06	.65	# 2.81E+15				
# 15	47.45 *	.70	# 2.10E+154	1.25€+11#	4.12E+08#	4.75E-04* 8.85E-12	
# 16	F 50.84 *	.75	# 1.46E+154	1.19E+11#	3.43E+08#	3.44E-04* 8.85E-12	
# 17	54.23 +	.90	# 9.12E+14			2.23E-04* 8.85E-12	
# 18 ·	57.62 *						
	–	.85	# 4.67E+14				-
# 19	# 61.01 *	• \$ 0	# 4.50E+13			8.61E-05* 6.85E-12	
# 20	# 64.48 *	• 45	# 1.50E+134	1.42E+10#	3.48E+07#	2.946-354 8.956-12	#
2222222		======		**********			3
MUMIXAM	CONDUCTIVITY	7.76	E-02 (MMOS	'M) 			=
******	*********	======	=======================================	222222222		22222222222222222222222222222222222222	=
#FOINT14	*********	======	=======================================	REDEYE	•	FREQUENCY	=
#FOINT14	NCZZLE KA	:==:::: ::LS	=======================================	REDEYE	•		=
#FOINT146	NCZZLE RA	:==:::: ::LS	#FOCKET #FOSITION	REDEYE 5000(FT)/10	# (FT/S) #	FREQUENCY	= •
#FOINT14	NCZZLE KA	:==:::: ::LS	#FOCKET	REDEYE 5000(FT)/10	# (FT/S) #	FREQUENCY 2.50E+03	= 4 4 4 = =
#FOINT146 # 2.60 6	NCZZLE	######################################	#FOCKET #FOSITION #	REDEYE 5000(FT)/10 0.832 (ATM	(FT/S) # DSPHERES#	FREQUENCY 2.50E+03 (HZ)	= 4 4 2 2 4
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#FOINT14# 2.60 # (M) # (M) # PADEX # PADEX # #	NCZZLE RA 1.48E- (M) ==================================	CILS O2 EXECUTE RACIUS 12 0.05 10 15 12 15 16 17 16 17 17 17 18 18 18 18 18 18 18 18 18 18	#FOCKET #FOSITION # #FFESSURE # # ELECTRON* # CI/M3) ** # CLECTRON* # CI/M3) ** # 2.73E+16* # 4.19E+16* # 3.89E+17* # 3.89E+17* # 3.89E+17* # 3.99E+15* # 3.40E+15*	REDEYE 5000(FT)/10 0.632 (ATM 232222222222222222222222222222222222	# # # # # # # # # # # # # # # # # # #	FREQUENCY 2.50E+03 (HZ) ***********************************	电极设置非常体型 医甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基
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# 4	# 10.17	• 15	# 3.10E+1	74 2.51E+11	# 5.00E+094	3.48E-02" 8.72	E-124
• 5	# 15.56	• •20	# 2.58E+1	74 2.46E+11	# 4.56E+091	2.96F-02* 5.73	E-124
# 6	# 16.95	• 25	# 3.35E+1				E-121
* 7		• • 30			# 4.92E+084	-	E-124
. 5	# 23.73	• .35	# 1.03E+1		# 2.88E+084		E-126
9		• .40	# 1.64E+1		# 3.65E+0A4		E-124
# 10	# 30.50	• .45	# 2.23F+1		# 4.24E+084		E-126
# 11	# 33.69	• •50 • •55	# 2.57E+1		# 4.37E+Q84		E 121
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# 15		• .70	_		# 3.48E+084		E-121
# 16		• .75			# 3.10E+094		E-121
# 17		•			# 2.70E+084		E-124
# 19	# 57.62	* .85			# 2.26F+084		E-12
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MAXIMUM CONGUCTIVITY # 2.31E-02 (MHOS/H)

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MAXIMUM CONGUCTIVITY : 1.95E-02 (MHUS/M)

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MAXIMUM CONCUCTIVITY : 1.685-02 (MHOS/M)

*****	= = =		=======================================		=======================================	*********	***********
#FOINT	204	HOZZLE	RACILS	#FCCKET	# PEDEYE	•	FREGUENCY #
# 3.5	0 #	1.45	SE-U2	#FOSITION	* 5000(FT)/10((FT/S) #	2.50E+08 #
# (H)		(1)	1)	#PRESSURE	1 0.832 (ATMOS	SPHERESP	(HZ) #
*****	===			********	PERESSEREEE	*********	*************
& RADI	AL#	RELATIVE	APSCLUTE	# ELECTRON	*COLLISION# F	LASHA # 52	GMA * EPSILUN #
# INDE	X #	RACIUS 4	FACIUS	# DENSITY	*FRE JUENCY FRE	PUENCY#	* *
		•	(K)	# (1/M3)	* (1/S) # ((1/S) # (MH	(C/4) * (FD/4) #
2227 22	= = 0	********	. = = = = = = :		***********		*************
# 1		0.90	0.00	# 5.24E+16	* 2.46E+11# 2.	06E+09# 6.4	4E-034 6.83E-12#
3 2		3.39	05	# 6.328+16	* 2.47E+11# 2.	26E+09# 7.3	1E-03* 8.82F-12#
# 3	•	6.7e	•10	# 9.42E+16	# 2.48E +11# 2.	76E+09# 1.0	7E-02* 8.81E-12#
# 4	#	10.17	•15	# 1.27F+17	+ 2.47E+11# 3.	20E+09# 1.4	5F-02* 8.80E-12#
# 5		13.56	•20	# 7.44t+16	* 2.43E+11# 2.	45E+09# 8.6	4E-03+ 8.82E-12#
# 6		16.95	•25	# 1.37F+16	* 2.36E+11# 1.	05E+09# 1.6	3E-034 8.85E-12#
# 7		20.34	• 30	# 1.41E+15	* 2.27E+11# 3.	37E+09# 1.7	75E-04+ 3.85E-12#
# 3	#	23.73 4	.35	# 2.08E+14	* 2.16E+11# 1.	29E+85# 2.1	11E-054 3.85E-12#
# 9		27.11	-48	# 1.61++14	* 2.05E+11# 1.	14E+09# 2.2	22E-05* 8.85E-12#
# 19		30.50	. 45	# 3.12E+14	* 1.93E+11# 1.	59E+0s# 4.5	55E-05° 6.85E-12#
# 11	4	33.49 4	•50	# 4.63F+14	+ 1.82E+11# 1.	93E+08# 7.1	5E-05+ 9.35E-12#
# 12	4	37.28	• 55	# 5.532+14	* 1.72E+11# 2.	11E+05# 9.0	3E-054 8.85E-12#
# 13	#	40.67	•60	# 5.935+14	+ 1.63E+11# 2.	130+00 1.0	2E-04+ 8.35E-12#
# 14		44.06	.65	# 5.998+14	* 1.55E+11# 2.	20E+0## 1.0	19E-14* 8.35E-12#
# 15	#	47.45	.70	# 5.30E+14	* 1.4%+11# 2.	16E+0## 1.1	OE-J4+ 8.85E-12#
# 16	4	50.64	.75	# 5.42F+14	* 1.42E+11# 2.	1.09E+03# 1.0	8E-04+ 8.85E-12#
# 17	#	54.25	• • • •	# 4.752+14	* 1.36E+11# 2.	.00E+04# 1.0	2E-04* 8.85E-12#
# 19		57.62	.85	# 4.435+14	* 1.32E+11# 1.	.39E+05# 3.4	8E-054 8.85E-12#
# 19		61.31	•90	# 3.30E+14	* 1.2 E+11# 1.	.77E+05# 4.5	9E-05+ 8.85E-12#
# 20		64.40	• 95	# 3.376+14	* 1.24E+11# 1.	65E+03# 7.6	4E-054 8.85E-12#
# 21		67.75	1.00	# 2.87E+14	* 1.21E+11# 1.	52E+05# 6.6	66E-05+ 8.856-12#
# 22	#	71.15	1.35	# 2.41E+14	* 1.19E+11# 1.	39E+03# 5.7	165-05% 8.85E-12#
# 23		74.56	1.10	# 1.98E+14	* 1.17E+11# 1.	266+09# 4.7	7E-85* 0.85E-12#
# 24	4	17.95	1.15	# 1.556+14	* 1.15E+11# 1.	13E+08# 3.5	1CE-05+ 8.85E-12#
# 25		31.34	1.20	# 1.25E+14	* 1.14E+11# 1.	00E+08# 3.1	UE-354 8.85E-12#
# 25		54.73	1.25	# 9.60E+13	* 1.12E+11# 3.	90E+07# 2.4	15-85+ 8.85E-12¢
# 27		54.12	1.30	# 7.03E+13	* 1.11E+11# 7.	55E+07# 1.7	73E-654 B.85E-124
# 23		91.51	1.35	# 3.23E+13	+ 6.22E+10# 5.	.10E+67# 1.4	6E-35+ 4.85E-12#
*****	===			========	31212322222		

MAXIMU4 CONDUCTIVITY : 1.45E-02 (MHOS/P)

#FOINT21 # 4.00 # (M)		#POCKET # REDEYE ##################################	
# RADIAL # INDEX		EF ELECTRONS COLLISIONS PLASMA F DENSITY STREQUENCY FREGUENCY F (1/M3) STREAM (1/S) F (1/S) F	
# 1 # 2 # 3	0 0.60 + 0.00 0 3.39 + .05 6 6.75 + .10	# 5.97E+16* 2.47E+11# 2.19E+09# # 6.85E+16* 2.47E+11# 2.35E+09# # 9.2GE+16* 2.47E+11# 2.72E+09#	7.81E-03* 8.92F-12# 1.05E-02* 8.81E-12#
• 5 • 5 • 7	# 10.1 * .15 # 13.76 * .20 # 16.95 * .25 # 20.34 * .30 # 23.73 * .35	# 1.0 36+17* 2.46E+11# 2.962+09# # 5.73E+16* 2.42E+11# 2.15E+09# # 1.03E+16* 2.35E+11# 9.10E*08# # 1.19E+15* 2.27E+11# 3.10E+09# # 1.6GE+14* 2.17E+11# 1.14E+00#	6.67E-03+ 8.03E-12# 1.23E-03+ 8.05E-12# 1.48E-04+ 8.05E-12#
# 9 # 10 # 11 # 12	# 27.11 * .40 # 30.50 * .45 # 33.85 * .50 # 37.22 * .55	# 7.91E+13* 2.06E+11# 7.93E+07# # 1.06E+14* 1.95E+11# 1.22E+09# # 3.37E+14* 1.85E+11# 1.65E+08# # 4.32E+14* 1.75E+11# 1.97E+08#	1.07E-05* 8.85E-12# 2.69E-05* 8.85E-12# 5.15E-05* 8.85E-12# 6.97E-05* 8.35E-12#
# 13 # 14 # 15 # 16 # 17	# 40.67 * .60 # 44.06 * .65 # 47.45 * .70 # 50.84 * .75	# 4.91E+14* 1.66E+11# 1.97E+08# # 4.98E+14* 1.58E+11# 2.00E+08# # 4.92E+14* 1.50E+11# 1.99E+08# # 4.6 9E+14* 1.44E+11# 1.94E+08# # 4.35E+14* 1.39E+11# 1.87E+08#	9.89E-05+ 8.85E-12# 9.21E-05+ 8.85E-12# 9.16E-05+ 8.85E-12#
10 10 10 10 10 10 10 10 10 10 10 10 10 1	# 54.23 * .80 # 57.62 * .85 # 61.01 * .90 # 64.40 * .95 # 67.79 * 1.00	# 4.35E+14* 1.39E+11# 1.87E+08# # 3.97E+14* 1.34E+11# 1.79E+08# # 3.55E+14* 1.30E+11# 1.69E+08# # 3.13E+14* 1.26E+11# 1.59E+08# # 2.72E+14* 1.23E+11# 1.48E+08#	8.35E-05+ 8.85E-12# 7.70E-05+ 8.45E-12# 6.58E-05+ 8.85E-12#
0 22 0 23 0 24 0 25	71.16 * 1.05 74.56 * 1.10 77.95 * 1.15 8 81.34 * 1.20	# 2.32E+14* 1.21E+11# 1.37E+00# # 1.36E+14* 1.10E+11# 1.26E+08# # 1.62E+14* 1.16E+11# 1.14E+09# # 1.33F+14* 1.15E+11# 1.03E+03F	5.43E-35+ 8.85E-12# 4.67E-05+ 8.85E-12# 3.92E-05+ 8.85E-12
26 0 27 0 25 0 25 0 25 0 25 0 25 0 25 0 25	# 64.73 * 1.25 # 99.12 * 1.30 # 91.51 * 1.35 # 94.30 * 1.40	# 1.35E+14* 1.13E+110 9.19E+070 # 8.15E+13* 1.12E+110 8.10E+070 # 6.00E+13* 1.11E+110 6.96E+070 # 1.09E+13* 2.35E+160 2.96E+070	2.04E-05* 8.65E-12# .52E-35* 8.65E-12#

MAXIMUM CONCUCTIVITY # 1.25E-02 (MHOS/M)

=	*****	3 1		3 5				===	= =	*****	: = =	282	3 2 2	***	32	*******	===	****	2 2 2 2
	FOLNTZZ	•	NOZZLE	H	ACILS		OCKE									FREG		-	•
	4.20		1.4	3F	-02	8 P	OSIT	ION		5000	(FT	1/1	0 (F	T/S)	•	2.5	0 E +	0.5	•
•	(H)	•		41						0.43						(HZ)		
=	******	21		22		8 2	E 2 2 2		==			===				*******	3 Z Z		3888
•	FACTAL	4	RELATIVE	•	ARSCI UTE		ELEC	THO	۸.	COLLI	5 T C	N#	PL	ASMA		SIGMA	* E	PSIL	ON #
I	INCEA		RACIUS		RACIUS		GENS	ITY	``₽	FREDU	NC	Y#F	SE C	DENC	* Y		#		
7	THUSA	*	A46203		(۲)			M3)						1/51	•	(MHC/M)	•	(FD/	M) #
_				-	\		\	***	= =		, , 2 2 2					******	222	****	7888
_		_	0.00	•	0.00		6.60	F 4 1	64	2.47	F • 1	1.0	2.5	51F+6	19#	7.54E-05	• 4	1. 92E	-12#
7	-				.05		7.24						2.1	SE+	138	3.31E-03		.82E	-12#
#	2	•	3.39	4						2.47				58E+0				. 61E	
9	3		6.78	•	-10	•	9.23							73E+	-			3. 91E	
•	•		10.17	_	.15				_	2.41		-		88E+1				. 43E	_
•	5		13.56	_	• 50	•				2.35				36E+				3.35E	
	6	•	16.95	_	.25								-	83E+(3. 45E	-
•	7	•	20,34	-	.30	•	9.93)2E+(_		9. 85E	
*	9		23.73	•	•35	•				2.17				32E+i				3. ASE	
	9	J	27.11	•	-40	•	5.76								-		-	3.85E	
	10	#	30.50	•	.45	•				1 97			_	04E+(8 . 85E	
#	11	#	33.49	-	•50	•	2.51							42E+	-			9.85E	
	12		57.28	•	•55		3.34						-	64E+1				3.07E	
	13		40.67	•	-60	•	3.55						_	76E+				9.07E	
	14		44.06	#	.65		4.10	-						42E+					
	15		47.45	#	.70	•	4.19	E +1	•		-			83E+				8.85E	
	16		50.04	•	.75		4.0	E+1	41					?1E+		_			
	17		54.23	-	.80		3.4	t +1	44	1.41	E + :	11#		75E+				8.85E	
	15	#	57.52	•	• 85		3.54	E+1	.44	1.36	E + :	11#		69E+				8.95E	
•	19		51.11	-	. 40		3.2	++1	44		_			61E+	_			8.95F	
4	23		54.40	•	.95		2.8	£ +1	4	1.25	€+:	11#		52F+			_	8.35E	
í	21		67.79		1.00		2.5	E. +1	4					43E+			-	8.85E	-
4	22		71.18	•	1.05	#	2.2	F+1	4	1.22	E+:	11#		34E+	_			8.85E	
4	2.3		74.56		1.10		1.5	E+1	4	1.20	E+	11#		24E+			-	3.55E	
4	24		77.15	•	1.15		1.6	(F. +1	44	1.16	E +:	11#	1.	14E+	061	5.856-09	_	8.856	
Ä	25		31.34		1.20	ä	1.3				E+:	11#	1.	04E+	0 a 4	5.24E-0!		8.356	
4	26		34.73	#	1.25				-	-				40E+		2.705-09	-	a. 356	
7	27	#	65.12		1.30		2.7							39E+	074	2.17E-0	5*	a. 852	-12#
7	21		11.51		1.35	•	6.7		_				7.	57E+	374	1.69E-0	5*	3.355	-12#
7	23	•	94.90		1.40		4.4							47E+			5•	8. 956	-12#
•		7 2 2	7777" #################################	. .		::	* # # #			22222	EE	= = = = = :	2 E 3	====	4 2 2	*******	# = #	=====	====

MAXIMUM CONGUCTIVITY 1 1.865-02 (MHOS/M)

	====== foint2:	: # : 4	######################################		ACILS		60CK	222 E7	==:	28E	5# 1 Ev 4	1888: :	******	***	FRECU	22222222
ĭ	4.40	-			-05			TIJN	-			-	10(FT/S			
i		ě		(N)				SULE					MOSPHER	-		
=		: =			, ::::::::::::::::::::::::::::::::::::			2222	***	222	33 1	 2555	*****	333		*********
	R40: 1		RELATIV	E=	AESOLUT	E#	ELE	CTRO		OLL	IS 2	CONF	PLASH	A	SIGMA .	EPSILON #
	INDEX		PACIUS	, .	RADIUS		DEN	SITY		REQ	UE !	ACY#	FREQUEN	CY		•
					(4)			/×31			/5		(1/5)	_	(MH0/M) .	(F3/H) #
*	******	: =	*******	:==:	*******	221	***		***	===	88 :	2222			*******	********
	1		0.40	•	0.00	•	7.0	1E+1	6*	2.4	7E (110	2.38E+	034	5.01E-03*	8.8ZE-12#
•	2				.05		7.5	JE+1	6*	2.4	7E 1	110	2.46E+	•		
•	3		5.70	•	•13			JE + 1	-			110			9.736-03*	
	•		10.17	*	•15	#	7.7	31: +1	6+				2.50E+			8.82E-12#
•	5	•	13.56	•	.20	_		6E + 1	_				1.65E+			
•	5			•	. 25			4E+1								
#	7		20.54	•	.30			1E + 1					2.57E+			8.85E-12#
	5	•		•	.35			7E+1							1.39E-05+	
	9		27.11	•	• 4 0			9E +1	-							
	10				• 45			3E + 1	-		_				1.47E-05*	
	11			•	•50			9E+3								
	12		•	•	.55			1F +1						2 7	4.27E-85*	
•	13			•	.60	•		9E+1								*****
	14			•	.65	•		5f. + 1					1.67E+			
	15	•	.,	-	.70			5£+1			-		1.69E+	-		
	16		50.84	•	•75			2E+1								· · · · ·
	17	•		*	. 60			7E+1	-						6.65E-05*	
	15 19	-	57.62		.es			6E+1 1E+1	•			•11# •11#	1.53E+		6.46E-05+ 6.15E-05+	• • • • • • •
-	50	*	61.01	_	.95			46 + 1	-				1.46E+			
-	21	*	•	•	1.00			6F+1				110		• • •	- •	
I	55	ï		•	1.05			0E +1			_		1.30E+			
•	23			•	1.10			16 + 1				110	1.21E+			
ě	24	<u> </u>	17.95		1.15			5E +1						-		
	25	•			1.20			2E+1	-							
	26		94.73		1.25			1E +1				110	3.44E+			
ě	27			•	1.30	-		4E+1	-			+11#		_	2.23E-05*	
	2.9		91.51		1.35			3F+1					7.63E+			· · · ·
	29			•	1.40			51+1	_						1.48E-J54	
•	30		y#.29	•	1.45			1£+1	-				_		1.168-05*	
	31			•	1.50				_	-	_		3.62E+			
	32		105.07		1.55				-	-		_			5.49E-06*	- · • ·
	3.5			4	1.60										2.94E-36*	
*			*******	**		3 3 :	**=	2232	321		33:			222		********

MAXIMUM CUNCUTIVITY 1 9.73E-03 (MHOS/P)

3	*****	2	******	2 2 1	*******	**	******	# # #		222	******		********
•	POINT24		NGZZŁ	E	ACIUS	#1	FUCKET	1 .	REDEY	E	•	FRECUE	FNCY #
•	4.60				-02					_	/10(FT/S)		
4		ě		(M)	- -						MOSPHEPES!		
-		-		• • •		•			,, , , , , , , , , , , , , , , , , , ,		103-02-631	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.,
-	RADIAL	_	RELATIV		ABSCLUT		FLECTRO			·			5001141
				_									EPSILUN .
	INDEX		AADIUS	_		•		_			FREQUENCY		
•	,	•		•	(+)		(1/23)	•	(1/5) (P (1/S) ((MHC/H) *	(FD/H) #
		#	******	2 2 1		3 2 3			= = = ==	===:		*********	
	1	•	0.00	•	0.00			-				9.32F-03*	
•	2	\$	3.59	•	.05		7.57E+1	5 * .	2 • 4 6E	+116	1 2.47E+U31	9.66E-03+	8.826-12#
4	\$ 5		6.78	•	.10		7.37E+1	6*	2.46E	+116	P 2.53E+09 <i>f</i>	3.15E-034	8.82E-12#
1	4	•	10.17	•	.15	•	6.301+1	6-	2 . 4 SE	+111	2.25E+ 091	7.29E-034	8.825-124
4	5	•	13.56		.20		2.475+1	6*	2 . 4 UE	+11	1.41E+096	2.91E-03+	8.84E-12#
1	<u>ن</u> (16.95		.25	•	4.17F+1	5*	2.34E	+11	5.80E+036	5.C2E-04*	8.85E-12#
4	7		20.34	•	.30							9.29E-35*	
4			23.73	#	.35							1.16E-05*	5.855-124
i	9	ě	27.11		.40			-				5.43E-06+	
4	10	•	30.50	•	.45		8.12E+1	_				1.15E-05*	8.55E-12#
-	11	•	33.89		.50		1.606+1					2.58E-05*	8.655-12#
7	12	ī	37.25		•55		2.226.+1					3.47E-15*	
	13	Ξ	40.67	4									
-				_	.60	7	2.65E+1					4.35E-05*	9.85E-120
	14		4.06	_	•65		2. +1E+1		1 • 6 4E			5.01E-05+	8.35E-124
•	15	•	47.45	*	.70		3.03E+1		1.57E			_	**
•	16		50.94	*	.75		3.05 +1		1.50E			5.71E-054	8.85E-12#
•	17	#	54.23	•	• 6 0		2.975+1		1 • 45E				0.95E-12#
•	1.5		57.52	•	• 9 5		2.316+1		1.40E			5.67E-05*	3.85E-12#
•	19	#	61.31	•	•90	•	2.63E+1	-				5.48E-05*	8.95E-12#
4	20		54.4C		• 95	#	2.410+1	4*	1 . 3 1E	+114	# 1.39E+9A#	5 - 17E-05+	8.855-124
4) 21	#	67.79	•	1.00	ø	2.19E+1	4*	1.285	+11	# 1.33E+086	4.81E-05+	1.55E-12#
1	22	#	71.15	•	1.05		1.45E+1	4#	1.25E	+11	P 1.25E+086	4.4CE-05*	8.95E-12#
1	23	#	74.56	•	1.10	#	1.728+1	4	1 . ? ZE	+114	# 1.13E+096	5.97F-054	4.85E-12#
1	24		77.45	•	1.15		1.508+1	4=	1.208	+11	# 1.18E+39	3.52E-85*	4.95E-12#
4	25	#	t1.34		1.20		1.305+1	4*	1.18E	+111	1.02E+08	1 5.09E-054	8.85E-12#
1	25		34.73	*	1.25		1.106+1	4.4	1.17E	+11	# 9.42E+076	2.66E-J5*	8.85E-12#
4	27		53.12	*	1.30		9.225.1		1.15E	_			4.45E-12#
•	28		91.51		1.35		7.575+1		1.14E	+11	# 7.31E+J76	1.87E-95*	3.85E-12#
4	29		34.30		1.40		5 . J1 £ +1		1.135				8.55E-12#
1	30		93.25		1.45		4.675+1		1.126			1.156-054	5.85F-12#
4	31	ě	131.66	•	1.50		3.35E+1				# 5.20E+07	-	8.35E-12#
-	32		105.07	4	1.55		2.296+1		1.10E				8.855-12#
	33	#	103.07		1.60		1.29E+1	-	1 . C +E				
*	, 33 } 34		111.65	-	1.65		2.165+1				1.32E+J7		9.85E-12#
*	35		115.24		1.70	# # # # # # # # # # # # # # # # # # #	1.096+1	-			9.395+16		
=	, J7	-	112014		1070	- -	エ・リコにマム		エチロフこ	410		, 400022101 40022221	70000000000000
		*	* * * * * = = =	3 3 3		E 8 :	===== ===============================	= = =	# # # # # #	333			

MAXIMUM CONCUCTIVITY : 9.155-03 (MHCS/M)

1	******		******	-	******	==:		13 2	===							********
(POINTES		NOZZL	E F	RACILS	#1	ROCKI	T	1	R	EOEY	Έ			P FREQUE	ENCY #
•	4. 19	•	1.	406	-02		1204	TO	N I	51	3000	FTI	/10	(FT/S)	2.50	E+08 #
1) (H)	•		(M))		PRES:	iUR	E 1		. 6 32	LA	TPO:	SPHEPES	B (H)	2) •
1	******	=		221	******	==:	****		221					******	*********	*********
-	P RADIAL		RELATIV	E+	ABSCLUT	E#	ELEC	FT;	OP.	501	LLIS	ION	•	PLASMA	# Sägma +	EPSILON .
(INDEX	#	RACIUS		RACIUS		DEN	112	4	FRE	EQUE	NCY	OFR	EQUENCY	•	•
•	•	#		•	(P)		(1/	/H3) •	• ((1/8		•	(1/5)	# {MHG/M} *	(FD/H) #
1		3	******	221	******	22:		***	===		2 2 2 2	***	===	*****	*********	********
(1	•	0.00		0.09		7.2	SE+	16*	2	. 466	+11	. 2	.42E+09	0.33E-03*	3.82E-12#
•	2	•	3.39		.05		7.41	E+	16+	2	. 46E	+11	. 2	. 44E+89	# 8.45E-03+	4.82E-12#
(3	•	6.78		.10		7.17	TE+	16*	2	. 45E	+11		.40E+89	# 8.26E-03*	451-358.8
(4	•	10.17	•	.15		5.01)E+	16*	. 2	. 43E	+11	# 2	.01E+09	# 5.80E-03*	8.83E-12#
•	5	•	13.56		• Z 0		1.9	LE+	16*	. 2	, 3 %	+11	. 1	.215+09	# 2.13E-03*	8.85E-12#
4	6	•	16.95	•	55 ،		3.0	BE +	15*	2	. 3 JE	+11	# 4	t 0 + 30 F .	# 3.71E-04*	9.85E-12#
•	7		20.34	•	.30		5.4	LE+	14*	. 5	. 26E	+11	# Z	.09&+09	# 6.73E-05+	8.85E-12#
- (#	23.73		.35		7.79	if +	13*	2	. 1 SE	+11	# 7	. 30E+07	# 1.00E-05+	8.85E-12#
() 9		27.11	*	. 4 0	#	3.1	BE +	13•	. 5	. 8 9 £	+11	# 5	.04E+07	# 4.25E-06*	6.55E-12#
(10		30.50	#	.45		6.6	h E +	13*	. 5	. O OE	+11	• 7	.31E+07	# 4.36E-06*	4.855-12#
•	11	#	33.49	#	.50		1.3	4E +	14*	1	. 91E	+11	. 1	.04E+05	# 1.98E-05*	8.55E-12#
•	12	#	37.28		• 55	#	1.8	BE+	14"	1.	. 82	+11	# 1	.23E+05	# 2.91E-05+	8.85E-12#
	13		40.67	*	.60		2.2	7E +	14*	1	. 7 JE	+11	# 1	.35E+08	# 3.68E-05*	8.85E-12#
•	14	2	44.06	•	• 65		2.5	2E+	14"	1.	. 6 SE	+11	# 1	.42E+08	# 4.2ôE-05*	8.852-12#
1	15	#	47.45	•	.70	•	2.5	bf. +	14*	1	. 5 9£	+11	. 1	.46E+08	# 4.70F-05*	8.85E-12#
(16		50.64	•	.75		2.5	435	14	1	. 526	+11	• 1	.47E+06	# 4.96E-054	8.85E-12#
1	17		54.23	•	. 80		2.6	4E.+	14.	1	. 468	+11	# 1	.46E+08	# 5.08E-05*	8.85E-12#
1	18		57.62	•	.85		2.5	3E +	14"	1	. 416	+11	# 1	.43E+08	# 5.03E-05*	8.35E-12#
4	19		61.01	#	.90		2.3	eE+	14*	1	. 37E	+11	# 1	.3aE+0:	# 4.9cE-05*	8.458-12#
4	20		64.40	7	• 35		2.2	LE+	144	1.	. 3.3E	+11	. 1	.33E+06	# 4.65E-05#	8.85E-12#
1	21	#	67.79	•	1.00		2.0	?E+	14*	1	. 2 YE	+11	# 1	.28E+08	# 4.39E-054	8.85E-12#
(22	#	71.18	*	1.05		1.5	2F +	14"	1	. 266	+11	# 1	.21E+0 <i>8</i>	# 4.07E-05*	8.855-12#
•	23		74.56		1.10	4	1.6	3E +	14	1	. 2 4E	+11	• 1	.15E+08	# 3.71E-05*	4.85E-12#
•	24	#	77.35	•	1.15		1.4	454	14*	1.	. Z 18	+11	* 1	.00E+05	# 3.33E-05*	8.858-126
4	25	#	61.34	•	1.20	#	1.2	E+	14-	1.	. 1 X	+11	# 1	. 01E+98	# 2.96E-05*	8.55E-12#
	25	•	64.75	•	1.25		1.3	9F +	14*	1.	. 17E	+11	. 9	. 33E+07	# 2.53E-05*	8.95E-12#
•	27	•	48.12	*	1.30		9.2	lt+	1 5*	1.	. 1 6E	+11	# 8	.61E+87	# 2.24E-05*	8.85E-12#
•	29	#	91.51	#	1.35	•	7.5	?E+	13	1.	. 1 FE	+11	# 7	. 36E+07	# 1.89E-05+	8.55E-12#
•	6 5		94.90	•	1.40		6.5	2t. +	13*	1	. 1 SE	+11	# 7	.14E+J7	# 1.57E-05*	8.855-12#
1	50	#	94.29	#	1.45		5.0	3E +	13*	1	• 1 <i>2</i> 5	+11	# 6	. 37E+07	# 1.26E-05*	8.85E-12#
•	31	#	101.63	•	1.50		3.5	9f +	13*	1.	. 1 15	+11	# 5	.60E+U7	• 9.84E-06+	8.556-12#
1	32		105.07	*	1.55	#	2.30	5E +	13"	1.	. 1 1E	+11	. 4	. 30E+37	# 7.27E-06*	6.85E-12#
•) 33	#	100.46	#	1.60	#	1.4	3E+	13*	-					# 4.95E-06+	8.35E-12#
4	34	#	111.35		1.65		1.1	4E +	13*					•03E+17		
1	35	#	115.24	•	1.70		5.7	7E +	124	. 8	. 726	+10	• 2	.16E+87	# 1.96E-36*	4.756-12#
1	******	8	222222	2 3:		= =		1 2 2	323	32:	2 Z Z Z		222	******	22222222	********

MAXIMUM CONSUCTIVITY : 6.436-03 (MMSCHM)

*****		******							***	42 22	==:	*******	********	********
OPCINT	260	NCZ7L	E F	ACILS	# F	CCK	E 1		RED	EYE			P FREGU	ENCY #
# 5.0	0	1.	43E	- 6 2	# 1	CSI	TION		500	OIFT	1/1	10(FT/S)	?.50	E+08 #
# (M))	(8)			FESS	SUPE		0.9	32 (ATP	HOSPHERES	D (4)	Z) #
*****		*******		******	# # 1	****		22	***		# 21			********
# RADI	ALE	PELATIV	/E#	AESCLUT	Eø	ELE	CTRO	-	COLL	1S I G	NF	PLASMA	# SIGMA +	EPSILCA #
. INDE	X #	FACIUS		FACIUS		CENS	SITY		FREG	UE NC	Y #1	FREQUENCY	•	•
•)	•	(M)		11.	/45)	•	[1	/S)		(1/5)	# (MMC/4) #	(FD/H) #
22222	1284	*******		*****		2728		**		** = =		********	*********	********
• 1		0.00	•	0.00		€.9	4E + 1	6#	2.4	6E + 1	1#	2.37E+09	6.01E-03*	8.82F-12#
. 2		3.39		.05		6.9	2E + 1	E#	2.4	X + 1	1#	2.368+09	7.95E-JJ+	8.62E-12#
# 3		5.76		•10		6.1	6E +1	5+	2.4	4E + 1	1#	2.23E+0+	• 7.13F-03+	8.82E-12#
	•	10.17	•	.15									# 4.49E-13+	
		13.56		.20	#								# 1.54E-03+	
		16.95	•	.25		2.3							# 2.64E-04*	
0 7	-	20.54		.30						6E + 1	1#	1.88E+05	# 5.45E-15+	4.45E-12#
	•	23.73	•	. 35	•	7.0					_	7.51E+07		8.85F-12#
		27.11		.40		2.7		-				4.68E+07		
. 10		36.50	•	.45	ė			-				5.65E+07		
. 11		33.85	#	.50		1.1		-			-	9.566+07		
# 18	-	T		.55	į		1E+1					1.14E+05		9.85E-12#
. 1		43.67		.60	•	1.9						1.266+08		
. 14		44.06	•	•65		-	_				_	1.53E+09		
. 15		47.45		.70	4							1.376+98		
. 16		50.94		.75		2.3				4E+1			# 4.35E-15*	
. 17				. 60			-				-		# 4.49E-05+	
. 1		57.62		•85	•				_			1.36E+08		
. 19		. 11117		.90							_	•	# 4.41E-05*	
# 20		11111		. 95							_		# 4.256-05*	
ē 21				1.00		1.8						1.23E+03		
. 22		71.14		1.05			-	_				1.17E+0		
# 23			•	1.10									# 3.46E-15*	
24				1.15			7E+1				_	1.056+08		-
. 29		31.34	*	1.20			1F + 1				_	9.86E+07		5. 55E-12#
0 29		34.73		1.25		_					_	9.21E+07		
# 27		70.12		1.30	•				1.1					
. 2				1.35							_	7.486+07		
. 2		14.50	*	1.40		-	75. +1	_			_	7.22E+07		
. 3		33.29	•	1.45			4£ +1					6.53L+07		
3 3 2		101.09		1.50	•		5E+1					5.358+07		
• 30				1.55	4	3.2				1E + 1	_			3.85=-12#
3 3 3			•	1.50	#		2E+1						# 6.166-06*	
8 34		111.35		1.65	•								# 4.29E-J64	
# 39		115.24	•	1.70	•		3F +1						# 2.66E-06*	
3 3				1.75	Ĭ	3.)		-			_		# 2.23[-J6*	
23222	. = 2 2		37.2		**		== = =	. ~ : % 3	1222	32 2 2	22	*******	*****	********

MAXIMUM CONDUCTIVITY # #.01E-03 (MHDS/P)

#POINT27		#POCKET # REDEVE # #FOSITION # 5000(FT)/10(FT/S) # #PPESSURE # 0.832 (ATHOSPHERES#	FREGUENCY # 2.50E+08 # (MZ)
# PAGIAL # INDEX		E# ELECTRON*COLLISION# PLASMA # # DENSITY *FREQUENCY#FREQUENCY# # (1/M3) * (1/S) # (1/S) #	SIGMA + EPSILON # + (MHO/M) + (FD/M) A
• 3	# 0.00 * 0.00 # 3.39 * .05 # 6.76 * .10	# 6.47E+16* 2.45E+11# 2.28E+09# # 6.22E+16* 2.44E+11# 2.24E+09# # 5.08E+16* 2.43E+11# 2.02E+09#	7.18F-03+ 3.82E-12# 5.89E-03+ 8.83E-12#
# 5	# 10.17	# 2.83E+16* 2.41E+11# 1.51E+09# # 9.00E+15* 2.37E+11# 8.52E+0## # 1.81E+15* 2.32E+11# 3.82E+08# # 3.48E+14* 2.25E+11# 1.68E+08# # 6.47E+13* 2.18E+11# 7.22E+07#	1.07E-03+ 8.65E-12# 2.20E-04+ 8.85E-12# 4.35E-05+ 8.85E-12#
9 9 10 11	# 27.11 * .40 # 30.50 * .45 # 33.89 * .50 # 37.28 * .55	# 2.34E+13* 2.10E+11# 4.34E+07# # 4.53E+13* 2.01E+11# 6.05E+07# # 9.63E+13* 1.93E+11# 8.81E+07# # 1.38E+14* 1.84E+11# 1.06E+03#	3.15E-06* 8.85E-12# 6.35E-06* 8.85E-12# 1.41E-05* 8.45E-12#
	# 40.67 * .60 # 44.06 * .65 # 47.45 * .70	# 1.70F+14* 1.76E+11# 1.17E+04# # 1.92F+14* 1.69E+11# 1.25E+04# # 2.05E+14* 1.62E+11# 1.29E+06# # 2.11E+14* 1.55E+11# 1.30E+09#	3.21E-05* 8.85E-12# 3.58E-05* 8.85E-12# 3.83E-05* 8.85E-12#
# 16 # 19	# 54.23 * .40 # 57.52 * .85 # 61.01 * .90 # 64.40 * .35 # 67.79 * 1.00	# 2.11F+14* 1.50E+11# 1.31E+00# # 2.06E+14* 1.44E+11# 1.29E+00# # 1.37F+14* 1.40E+11# 1.26E+00# # 1.66E+14* 1.36E+11# 1.22E+00# # 1.73E+14* 1.32E+11# 1.18E+03#	4.03E-05+ 8.95E-12# 3.97E-05+ 8.85E-12# 3.86E-05+ 8.35E-12#
£ 22 # 23 # 24 # 25	# 71.18 * 1.05 # 74.56 * 1.18 # 77.95 * 1.15 # 81.34 * 1.20	# 1.59F+14* 1.29E+11# 1.13E+08# # 1.44E+14* 1.26E+11# 1.08E+09# # 1.30F+14* 1.24E+11# 1.02E+08# # 1.16E+14* 1.21E+11# 9.65E+07#	3.23E-05+ 6.65E-12# 2.96E-05+ 8.65E-12# 2.66E-05+ 8.65E-12#
0 27 0 25	# 64.73 * 1.25 # 88.12 * 1.30 # 91.51 * 1.35 # 94.90 * 1.40 # 98.29 * 1.45	# 1.02E+14* 1.20E+11# 9.00E+07# # E.09E+13* 1.18E+11# 8.46E+07# # 7.69E+13* 1.16E+11# 7.88E+07# # 6.53E+13* 1.15E+11# 7.26E+07# # 5.49E+13* 1.14E+11# 6.65E+07#	2.13E-05+ 8.85E-12# 1.66E-05+ 8.85E-12# 1.66E-05+ 8.85E-12#
# 31 # 32 # 33 # 34	# 101.6e # 1.50 # 105.07 # 1.55 # 108.46 # 1.60 # 111.45 + 1.61	# 4.50E+13* 1.13E+11# 6.03E+07# # 3.59E+13* 1.12E+11# 5.38E+07# # 2.*0E+13* 1.11E+11# 4.75E+07# # 2.03E+13* 1.10E+11# 4.04E+07#	1.15E-05* 0.65E-12# 9.05E-06* 8.55E-12# 7.11E-06* 8.85E-12#
# 35 # 36 # 37 # 34	# 115.24 * 1.70 # 118.63 * 1.75 * 122.01 * 1.80 # 125.40 * 1.85	# 1.46E+13* 1.13E+116 3.43E+07# # 9.14F+12* 1.09E+11# 2.71E+07# # 9.43E+11* 1.17E+10# 8.72E+G6# # 4.83F+11* 1.17E+10# 6.24E+06#	2.35E-06* 8.85E-12# 2.23E-06* 8.85E-12# 1.15E-06* 8.85E-12#

MAXIMUM CONDUCTIVITY : 7.455-03 (MHOS/M)

#FGINT28/ # 5.40 / # (M)		OFUCKET & REDEYE OF PRESIDENT & SOUD(FT)/10(FT/S) OF PRESSURE & 0.832 (ATMOSPHERES)	FREQUENCY # 2.50E+08 # (HZ) #
# PADIAL	- -	E# ELECTRON*COLLISION# PLASMA # # Density *frequency#frequency# # (1/m3) * (1/s) # (1/s) #	SIGHA * EPSILON # (MHC/M) * (FD/M) #
1 2		# 5.576+16* 2.44E+11* 2.12E+09# # 5.20E+16* 2.44E+11# 2.05E+09# # 3.94E+16* 2.42E+11# 1.78E+09# # 2.64E+16* 2.40E+11# 1.28E+09#	6.02E-03* 8.83E-12# 4.58E-03* 4.84E-12#
5 6 6 6 7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	13.56 * .20 16.95 * .25 20.34 * .30 23.73 * .35	# 6.36F+15* 2.36E+11# 7.16E+88# # 1.40E+15* 2.31E+11# 3.36E+09# # 2.81F+14* 2.25E+11# 1.51E+09# # 5.86E+13* 2.18E+11# 6.97E+07#	1.70E-04* 8.95E-12# 3.52E-05* 8.85E-12# 7.58E-06* 8.35E-12#
# 10 (# 11 (# 12 (# 13 (27.11 * .40 1 30.50 * .45 1 33.39 * .50 1 37.28 * .55 1 40.67 * .60	# 2.06E+13* 2.10E+11# 4.07E+07# # 3.82E+13* 2.02E+11# 5.55E+07# # 6.34E+13* 1.93E+11# 8.20E+02# # 1.21E+14* 1.65E+11# 9.88E+U7# # 1.50E+14* 1.77E+11# 1.10E+0##	5.33E-06* 8.85E-12# 1.22E-05* 8.85E-12# 1.44E-05* 8.85E-12# 2.39E-05* 4.85E-12#
# 15 (# 15 (# 17 (# 44.06 * .65 # 47.45 * .70 # 50.44 * .75 # 54.23 * .80 # 57.52 * .85	# 1.71t+'4* 1.70E+11# 1.17E+08# # 1.54E+14* 1.63E+11# 1.22E+04# # 1.90E+14* 1.57E+11# 1.24E+09# # 1.91E+14* 1.51E+11# 1.24E+08# # 1.81E+14* 1.46E+11# 1.23E+J3#	3.18E-05+ 8.85E-12# 3.42E-05+ 8.85E-12# 3.57E-05+ 8.85E-12#
0 19 0 0 20 0 0 21 0	61.01 * .90 64.40 * .35 67.79 * 1.00 71.16 * 1.05	# 1.816 +14* 1.41E +11# 1.21E +09# # 1.72E + 4* 1.37E +11# 1.18E +03# # 1.51E +14* 1.33E +11# 1.14E +08# # 1.49E +14* 1.30E +11# 1.10E +06#	3.615-05* 6.85E-12# 3.53E-05* 6.85E-12# 3.405-05* 6.85E-12# 3.22E-05* 9.85E-12#
	74.56 * 1.10 77.95 * 1.15 8 81.34 * 1.20 8 84.73 * 1.25 8 83.12 * 1.30	# 1.36E+14* 1.27E+11# 1.05E+06* # 1.23E+14* 1.25E+11# 9.96E+07# # 1.11E+14* 1.22E+11# 9.95E+07# # 9.86F+13* 1.2JE+11# 3.91E+07# # 8.5#E+13* 1.19E+11# 8.36E+07#	2.79E-05+ 9.85E-12# 2.55E-75+ 8.85E-12# 2.31E-05+ 8.85E-12#
# 29 (# 30 (# 31 (# 91.51 * 1.55 # 94.30 * 1.40 # 93.29 * 1.45 # 101.68 * 1.50	# 7.56: +13* 1.170+11# 7.816+07# # 6.526+13* 1.166+11# 7.250+07# # 5.566+13* 1.156+11# 6.596+07# # 4.63 +13* 1.136+11# 6.116+07#	1.62E-JS* 8.85E-12# 1.59E-05* 9.35E-12# 1.37E-05* 8.85E-12# 1.15E-35* 4.85E-12#
# 34 # 35	# 105.07 * 1.55 # 105.46 * 1.60 # 111.35 * 1.65 # 115.24 *70 # 118.63 * 1.75	# 3.32E+13* 1.12E+11* 5.35E+07* # 3.04E+13* 1.12E+11* 4.95E+67* # 2.36E+13* 1.11E+11* 4.36E+07* # 1.75E+13* 1.19E+11* 3.75E+07* # 1.20E+13* 1.10E+11* 3.11E+07*	7.68E-06* 8.95E-12# 5.98E-06* 8.95E-12# .46E-JE* 3.85E-12#
# 57 # 53	# 122.01 * 1.50 # 125.40 * 1.85	# 6 sm 4F +124 3. 23E +10# 2. 32E+07#	

MAXIMUM CUNCUCTIVITY & F.435-08 (MHGS/M)

22	****** 01NT29		######################################	F	ACIUS	2 2 2 2 4 1	10C	* * * (F T	***	*** ! R	ERR For	8 2 % () V F		3 2 2 3	*===:	FREQUE	MCV PON
•	5.60				-02							. –	/11	D (F	T/S)	_	_
	(H)			(4)									-		HERESI		
==	*****	=	******	224	48888==	==:	***	* * *			2 2 3		#1				********
•	RADIAL		RELATIV	E*	AESCLI	Εø	ELE	ECT	RON	+ CO	LLI	AOI 2		FL	ASHA (SIGHA .	EPSILUN #
•	XJCNI		RACIUS		RACIUS	•	DE	151	TY	* FP	EQU	ENCY	#F	REGI	JENCY	*	
•		•		•	(F)	•	()	L / P 1	3)	•	(1/	S)	•	(1	/S) (* (HNOHH) *	(FO/H) #
* =	*====	=	=====×	2 2 1	*****												F#######
	1	•	0.00	*	0.00											5.26E-03*	_
•	2		3.39	#	.05											1 4.79E-03*	
•	3		6.78	*	•10							_				3.42E-03+	
•	4		10.17	*	.15					-						1.69E-03+	
•	5		13.56	*	.20								-			5.30E-04*	
	6 7	,	16.95	•	.25		-									1.30E-04+	
-	-	_	20.34	*	.30 .35						-					2.84[-05* 6.73E-06*	
7	9	ï	27.11	•	•40											7.32E-06*	
-	10		30.50		.45											J.56E-06*	
4	11		35.89		.50					-						8.93E-06+	_
ä	12	ě	37.28		.55					_		_			_	1.516-05	
	13	ā	40.67	•	.60											2.05E-05*	_
	14	•	44.06	*	•65											2.48E-054	
•	15	ě	47.45		.70											* 2.02E-05*	
	16				.75											3.06E-05+	
	17		54.23		.80											3.21E-J5+	
	1.5	•	57.62	•	.85				_	_			-	_		3.30E-05+	
	19	#	61.01	•	.90		1.0	576	+14	* 1	.45	E+11		1.1	6E+03	1 3.29E-05*	8.858-12#
	20		64.46	•	•95		1.	346	+14	* 1	. 33	E+11		1.1	3E+09	3.24E-05*	8.95E-12#
	21		67.79	•	1.00		1.	505	+14	* 1	. 35	E+11	L#	1.1	GE+04	3.14E-US+	8.85E-12#
•	22	ø	71.18	#	1.05	•	1 .	3 9 E	+14	- 1	. 31	E+11		1.0	6E+0c	2.99E-05*	6.85E-12#
	23	#	74.56	*	1.10		1.	29E	+14	* 1	. Z 5	E+11		1.0	2E+88	2.02E-05*	8.456-12#
	24	#	77.95	*	1.15											# 2.63E-05*	
#	25	#	41.34	•	1.20											1 2.42E-05*	
•	26	#	84.73	•	1.25			-		_			-			2.21E-05+	
	27	ě	35.12	•	1.30					_			-			1.99E-054	
•	25	#	91.51	*	1.35				_	_	_		-			1.77E-05*	_
7	٤٦		94.90	*	1.40											1.57E-05*	
-	30		33.29	*	1.45											# 1.36E-95*	
F	31	•	101.68	_	1.50											1.17E-JS+ 5.9CE-06+	
-	32 33		105.47 105.46		1.55 1.60											8.15E-06*	
#	33 34		77.	•	1.65											# 5.59E-06*	
	35		115.24		1.70					_			_			5.06E+06+	
ě	36		115.63		1.75											3.762-06+	
•	37	ě			1.00		_						_			2.59E-06*	
•	38		125,46		1.85											1.54E-06*	
	30		128.79	•	1.90				_	_			_			# 1.15E-06*	
==	=====	=	E1E31151			E T	*==		222	- Z =	= = =					********	

MAXIMUM CONCUCTIVITY # 5.26E+03 (MHCS/F)

The second secon

= :		*********	*******		*************	*****************
	FOINY30	MOZZLE	PACIUS #1	FOCKET .	REDEVE	FREGUENCY #
	F.80	# 1.45	C-02 #	FOSITION :	5000(FT)/10(FT/S) 4	2.50E+08 #
¢	(H)	# (1.1			0.832 (ATMOSPHERES	
2				********	*************	************
	RADIAL	# PELATIVE*	APSCLUTE#	ELECTRON*	COLLISION PLASMA	SIGHA + EPSILON #
	INDEX				REQUENCY PEREQUENCY	
			(R) #	(17H3) A		(MHO/M) + (FD/M) •
= :			*********			- · · · - · · · · · · · · · · · · · · · · · · ·
	1	. 0.00 *	0.00	3.44F4160		4.30E-034 5.84F-124
-	خ	# 3.59 *				3.54E-03+ 5.54E-120
-	3	# 6.78 *	.10			2.38E-03* 3.84E-12#
-	4	# 10.17 *				1.13E-J3+ 0.05E-120
-	5	# 13.56 *	- .			3.58E-14* 8.85E-12#
-	G	# 16.95 *				9.75E-U5+ 8.85E-12#
-	7	# 20.54 *			-	2.27E-05* 0.85E-12#
7					· · · · · · · · · · · · · · · · · · ·	
•	h					5.99E-06* 8.85E-12#
	3		_		_	1.876-064 8.856-124
7	10		.45 #	• •	- · ·	1.538-084 0.458-124
	11	# 33.89 *	•50 #		- · · · · · · · · · · · · · · · · · · ·	5.22E-06* 8.85E-12#
-	12	# 37.2F +		-		1.16E-05+ 3.85E-12#
	13		•6C #			1.71E-05* 5.95E-12#
•	14	# 44.06 *	.65			2.15E-05* 8.85E-120
	15	# 47.45			- · · · ·	2.495-35+ 8.855-126
	16	# 50.84 4	.75		· · · · · · · · · · · · · · · · · · ·	2.73E-05* 5.45E-12A
	17	# 54.23 *	• 90 #	· · · · · -		2.d9E-05+ 8.45E-12#
	15	# 57.62 *	•85 #		1.49E+11# 1.13E+08	
÷.	19	# 61.01 *	.90 #	_		3.01E-05* 8.85E-12#
•	50	# 64.46 *	.95 #			2.97E-05+ 8.85E-12#
	21	# 67.75 *	1.00 #	-	· · · · · · · · · · · · · · · · · · ·	2.90E-05* 9.45E-12#
	22	# 71.19 *	1.05 #			2.765-05* 8.855-12#
•	23	# 74.5F *	1.10 #			1 2.64E-054 0.45E-124
	24	# 77.35 *	1.15		1.27E+11# 9.43E+07#	
	25	# 81.34 *	1.20 #			2.30E-05* 8.35E-12#
	26	* 54.73 *	1.25 #			2.11E-05* 3.35E-120
	27	# 43,12 *	1.30 #		1.20E+11# 8.13E+074	
	29	# 91.51 *				1.72E-05* 8.85E-12#
#	2 1	# 94.30 *	1.49 #		· · · · · · · · · · · · · · · · ·	1.54F-35* 8.85E-12#
	30	# 49.24 *			1.16E+11# 6.69E+07#	
	31	# 161.66 *	1.50 #	4. ~1E +1 3*	1.15E+11# 5.22E+074	1.12E-054 d.55E-12#
	32	# 105.07 *	1.55	4,080+13*	1.14E+11# 5.73E+076	1.01E-05- 8.85E-12#
	3.3	# 106.46 *	1.60 #	3.42F+13#	1.13E+11# 5.25E+07#	# 8.53E-06* 8.85E-12#
•	34	# 111.85 *	1.65 #	2.805+134	1.126+11# 4.756+37#	
	35	4 115.24 *	1.70 #	2.222+13*	1.11E+11# 4.25E+07#	5.63E-05+ 6.85E-12#
	36	# 119.53 *	1.75 #	1.725+13*	1.115+11# 3.726+074	4.38E-064 8.85E-12#
	37	* 122.01 *	1.00 #	1.220+13*	1.13E+11# 3.13E+07#	3.12E-U6+ 3.35E-12#
	3 3	# 125.40 *	1.85 #	#.31E+12#	1.09E+11# 2.59E+074	. 2.14E-06* 5.35E-12#
	39	# 123.79 *	1.90 #	4.16(+12*	1.02E+11# 1.95E+076	1.15E-06+ 8.85E-12#
3	**=====	=======================================	========	=======================================		*****************

MAXIMUM CONCUCTIVITY # 4.305-03 (MHCS/M)

*******			***************
CFGINT31	MOZZLE RACILS	#FOCKET REDEYE	FREQUENCY #
# 6.00	# 1.48t-02	#POSITION # 5000(FT)/10(FT/S) #	2.50E+08 •
# (M)	Ø (H)	PPFESSURE : 0.832 (ATHOSPHERES)	(HZ) #
*******	***********	*********************	***************
# RADIAL	# RELATIVE* ABSCLUT	:# ELECTROR*COLLISION# PLASHA #	SIGNA + EPSILON #
# INDEX	# RACIUS * RACIUS	# DENSITY *FREQUENCY#FREQUENCY#	•
•	# (r)	# (1/M3) * (1/S) # (1/S) #	(MHO/M) + (FD/M) #
*******	***** *******	************************	******************
• 1	• 0.00 • C.00	# 2.43E+16* 2.41E+11# 1.41E+09#	2.90E-03+ 8.34E-12#
9 2	ø 3.39 + .05	+ 2.16E+16* 2.41E+11# 1.32E+09#	2.53E-03* 6.84E-12#
9 3	# 6.78 * .10	# 1.41E+16* 2.39E+11# 1.07E+39#	1.66E-03+ 8.55E-12#
# 4	# 10.17 * .15	# 6.59E+15+ 2.37E+11# 7.29E+0##	7.83E-04* 8.85E-120
# 5	# 13.56 * .20	# 2.12£+15* 2.34E+11# 4.14E+08#	2.56E-04+ 8.85E-12#
• 6	# 16.95 * .25	# 6.10E+14* 2.29E+11# 2.22E+08#	_
# 7	# 20.34 * .30	# 1.47E+14* 2.23E+11# 1.09E+096	
₽ 8	23.73 .35	# 4.05E+13* 2.17E+11# 5.72E+07#	
# 3	# 27.11 * .40	# 1.23E+13+ 2.10E+11# 2.15E+07#	
# 10	# 30~50 * .45	# 9.22E+12* 2.03E+11# 2.73E+07#	-
• 11	# 33.89 * .50	# 2.91E+13* 1.35E+11# 4.84E+07#	
12	# 37.29 + .55	# 6.46E+13* 1.89E+11# 7.22E+071	
# 13	# 40.67 * .60	# 9.356+13* 1.8UE+11# 8.58E+07#	-
14	# 44.06 * .65	# 1.15E+14* 1.73E+11# 9.63E+074	
1 5	# 47.45 * .70	# 1.30E+14# 1.67E+11# 1.02E+08#	
16	# 50.84 4 .75	# 1.39F+14* 1.61E+11# 1.06E+08#	
0 17	# 54.23 * .80	# 1.44E+14* 1.55E+117 1.08E+094	_
# 13	# 57.62 * .95	# 1.44E+14* 1.50E+11# 1.08E+08	
19	# 61.01 * .90	# 1.42E+14* 1.45E+11# 1.07E+034	
# 20	# 64.40 * .95	# 1.37E+14* 1.41E+11# 1.05E+084	
# 21	# 67.79 * 1.00	# 1.316+14* 1.376+11# 1.036+08#	
22	# 71.19 # 1.05	# 1.23E+14* 1.34E+11# 9.97E+076 # 1.15E+14* 1.31E+11# 9.62E+076	
# 23 # 24	# 74.56 * 1.10 # 77.95 * 1.15	# 1.05C+14* 1.25E+11# 9.24E+074	
		# 9.79E+13* 1.25E+11# d.34E+074	
# 25 # 25	# 81.34 * 1.20 # 84.73 * 1.25	# 8.81E+13* 1.23E+11# 8.43E+076	
# 27	# 83.12 * 1.30	# 7.94E+13+ 1.21E+11# 8.00E+074	
# 28	# 31.51 * 1.35	# 7.03E+13# 1.13E+11# 7.56E+07#	
# 29	# 94.90 * 1.40	# 6.29E+13* 1.18E+11# 7.12E+074	
# 30	# 93.25 * 1.45	# 5.51t+13* 1.17E+11# 6.67E+07	
# 31	# 101.6 ^a + 1.50	# 4.91E+13* 1.15E+11# 6.23E+07#	
• 32	# 105.07 * 1.55	# 4.12E+13* 1.14E+11# 5.77E+07#	
# 33	# 103.46 # 1.60	# 3.52E+13* 1.13E+11# 5.32E+076	
• 34	# 111.65 * 1.65	# 2.92E+13* 1.12E+11# 4.95E+07	
# 35	* 115.24 * 1.70	# 2.40F+13* 1.12E+11# 4.40E+07	
8 36	# 119.63 * 1.75	# 1.91E+13* 1.11E+11# 3.93E+076	
# 37	# 122.01 * 1.60	# 1.46E+13* 1.1JE+11# 3.43E+07	
. 39	# 125.40 + 1.85	# 1.05E+13* 1.10E+11# 2.92E+07	
# 39	# 128.79 * 1.99	# 1.25E+12# 3.06E+10# 1.00E+07	
2213333	*************		

MAXIMUM CONDUCTIVITY 1 2.90E-03 (MHOS/M)

=	222322	=======================================				
	FOINT 52	# NCZZLE	RACILS (#ROCKET :	REDEVE	FREGUENCY #
	6.20	# 1.48	3E-02	#FOSITION :	5000(FT)/10(FT/S) (
#	(81)	# (1	1)	#FFESSURE #	0.832 (ATMOSPHERES!) (HZ) #
#	======			=======================================		*****************
#	RADIAL	# RELATIVE	ABSCLUTE	# ELECTRON#C	COLLISION# PLASMA (SIGHA - EPSILON #
	INDEX	# RACIUS	RACIUS (# DENSITY *F	REQUENCY#FREQUENCY	• •
		•	· (M) (# (1/M3) *	(1/S) # (1/S) (* (MHO/M) * (FD/N) *
=	# L = E = 2 = 1	********			. 65 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	**************
	1	# 0.00	0.00	# 1.71E+16 *	2.40E+11# 1.17E+096	2.00E-03+ 8.85E-12#
#	2	# 3.39	• 05	# 1.47E+16*	2.40E+11# 1.09E+096	1.73E-03+ 5.85E-12#
	3	# 6.74	• 10 1	# 9.45E+15#	2.38E+11# 8.73E+086	1.12E-03+ 5.85F-12#
#	4	# 10.17 4				# 5.28E-04* 8.85E-12#
#	5	# 13.56 4				1.82E-04* 6.85E-12#
#	5	# 16.95				5.72E-05* 8.85E-12#
#	7	# 20.34 4				1.51E-05* 0.65E-12#
	8	# 23.73 4				# 4.61E-06* &.85E-12#
	9	* 27.11 4				# 1.49E-06+ 3.85E-12#
	10	# 30.50 4				1.09E-06* 8.85E-12#
	11	# 33.89 4				# 3.41E-06+ 8.85E-12#
#	12					6 3.19E-06* 8.85E-12#
#	13	# 40.67 4				F 1.26E-05+ 8.85E-12#
#						# 1.63E-05+ 8.85E-12#
#	15	# 47.45 4				1.94E-05+ 8.85E-12#
#	16					# 2.18E-05* 8.85E-12#
#	17	# 54.23 4				# 2.35E-05+ 3.35E-12#
#						# 2.47E-05* 8.85E-12#
#	-					2.53E-J5* 0.85E-12#
#		" J				# 2.52F-75* 8.85E-12#
#		# 67,79	1.00	# 1.22E+14*	1.39E+11# 9.92E+07	# 2.49E-05+ 6.85E-12#
#						# 2.42E-05* 8.95E-12#
#		# 74.56				# 2.32E-05+ 8.85E-12#
#			1.15			# 2.21E-05# 8.85E-12#
	_	" (1004				# 2.07E-85+ 8.85E-12#
#						# 1.92E-05* 8.85E-12#
#	-	# 38.12				# 1.77E-05+ 8.85E-12#
#		# 41.51	1.35		1.20E+11# 7.46E+07	
#		# 94.30	1.40	. – . –	1.19E+11# 7.05E+07	
#			1.45		1.17E+11# 6.63E+07	
#						# 1.16E-05+ 8.85E-12#
7		" 10,00.	1.55			# 1.32E-35# 8.85E-12#
#	33		* 1.60 * 1.65			# 9.36E-06+ 8.95E-12# # 7.54E-06+ 8.85E-12#
#			1.03		1.13E+11# 4.34E+07	
#			1.70 1.75			# 6.38E-164 8.85E-12#
#						# 5.23E-06* 8.85E-12#
# ע						# 4.20E-06* 8.85E-12# # 3.19E-06* 8.85E-12#
#			1.35		1.10E +11# 3.17E+07	
#			* 1.90	# 4.1U% *12*	# 4 1 CE + 1 H	# 2.89E-06+ 8.95E-12#
#	47	# 132.16	1.95	F 2.49L+12*	4.100 +10# 1.736+0/	# 1.95E-06* 8.55E-12#

MAXIMUM CONGUCTIVITY & 2.00E-03 (MHOS/M)

# 1	*****	2 2	2222222	##	=======================================	==:		28	* * * * * * * * * * * *	:::::::::::::::::::::::::::::::::::::::	********	********
#1	POINTS	3 #	NCZZL	E	FACILS	# 6	POCKET	ı	PEDEYE	4	FREQU	ENCY #
	5.40				E-02					/10 (FT/S)		
-	(M)	-		(H)	-					MOSFHERES		
											· ·	
= :			*******								*=======	
	RADIA	_							COLLISION			EPSILON #
	INDEX	#	RACIUS	•	PACIUS	#	DENSITY	#	FREQUENCY	PFREQUENCY (•	
		#		#	(۲)	#	(1/M3)	#	(1/S)	! (1/5) (F (MHC/M) *	(FD/M) #
2:	22222	3 Z	2222222	32	=======================================	Z = :		:		:22222223	*********	=======================================
	1	#	0.00	#	0.00		1.09E+1	6#	2.33E+116	9.36E+0A4	1.28E-03*	8.85E-12#
	2		3.39	4	•05		9-31E+15	5#	2.38E+116	6.66E+0#4	1.10E-03*	8.85E-12#
	3	4	6.78		.10		5.98E+19				7.10E-044	
-	4	-	10.17		.15						3.43E-04+	
7	5			#	.20		1.05E+1				1.28E-04*	
#		7	13.56									
₹	6		16.95	*	.25		3.46E+1				4.29E-05+	
#	7		20.34	#	.30		9.59E+1			6.79E+076		8.85E-12*
#	8	#	23.73	*	.35	#	3.098+1			4.99E+071		
#	9	#	27.11	#	• • 0	#	1.03E+1	3#			1.38E-06*	
	10		30.50	*	• 45	#	6.745+17	2*	2.03E+11	2.33E+07/	9.36E-07#	3.85E-12#
	11.		33.89	-	•50	#	1.94E+1	3*	1.96E+114	3.96E+874	\$ 2.79E-06*	8.85E-12#
	12		37.28	#	.55	#	4.69E+1	3*	1.89E+11	6.15E+074	7.00E-06*	8.85E-12#
4	13		40.67	#	.60	#	7.03E+1				1.09E-05*	
-	14	-	44.06		.65		8.91E+1				1.43E-05*	
×	15	*	-				1.03E+1			9.11E+07		8.85E-12#
#		7	47.45		.70							8.85E-12#
#	16	7	50.84	#	•75	#	1.13E+1			9.53E+07		
	17		54.23	#	• 90		1.1cE+1				2.12E-05+	5.85E-12#
#	19	#		+	. 85		1.21E+14				2.24E-05*	8.85E-12#
#	19		61.01	#	•90	#	1.21E+1	4*			# 2.31E-05*	8.85E-12#
	20	#	64.40	*	•95	#	1.18E+1	4 #	1.43E+11	1 3.76E+071	* 2.32E-05*	8.85E-12#
#	21	#	67.79	#	1.00	#	1.14E+14	4#	1.59E+11	# 9.58E+071	# 2.30E-05*	8.85E-12#
	22		71.18	*	1.05	#	1.09E+14	4#	1.36E+116	# 9.37E+07#	1 2.26E-05*	8.85E-12#
#	23	#	74.56	*	1.10	#	1.026+1			9.09E+076		8.85E-12#
	24		77.95	*	1.15	#	9.57E+1				2.08E-05*	8.85E-12#
	25			*	1.20		8.56E+1				1.96E-05*	8.85E-12#
-	26	#			1.25	-	6.14E+1			8.10E+07	= -	8.85E-12#
- W						-						
#	27	#		*	1.75		7.42E+1.				1.70E-05*	8.85E-12#
Ŧ	28			*	1.35						1.56E-05+	8.85E-12#
#	29	#		*	1.40	#					1.42E-35*	8.95=-12#
#	30	#	99.29	•	1.45	#	5.38E+1.				1.29E-05+	8.85E-12#
#	31	#	101.68	*	1.50	#	4.75E+1	3+	1.17E+114		1.15E-05*	6.85E-12#
#	32	ø	105.07	#	1.55	#	4.17E+1.	3*	1.15E+11#	\$ 5.80E+071	1.02E-05+	8.85E-12#
#	35	#	108.46	*	1.60	#	3.62E+1.	3#	1.148+114	5.40E+076	# 8.90E-064	1.85E-12#
#	34	#	111.85		1.65		3.11E+13	3#	1.13E+11#	5.01E+07	7.73E-06+	8.355-12#
#		#	115.24		1.70	#					6.60E-06+	
	36		119.63	*	1.75						5.54E-064	
#	37		122.01	*	1.80						# 4.58E-J6+	
W	3 f		125.40	*	1.95						3.62E-06*	
.# .#												
#	39		129.79	*	1.90						1 2 42E-06*	
#	40		132.16	#	1.95						2.00E-06*	
#	41		133.57	*							1.56E-06*	
= :	=====	= =	=======	==:	=======	= = :	========	2 2		:======::::	:	222222222

MAXIMUM CONDUCTIVITY : 1.265-03 (MHOS/M)

3 1	*****	# #	******	# # #				***		1 2 2 2	212	2221			*********	********
	OINTS	4#	NOZZI	LE I	FACIUS		FOCK	ET		RE	DEY	E			# FREGU	ENCY #
	6.60		1	.48	E-02	#	FOSI	TIO	N :	50	306	FTI	100	FT/S)	2.50	E+09 #
	(M)			(H)									PHERES		
3 1		3 E	#######	2 £ 2 £	******			323			222				******	********
	RADIA	L#	RELATI	VE-	ABSOLUT	E#	ELE	CTR	04	COL	LIS	ION) P	LASHA	# SIGMA #	EPSILON #
	INDEX		RACIUS											QUENCY		4
Ā				. *	(M)	#		/M3			1/5				6 (MHC/M) *	(FD/M) 8
= :		= =	======	===	=======	 	 ::::	222	**	, ::::::	122				********	
ě	1		0.00	*	0.00	4	7.1	FF +	154	2.	LAF	4111	t 7.	706+1) N	# 8.72E-94*	8.85E-12#
	ž	4	3.39	•	.05										7.50E-04*	
Ä	3	-	5.7A	*	.10										4.96E-04*	
	4		10.17		.15			_		-					2.45E-04*	
4	5	-	13.56		.20										# 3.55E-05*	
-	6	-	16.95		.25										\$ 3.36E-05*	
*	7	4	20.34	•	.30										# 1.02E-05+	
<u> </u>	9	*	23.73		.35											
- T	9		27.11		.40										8 3.52E-06*	
-	10	#	37.50												# 1.26E-06#	
7		-			•45							-			# 8.23E-07+	
*	11 12	#	33.9⊊ 37.2€	#	•50 •55					_					# 2.35E-06*	
- T		7		*											6.14E-06+	
7	13	*	40.67		.60					_	_				# 9.67E-06*	
7	14	#	44.06	*	•65					-					# 1.28E-05#	
#	15	#	47.45	#	.70						-				# 1.55E-05+	
#	15	#	50.84	#	.75										# 1.76E-05#	
#	17	#	54.23	*	• 50									-	# 1.93E-U5#	
#	18	#	57.62	*	.85										# 2.05E+35*	8.85E-12#
#	19	#	51.61	#	.90							-		-	# 2.12E-05*	
#	20	#	64.40	*	.95										# 2.15E-05*	
#	21	#	67.79	*	1.00										# 2.14E-05+	
	22	#	71.18	*	1.05										# 2.115-054	
	23	#	74.56	#	1.19			_							# 2.05E-05*	
#	24	#	77.95	#	1.15										# 1.96E-05+	
	25	#	81.34		1.20										# 1.86E-95+	
#	26	#	54.73	#	1.25								-		# 1.75E-0F+	8.85E-12#
#	27	#	88.12	*	1.30		_				-				# 1.63f-35*	
#	25	#	91.51	*	1.35										# 1.51E-05+	3.35E-12#
#	29	#	94.90	*	1.40							+114			# 1.38E-05#	
#	30	#	33.29	#	1.45					_					# 1.26E-05*	
#	31	*	101.66	*	1.50										# 1.13E-05+	3.05E-12#
#	32	#	105.07	*	1.55										# 1.01E-05*	8.85E-12#
#	33	#	103.45	#	1.60				_						# 8.89E-06*	8.35E-12#
#	34	#	111.65	*	1.65										# 7.50E-06+	8.956-126
#	35		115.24	•	1.70										# 6.71E-06+	
#	36		113.63	#	1.75										# 5.745-36+	
#	37		122.01	#	1.60				_	-					# 4.8GE-36*	
#	3 9		125.40	*	1.65									-	# 3.94E-16-	
#	39		120.79		1.90										# 3.15' 06*	
#	40		132.16	*	1.95										# 2.40E-06*	
#	41		135.57	*	5.00					-					# 1.95E-06*	
= :	=====	= =		===		==	====	::::	===	::::	===	===:	====	======	=======================================	========

MAXIMUM CONCUCTIVITY : 5.728-04 (MH35/M)

2				223	******	## 1						********	********	********
4	FOINT	350	NOZZ	LE A	ACIUS		OCK	ET	1	REDEY	E		FREQUE	NCY #
ï	6.8	-		.485			-				_	/16(FY/S) #	2.506	
•		•		(H)								MOSPHERES	(H2	
	22222			, 2255		**:		UE 2 2:		22222				.,
4		Al s	RF: ATT	VF+	AESCLUT	F ű	FIF	CTAD	h# (21 110	TON	PLASHA #	SIGMA *	EPSILON #
4				. –		-			-			FREQUENCY	*	4
•	_	^ 🖁	NAC 10	J .	(4)	-		/H31		(:/5			(NHC/H) +	(FD/H) #
		₩ 200			(7) ######	 			• • •	1273	, ,	, (1/3/ 4	1000000	150767
7			0.00		0.00		· •	75 4 4 1	 	2 776			5.64E-04*	4 AEE-124
	1	#		*										
•	2				• 0 5								4.67E-044	
	3		6.76	•	•16		_	9E+1	_			4.66E+09#		8.85E-12#
-	4		10.17		•15			7E+1	-				1.66E-04*	
•	5		13.56		• 20			8E +1				2.14E+08#		8.85E-12#
4	, 6				•25			3E -1				1.29E+03#		8.85E-12#
4	7	#			•30	#	6.7	0E 41	3+				8.55E-06*	
á	<i>;</i> 9		23.73	*	.35		2.3	5E +1.	3*			# 4.35E+07#		8.85E-12#
4	, ,	#	27.11	-	• 40	#	8.7	4E + 1	2*	2,09E	+11/	\$ 2.65E+07#	1.18E-06*	8.556-12#
-	10	#	30.50	-	.45	#	5.2	0E +1	2*	2.03E	+11(₽ 2.05E+07#	7.22E-07*	8.85E-12#
4	11	#	33.89	#	•50	#	1.5	6E+1	3*	1.96E	+11%	3.32E+07#	1.96E-06*	8.85E-12#
1	12	#	37.26	#	•55		3.6	21 +1	3*	1.908	+11	5.40E+07#	5.36F-06*	8.85E-12#
4	13		40.67	#	•60	#	5.5	8E+1	3+	1.83E	+116	# 6.71E+07#	8.59E-06*	8.85E-12#
1	14	#	44.06	*	•65	#	7.1	9E+1	3*	1.77E	+11/	7.61E+07#	1.15E-05*	8.85E-12#
4	15			*	.70	#	8.4	4E+1	3#	1.71E	+114	8.25L+J7#	1.39E-054	8.85E-12#
4	16		50.84	*	• 75	#	9.3	4E+1	3#	1.65E	+111	# 8.68E+07#	1.60E-05+	8.85E-12#
4	17				. 80			4E+1				8.95E+07#		8.85E-12#
4	18		57.62		• 95			3E+1				9.10E+07#		J.85E-12#
-	19	- 4	61.01		-90			4E+1				3.15E+07#		8.85E-12#
i	50			4	•95	#	-	3E+1				9.10E+07#	-	8.85E-12#
ì	21	•			1.00	-		BE+1				3.98E+07#		8.85E-12#
7	55				1.05	#		3E +1				8.51E+07#		9.85E-12#
7	23				1.10	- 4		8E+1				3.60E+07#	-	8.85E-12#
- 1	24				1.15	#		5E+1				8.35E+07#		8.65E-12#
- 7						-		9E+1		1.29E			1.77E-J5+	8.85E-12#
	25				1.20	*		_						_
4	26				1.25			ùE+1		1.27E			1.675-05*	5.95E-12#
1	27				1.30	*		11E+1				7.46E+07#		5.65E-12#
1	28				1.35	#		25+1				* 7.145+07#		8.85E-12#
1	59			*	1.40	#		4E+1		1.21E			1.34E-05*	8.85E-12#
1	30		33.29		1.45	4		3E +1				6.46E+07#		8.95E-12#
1	31				1.50	#		4E+1				6.11E+07#		8.35E-12#
-	32				1.55	#		2E+1		1.17E			9.96E+06*	8.85E-12#
:					1.60	#		3E+1				* 5.41L+07#		8.855-12#
1	34	4	111.95	•	1.65			. SE +1					7.83E-06+	8.85E-12#
4	35	Ħ	115.24	*	1.70								6.80E-06+	
1	F 36	4	114.63	•	1.75	#	2.3	EE +1	3*	1.13E	+11(# 4.36E+J7#	5.89E-J6*	3.35E-12#
•) 37		122.01	-	1.80	#	1.9) = E + 1	3 *	1.12E	+114	# 4. 00E+07#	4.99E-06*	3.85E-12#
1	5 9	#	125.40	#	1.85								4.19E-06*	
4	¥ 39		128.79		1.90								5.42E-06*	
4	¥ 40		1 1 5 2 . 1 9		1.95	#	1.0	7E +1	3#	1.1JE	+114	# 2.33E+07#	2.73E-36*	8.65E-12#
4	41	4	135.57	*	2.90								2.09E-06+	
1			138.95										1.82E-06*	
1			142.35		2.10								1.31E-06+	
:														

MAXIMUM CONDUCTIVITY : 5.64E-04 (MH05/M)

#:		# #	******	2251		E 2 :					********	
41	ETHIO	F #	NO 2 71	1 F S	RACILS	4	ROCKET	•	REDEYE		FREGUE	NCA 4
	7.00				-02				5000(FT)/	10(FT/S) #		
ä	(H)	ē	-	(H)					0.832 (AT			
		= =	******	2 2 2 1		 	*******		********		********	
	RADIA	L#	RELATIV	VE#	ASSCLUT	E	FLECTRON		COLLISIONS	PLASMA #	SIGNA .	EPSILON .
	INDEX	-	RAGIUS						FREQUENCY			3
•				•	(4)	ě	(1/H3)		(1/S) #		(MHC/4) *	(F0/H) #
*	*****	: :	222322	***	*****		******	: =	222222222			********
	1		0.00		0.00		2.34E+15		2.35E+110	4.A7E+08#	3.52E-04*	A. ASF-128
	ž		3.33	•	.05		•		2.35E+11#		-	8.85E-12#
	3	ä	6.78	•	.16		1.73E+15			3.73E+03#		9.45E-12#
	4		10.17	•	.15		9.19E+14					8.85F-12#
	5		13.56		.20		4.99E+14			1.81E+00#		8.85E-12#
	Ē,		16.95		.25			-	2.25E+11#			9.85E-12#
	7		30.34	#	.30		5.61E+13				7.18E-96+	8.85E-12#
	3		23.73		.35		2.03E+13		_	4.04E+07#		8.85E-12#
	3		27.11		.40		7.988+12		_	2.54E+0/#	•	8.85E-12#
	1)		30.50		.45		4.56E+12					3.95E-12#
	11		33.89	*	.50		1.138+13	_	1.96E+11#			8.85E-12#
ä	12		37.28	#	.55		3.19E+13		• • • • • • • •		4.73E-06+	8.85E-12#
	13	#			.60	ě	4.98E+13	-	1.84E+11#			3.85E-12#
	14		44.06	*	.65		6.48E+13			7.232+07#		8.85E-12#
	15		47.45	4	.70		7.66E+13			7.86E+07#		8.55E-12#
ä	16		50.84		.75		8.535+1			8.29E+07#		8.55E-12#
ā	17				.90	4	9.12E+13		1.60E+11#			8.55E-12#
	13		57.52	#	.85	ä	9.47E+13			3.74E+07#		3.85E-120
ä	19		61.01		.90		9.62F+13				1.80E-05*	8.85E-12#
•	20	#		*	.95	#	9.5 E+1			8.79E+07#		8.35E-12#
	21	#		*	1.00		9.37E+1			8.69E+07#		8.55E-12#
	22	#	_		1.05	#	9.07E+13		_		1.84E-05=	8.85E-12*
	23		74.55	*	1.10		8.695+13			8.37E+07#		8.855-12#
*	24	#	77.95	#	1.15	#				8-14E+07#		8.855-12#
	25	#	51.34	#	1.20	#	7.738+13	-		7.896+07#		8.95=-12#
	25		54.73	#	1.25	#	7.205+13			7.625+07#		3.85E-12#
	27		33.12	•	1.30	#	6.666+13		_	7.33E+17#		9.85E-12#
	28		31.51		1.35		6 . 1 2E +13			7.026+07#		8.455-12#
	29	#	34.90		1.40	#	5.536+13		_	6.71E+07#		0.85E-12#
#	31	#	98.29	¥	1.45	#	5.07E+13					5.35E-12#
	51		131.68	*	1.50	#	4.578+13			6.07E+07#		8.85E-12#
	32	#	105.07	4	1.55	#	4.08E+1		1.1/E+11#			8.35E-12#
#	33	*	108.46	*	1.60	#	3.635+13		1.16E+11#			8.855-12#
#	34	#	111.45	#	1.55	#	3.19++13		1.15E+11#		7.426-96#	8.85F-12#
#	35	#	115.24	#	1.70						6.dyE-J6+	
#	36		119.63	•	1.75						6.30E-06*	
#	37		122.01	*	1.90						5.15E+36#	
#	38		125.40	*	1.35			_			4.53E-06#	_
ø	39		123.79		1.90			-			3.62E-16*	· · · · · — —
	40		132.15	-	1.95						2.995-06+	
#	41		135.57	•	2.00						2.355-16-	
	42		135.36	4	2.65						1.82E-06*	
#	43		142.35	*	2.10						1.31E-06*	
			_	====							=======================================	

MAXIMUM CONDUCTIVITY : 3.528-04 (MHOS/M)

THE REPORT OF THE PROPERTY OF

	2 * * * * *	2		22:	******	= = 1		***	===	22	* * * *		==:		********	********
#1	FOINT3	7#	NOZZL	E F	RACIUS		ROCK	ET		R!	EDE	E			# FRE	GUENCY #
	7.24		1.	436	-02	#1	POSI	110	N I	51	000	(FT)	/10	O(FT/S)	. 2.	50E+08 #
•	(H)			(H)			FRFS	SUR	E I	0	. 83	2 (A	TH	OSFHEFES		(HZ) #
=		= =	******	**1	******	2 # 2	: 2 2 2	122	220	22	2 2 2 :	* # # #	221		******	*********
	PADIA	L#	RELATIV	E#												+ EPSILON #
•	INDEX		RACIUS		FACIUS		DEN	SIT	٧ *	FR	EQU	ENCY	#FF	REQUENCY	'#	• •
•					(4)		(1	/M3) +	•	(1/	5)	#	(1/5)	# (MHC/M)	* (FD/H) #
=		3 2	222222	Z # 1	*******	2	====	===	***	**	3 3 3:	===	**:		********	*********
#	1		0.00	#	6.00		2.0	3E+	15+	2	. 346	E + 11.		4.04E+08	# 2.44E-0	44 8.85E-12#
	2	#	1.39	•	.05		1.7	72+	154	2	. 341	E+11	# 3	3.78E+05	# 2.14E-0	4+ 8.85E-12#
	3		6.78	•	.10	#	1.2	SE +	15+	2	. 321	+11	# ;	3.14E+05	# 1.4FE-0	44 8.85E-12#
	4	ø	10.17	*	.15	#	6.6	<u> ۶</u> ٤ +	14*	2	. 30!	E+11	• 3	2.32E+08	# 8.18E-0	5* 8.85E-12#
•	5	#	13.56	•	.20	#	3.1	1F +	14*	2	. 24	+11	# 1	1.55E+09	# 3.85E-0	5+ 3.55E-12#
	6	#	16,95	#	• 25	•	1.2	6E +	14*	2	. 24	+11	# 1	1.01448	# 1.59E-0	5+ 8.85E-12#
	7	#	20.34	#	.30	#	4.7	4E+	13*	2	. 1 H	+11			'# 6.09E-J	
#	9	#	23.73	#	.35	#	1.7	7E+	1 3*			+11			# 2.32E-0	
#	3	#	27.11	*	.40	#	7.2							2•42E+07		
	16	#	30.50	#	•45	#	4.4	EE+	124					1.90E+07	# 6.2uE-0	
#	11	#	33.49	*	•50	#	1.2	1E +	13+	_	-	+11			'# 1.74E-0	
#	12	#	37.28	#	•55	#	2.8					+11			* 4.27E-0	
#	13	#	40.67	*	.60			1E+				E+11		6.03E+07		
	14	#	44.06	•	•65	#	5.9		- -	_		+11		6.38E+07		
#	15	#	47.45	*	.70	#		2E+							# 1.15E-0	
•	16.	#	50.64	•	•75	#		6E+	_					7. 3 6E+07		· • · · ·
	17	#	54.23	•	. 80	#		4E+		-	-	+11		8.25E+07		
	18	#	57.52	#	.85	#		0 E +				+11			# 1.59E-0	
	19	#	61.01	*	•90		8.9		-			+11			# 1.67E-0	
•	20	#	64.40	•	.95	#	8.9			_	_			9.51E+07		
	21	#	67.79	*	1.00	#		2£+			-	+11		8 • 43E+U7		_
	55	#	71.18	•	1.05			EE+				+11		_	# 1.73E-0	
	23		74.56	*	1.10		2 • 2					+11		8.15E+07		
	24	#	77.95	•	1.15		7.8							7.94E+07		
	25	#	81.34	*	1.20		7.3					+11			# 1.59F-J	· · · · · · · · ·
#	26	#	84.73	4	1.25	#	6.4	16+				+11		7.47E+07		
7	27		68.12	*	1.30 1.35							+11		7.20E+07		
#	2 9	#	91.51 94.90			₩	5.4					+11		6.91F+07		· · · · · - -
7	29 30	#	98.29		1.40 1.45	-	4.9	44. +				+11		6.52E+07	'# 1.25E-0 '# 1.16E-0	
4	31		101.68		1.50		4.4	_							# 1.06E-0	
#	32	*	105.07	*	1.55				_			+11			* 1.00E-0	
#	33	-	108.46		1.60		3.6					+11		5.3yE+07		
-	34	#	111.85		1.65							+11		5.07E+07		
#	35	#		#	1.70										-	6* 8.85E-12#
#	36		113.53		1.75											6* 8.85E-12#
	37	#		#	1.80											6+ 8.35E-12#
#	38	#		-	1.85											6+ 3.85E-12#
#	39	-	124.79	#	1.90											6* 8.85E-12#
#	40	#		+	1.95											6* 8.655-12#
#	41			#	2.00											5* 8.85E+12#
#	42		138.95	*	2.05											6* 8.85E-12#
#	43		142.35		2.10											6* 8.85E-12#
#	44			*	2.15											6* 8.45E-12#
#	45		143.13	•	2.20											7* 9.95E-12#
=	=====	==	=======	==:												*********

- Compared
| 221 | ***** | ********* | | # E : | | | = 2 | 2 2 21 | | | ********* | 2822222 |
|----------|----------|-------------------|------------------|-------|-------|-----------|--------------|-----------|-------|---------------|----------------------------------------|---------------------------------------|
| #F(| CINT 38 | | FACILS | | OCKE | | | EDE | _ | | FREGU | |
| | 7.40 | | 9E - 02 | # 5 | 1120 | NOI | 1 5 | 000 | (FT) | /10(FT/S) | | |
| | (H) | # (1 | 4) | # 6 | PRESS | (taE | . 0 | . 8 32 | 2 (A | Thospheres | ₽ (H | Z) • |
| *** | | | | £ 2 1 | | | === | 2 2 2 2 1 | | | ###################################### | 22222222 |
| | RADIAL | | | | | | | | | _ | | EPSILON # |
| | NDEX | # RACIUS | | • | | | | | | #FREQUENCY | | 453444 |
| | | • | * (P) | | (2/ | M3) | - | (1/3 |) | # (1/S) | # (MHC/N) * | (F0/H) # |
| 4 | 4 | # 0.0C | * 0.00 | | 4 77 | |
4 2 | 770 | | 8 2 74E A A A | # 1.61E-04* | 6.85E-12# |
| ¥ | 2 | | • 0.00 | | | 'E +15 | - | | | | # 1.42E-04* | |
| Ĭ. | 3 | | • 10 | 4 | | | _ | | | | # 1.01E-04* | · · · · · · · · · · · · · · · · · · · |
| 4 | 4 | | • 15 | | | E+14 | | | | | # 5.01E-05* | |
| ä | 5 | # 13.5E | 20 | | | | | | | | # 2.99E-054 | |
| ě | 6 | | • .25 | i | | E+13 | | | +11 | | # 1.25E-05* | |
| | 7 | | • .30 | | | | _ | | | | # 5.12E-06* | |
| # | 9 | # 23.73 · | .35 | | 1.53 | E+13 | + 2 | . 1 48 | +11 | # 3.52E+07 | # 2.02E-06* | 8.35E-12# |
| | 9 | | • .40 | | | | | | | | # 9.07E-07* | |
| • | 10 | # 30.56 | • .45 | | 4.66 | E+12 | * 2 | . 0 SE | +11 | # 1.93E+07 | # 6.40E-07* | 5.95E-12# |
| • | 11 | # 33.89 | • •50 | # | 1.35 | E+13 | | | | | # 1.98E-06* | |
| # | 12 | # 37.28 4 | • •55 | | 2.77 | 'E +1 3 | + 1 | . 9)8 | +11 | # 4.72E+07 | # 4.09E-06* | 8.55E-12# |
| # | 13 | # 40.67 | * ,6G | # | 4.15 | E+13 | | | | | # 6.40E-06* | |
| • | 14 | | • .65 | | | IE +13 | | | | | # 8.58E-06* | |
| # | 15 | | • .70 | | | E+13 | | | | # 7.22E+07 | | |
| # | 15 | # 50.34 | .75 | | | | | | | | # 1.22E-05* | |
| | 17 | | • .80 | | | | | | | | # 1.36E-95* | |
| | 18 | | • • • • • • | | | | | | | | # 1.47E-05* | |
| 7 | 19 | # 61.01 | • •90 | | | E+13 | _ | | | | # 1.55E-05* | |
| F | 20 | | .95 | 7 | | | | | | | # 1.60E-05*
1.62E-05* | |
| - | 21
22 | | • 1.00
• 1.05 | # | | F+13 | _ | | | | # 1.62E-05* | |
| - | 23 | | 1.10 | # | | | | | | | # 1.61E-35* | |
| # | 24 | # 77.95 | 1.15 | 7 | | | | | | # 7.75E+07 | | |
| | 25 | * 31.34 | 1.20 | | | | - | | - | # 7.54E+07 | | |
| 4 | 26 | | 1.25 | | | F +13 | | | E +11 | | # 1.45E-05* | |
| ë | 27 | # 69.12 | * 1.30 | | | | | | | # 7.36E+07 | | |
| # | 23 | _ | 1.35 | # | | C+13 | | | | | | |
| # | 29 | | 1.40 | # | | E+13 | | | | | # 1.21E-05* | 8.95E-12# |
| # | 30 | # 95,29 1 | 1.45 | # | 4.5 | E + 13 | + 1 | . 218 | +11 | # 6.24E+07 | # 1.126-05* | 8.85F-12# |
| # | 31 | # 101.68 | 1.50 | # | 4.40 | 16+13 | - 1 | . 208 | +11 | # 5.96E+37 | # 1.04E-35* | 8.85E-12# |
| # | 32 | # 105.07 | 1.55 | # | 3.97 | 'E+13 | | | E+11 | | | |
| # | 33 | # 108.46 | 1.60 | Ħ | | PE + 1, 3 | | | | # 5.37E+07 | | |
| # | 34 | # 111.35 ' | 1.65 | # | 3.18 | E+13 | * 1 | .16 | +11 | # 5.056+07 | # 7.73E-06* | 5.45E-12# |
| # | | | 1.70 | | | | | | | | # 6.92E-06* | |
| # | 36 | | 1.75 | | | | | | | | # 6.10E-J6+ | |
| | | | 1.80 | | | | | | | | # 5.36E-06* | |
| • | | # 125.40 | 1.85
1.90 | | | | | | | | # 4.63E-06*
3.96E-06* | |
| - | | | * 1.90
* 1.95 | | | | | | | | # 3.32E-06* | |
| - | 40
41 | | 5.00 | | | | | | | | # 2.74E=06* | |
| | _ | - ' | 2.05 | * | | | | | | | # 8.21E-36+ | |
| | | | 2.10 | | | | | | | | # 1.695-06* | |
| ī | | _ | • 2.15 | | | | | | | | # 1.2"E-06* | |
| # | · · · | • | 2.20 | # | 3.40 | DE +12 | * 1 | . 0 96 | E+11 | # 1.55E+07 | # 8.76E-07* | 8.855-12# |
| | 46 | | * 2.25 | # | 7.79 | E+11 | + 3 | . 23 | E+15 | # 7.92E+96 | # 6.79E-57* | 8.85E-12# |
| | 47 | # 155,91 | * 2.30 | # | 3.97 | 7E+11 | . + 3 | 1.22 | E+10 | # 5.66E+06 | 4 3.478-9/4 | 9.856-12# |
| = = = | ***** | | | | | | | | | | 2223352333 | |

ATTENDED TO SECURE OF THE PROPERTY OF THE PROP

#FOINTS	5.4	NO271 F	FACILS	#FO	KFT		REDE	YF		FRECUE	NCA T
# 7.60			8F-02					_	/10(FT/S)		
# (H)			(M)						TPOSPHERES		
			:			***					.,
			* AESCLUT			N# (EPSILON #
# INJEX		RACIUS							*FREQUENCY		4
* *15		776103	• (#)		(1/M3)					F (MHC/H) +	(FD/H)
******	.	2252222		2222	(本) ロット		\	3 / 2 = = =	* (1/3/	, (UUCLU) .	4 (70/07) ====================================
f 1		0.00	¥ 0.00	4 8	82541	44	2. 12	 	A 2 676+0A	1.07E-04*	A. 45F-124
. 2		3.39	• .05							9.548-05+	
* 3	ï	6.78	+ .10			-				# 6.94E-05*	
* 4		10.17	• .15							# 4.15E-35#	
* 5	-	13.56	+ .20			-					
# 6	-	16,95	+ .25							# 2.17E-054 # 9.85E-06*	
. 7	-	20.34	- 30							# 4.28E-06*	
	<u> </u>	23.73	* .35								
# 3	*	27.11	* .40							# 1.76E-06* # 8.47E-07*	
# 10	- T	30.50	+ .45							6.97E-07	
	-	33.39									
# 11	-									# 2.34E-06*	
12	7	37.26	• • •							4.24E-06*	
13		40.57								# 6.16E-06*	
# 14	7	44.16	* .65		-					# A.02E-06+	
# 15	7	47.45	* .70 * .75							9.76E-06+	
16	7	50.84	• • •							# 1.13E-05*	
# 17	7	54.23	* .60							# 1.26E-05*	
# 14		57.62	• • • • • • • • • • • • • • • • • • • •							1.36E-95*	
# 19		61.01	* .90							# 1.44E-05*	
# 20		64.40	• •95							# 1.50E-05*	
7 21		67.79	1.00							1.52E-05*	
# 22		71.18	+ 1.05				_			# 1.52E-05*	-
# 23	7	74.56	* 1.10		_					1.51E-05+	
# 24		77.95	* 1.15							# 1.46E-15+	
# 25		51.34	* 1.20		756+1					1.44E-35*	3.85E-12#
# 26	#	84.73	1.25		37E+1					1.38E-05*	
# 27	#	ed.12	1.30							# 1.32E-05*	
# 28	*	21.51	+ 1.35							# 1.25E-05*	
* 29	#	94.30	1.40		13E+1	-				1.17E-05*	
# 30		93.29	1.45		72E+1					1.09E-05+	
# 31	*	101.68	1.50		31E+1					# 1.01E-05*	
# 32	#	135.07	+ 1.55	_	31E+1				- · · · · · ·	9.25E-06*	
# 33		103.46	* 1.60		53F +1					# 8.47E-06+	8.85E-12#
# 34	#	111.85	* 1.65		176 +1					7.67E-06*	
# 35		115.24	4 1.70							6.90E-06+	
# 35		118.63	4 1.75							# 6.14E-06+	
# 37		122.01	1.00							# 5.43E-06+	
# 35		125.40	4 1.85							# 4.73E-36+	
# 39		129.79	* 1.90							# 4.11E-06+	
# 40		132-19	* 1.95							# 3.47E-064	
# 41		135.57	* 2.00							2.425-36+	
# 42		138.76	÷ 2.05							# 2.37E-36*	
# 43		142.35	2.10							1.585-064	
# 44		145.74	* 2.15							1.42E-76#	
# 45		143.13	. 2.50							# 1.0UE-05*	
# 46		152.52	* 2.25							6.8CE-07+	
# 47		155.51	* 2.30							# 3.4AE-07+	
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THE REPORT OF THE PROPERTY OF

_	*45***	_	_		223222821	: =		2 2 2	* =			* = : :	*****	= =		********
•	POINT4			_	RACILS		FOCKE			REDE				*	FREGUE	•
•	7.80	F	1.		E-02	-							FT/S)		2.50	
	(H)			(H) 		PF ESS	URE		0.53	: (A	TMOS	PHEFES	•	(4)	Z) •
3			********	22		. =	22231		32	****		****	222222	22	*********	********
	RADIA	_	RELATIV		ABSCLUTE								LASMA		SIGMA #	EPSILON #
4	INDEX	#	RACIUS	Ī	RACIUS	7							BUENCY		*	
*					(M) =======		(1/	M3)		(1.75	i	* (1/5)	#	(MHG/M) *	(FD/M) #
4	1		u • 0 0		0.00	4	6.26	5 4 4	. .	2.206		4 2	256+08	4	7.686-35*	
-	2		3.39		.05	•	5.61						13E+ù 3		6.07E=054	
	3		6.78	#	•10								33E+05		5.09E-05*	
ä	4	ě	10.17	•	•15	#				2.276			43E+00		5.13E-J5*	8.85E-12#
	5	ě	13.56	*	.20					2.24			04E+08		1.696-05+	8.45E-12#
#	6	#	16.95		•25		6.26								7.98E-06*	8.855-12#
	7		23.34	•	.30								75E+07		3.63E-06+	3.85E-12#
#	4	#	23.73		.35					2.138			06E+07		1.545-06*	8.855-12#
	4		27.11		-40		5.70						14E+07		7.74E-074	8.85E-12#
	10	#	33.50		.45	#	4.79						96E+07		6.62E-07*	0,85F-12#
#	11		33.89	•	.50		1.57						55E+07		2.25E-06*	d. 85E-12#
#	12	¢	37.28	#	•55		2.76	E+1	3*	1.916	+11	# 4.	728+37		4.03E-06+	8.85E-12#
	13	#	40.67	#	•60	#	3.85	E+1	3*	1 . 858	+11	# 5.	57E+07	#	5.67E-06*	8.85E-12#
•	14	#	44.06	•	• 65	#	4.33						24E+07	#	7.59E-06+	8.35E-12#
#	15		47.45	#	•70	#	5.65	E + 1	3*	1.748	+11	# 6.	75E+07	ŧ	9.17E-06+	3.95E-12#
#	15	*	50.84	#	•75	#	6.32						146+07		1.36E-05*	8.85E-12#
#	17		54.23	*	. 43	#	6.82	_	-						1.18E-05*	8.55E-12#
¢	1.7	#	57.62	*	• 85	#	7.17	_	-						1.275-054	9.85E-12#
#	19	#	61.91	*	• 90	#	7.38								1.35E-05*	4.95E-12#
#	20	#	64.40	*	•95		7.46	_							1.485-05*	8.955-12#
	21	*	67.79	*	1.00		7.40								1.436-054	8.85E-12#
	22	#	71.18	*	1.03	#	7.26						65E+07		1.446-05+	5.35E-12#
	23	#	74.56	*	1.10	*	7.16								1.43E-05*	8.85E-12#
	24	#	77.95	4	1.15	#	6.73								1.41E-05+	9.35E-12#
7	25 26	7	31.34	*	1.20	7	6.47						22E+07		1.37E-U5+	3.95F-12#
7	25 27		84.73 55.12	*	1.25 1.30	#	6.13								1.32E-05#	8.65E-12#
7	29	"	31.51		1.35	4	5.75 5.37			1.295 1.236			91E+07 58E+07		1.26E-05*	8.85E-12#
4	23	*	94.35	*	1.43	Ă	4.33						34E+U/		1.205-05+	9.95E-12#
ä	30	ï	34.83	*	1.45	#	4.96						34E+37		1.26E-35*	3.85E-12#
•	31		101.65		1.50	•	4.22	_					33E+07		9.64E-36*	3.65E-12#
•	32		105.07	*	1.55		3.95	_					5/E+07		9.08E-16*	8.85E-12#
#	33	#	103.46	٠	1.60	#	3.49								6.32E-36*	
	34	*	111.15	+											7.59E-06*	
#	35		115.24	•											6.84E-J6+	
#	36		118.63	*											6.14F-06*	
	37		122.91	*											5.465-16*	
#	33	#	125.40	•											4.61E-06*	
#	39	#	124.79	*											4.20F-J6#	
#	43	#	132.18	•											3.61E-06#	
#	41	#	135.57	*											1.08E-36*	
#	42	#	133.96	-	2.05	#	1.39	6+1	3 *	1.11E	+11	2.	14E+07	*	2.555-06+	3.356-12#
#	43		142.35	•											2.06E-06#	
#	44		145.74	•											1.63E=96*	
#	45		14 7.1 5	•											1.22E-06#	
#	46		152.52												3.565-37*	
	47		155.°1	*											3.48E-07~	
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Transfer of the Control of the Con

***				3 2 2	******	± z :			******		:::::::::::::::::::::::::::::::::::::::	**********	*********
##0	INT41		NOZZL	E R	ACIUS	#1	OCKET	1	REDEY	Ε	(FREGUI	ENCY #
	8.00		1.	486	-02	# (FOSITI	ON B	50000	FT)/	10(FT/S) (2.501	+08 #
	(M)			(H)							HOSPHERES		
		: 2		3 2 2	*******	2 W .		2223	22222	1821		::::::::::::::::::::::::::::::::::::	
# 5	ADTAL		RELATIV	F#	APSCLUT	F#	FLECT	RON	COLLIS	ION	PLASMA (SIGNA *	EPSILON #
	INDEX		PACIUS				_				FREQUENCY		
	MULA	-	- 40100		(4)			3) *				F (MHC/M) *	(FO/M) #
			******		\		1111 			, ,	, (1/3/ (4 10107) 72722222
				*	0 00		L 71.5		2 205	4414		5.33E-05*	w 466-424
	1	*	0.00	_	0.00					-		-	
	Ş		3.39	•	•05	Ŧ						4.81E-05*	
	3		6.78	•	•10	,						3.64E-05+	
	4		10.17	#	•15		1.36F	_				2.32E-05*	
#	5	#	13.56	•	•20							1.30E-05*	
	6	#	16.95	*	• 25							# 5.35E-06*	
	7			•	.30							# 3.05E-06+	
•	3		23.73	•	.35							* 1.35E-06*	
#	9	#	27.11	*	•40		5.158	+12*				7.U2E-07*	8.856-12#
	10	#	30.50	•	• 45	#	4.41E	+12*	2 4 0 2E	+114	1.39E+07	₽ 6.16E-07*	8.856-12#
	11	#	37.89	#	.50	#	1.45E	+13*	1.96E	+116	3.44E+07	# 2.10E-06*	8.35E-12#
#	12	#	37.28	#	.55	#	2.62E	+134	1.91E	+116	# 4.50E+U7	# 3.47E-06*	8.85E-12#
	13	#	40.67	*	•60	#	3.668	+134	1.85E	+116	5.43E+07	# 5.57E-06*	8.85E-12#
	14	*	44.06	#	•65	#	4.570	+134	1.80E	+116	6.07E+07	# 7.16E-J6*	9.85F-12#
#	15	#	47.45		.70		5.33E	+134	1.74E	+11	6.56E+07	# 5.63E-06*	8.85E-12#
	16			#	.75		5.95E	+134	1.69E	+116	6.92E+07	9.92E-06*	9.858-12#
	17				.80		6.428	+1 34	1.64E	+11	7.19E+07	1.10E-35+	8.85E-12#
Ä	18	ä	57.62		. 35		6.756	_				1.20E-054	
4	19		61.01		.90		5.355					1.27E-05+	
Ä	23	ě		*	•95		7.05E					1.325-05+	
Ä	21	i			1.00		7.010					1.35E-05*	3.956-12#
7	22	*			1.65		5.998				_	1.36E-05+	5.35E-12#
× ×		#		<u>.</u>			6.725					1.36E-35*	8.55E-12#
4	23	#		•	1:10							# 1.54E-05*	-
7	24	#	77.95		1.15		6.436		-			# 1.31E-05*	8.855-12#
	25	*	31.34	_	1.20		5.245			_			
•	26	界	84.73	-	1.25		5.396					# 1.26E-05*	
#	27	#		-	1.30	#						1.21E-05*	
#	28	#		*	1.35		5.200					# 1.16E-05*	
	29	#		•	1.40		4.54E				6 -25E+07		4.455-12#
#	30	#		*	1,45	#	4 .4 98					1.03E-05-	5.85F-12#
#	31	#		•	1.50	#	4.13E					# 9.56E-06*	8.856-12#
#	32	#	105.07	4	1.55		3.70			_			8.955-12#
	33	#	108.46	*	1.50		5 . 44E				5.262+07	•	8.95E-12#
#	34	#		*	1.65							# 7.48E-06+	
#	35		115.24	*	1.70							# 6.73E-36*	
	16	#	113.63	4	1.75							# 6.13E-06*	
#	37	tr	122.01		1.85							# 5.47E-16#	
#	38	#	125.40	-	1.85	#	1.958	~ 13°	1.148	+11	# 3.95E+07	# 4.87E-06+	8.35E-12¥
#	39	#	128.79	15	1,48	#	1 7 11	+134	1.13E	+11	# 3.72E+07	# 4.285-06#	8.85E-12#
#	4.0		132.13	*	1.95	#	1.636	+134	1.12E	+11	# 5.46E+97	# 3.72E-06*	8.358-12#
#	41	#		•	2.00							# 3.2GE-06*	
	42	#	134.96	-	2.05							# 2.71E-16*	
	43	#	142.33		2.10							# 2.26E-06*	
	44	Ü	145.7	•	2.15							# 1.826-36*	
	45	H	143.13		2.20							# 1.43E-16*	
*	40		192.53	#	2.25							# 1.358-36*	
ě	67		155.41		2.30							# 9.67F-07*	
v.	4 4		153.30	•	2.35	#	6.516	+114	2,770	+10:	7.25F+0h	# 5.00E-07*	4.85F=17#
7 7 7												*********	
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*	******	*********		**********		**************
	PCINT42	MOZZLE	-ACIUS #	FOCKET # #	REDEYE	FREQUENCY #
	8.20	-			300(FT)/10(FT/S) #	
-	(M'	# (M			. 932 (ATHOSPHERES)	
-	*****		,, 	********	TERRETERING THE TEREST	W 1377
•	FADIAL	# PELATIVE*	AASCLUTEA	ELECTRON*CO	LI TO TONA CLACMA A	CICHA A FOCT: NA A
	INDEX		· · · · · · · · · · · · · · · · · · ·			
×	THUEX	* KML_((3) *	(REQUENCY FREQUENCY #	
_		,	(") #	(1/M3) +	(1/5) / (1/5) /	(HHC/Y) + (FO/H) #
-		* * * * * * * * * * * * * * * * * * *				
Ţ	-	• 0.03 m	-		. 2 UE + 110 1 . 57E + 030	
	2	3.34			·24E+11# 1.50E+04#	
•	3	# 6.75 *			.275+11# 1.31E+03#	
	4	# 10-17 #			.25C+11# 1.05E+09#	
•	<u> </u>	# 13.56 *	***		.22E +11# 8.01E+07#	
	6	p 16.95 *	•••		1.19E+11# 5.69E+07#	
	7	# 20.34 +			?.15E+11# 3.96E+07#	
	8	# 23.73 *			?.11E+11# 2.68E+07#	•
3	9	# 27.11 *	-40 #	4.64F+12* 2	?.07E+11# 1.93E+07#	6.33E-07+ 8.85E-12#
#	10	# 3J.50 *	.45	4.045+124 2	?.01E+11# 1.80E+U?#	5.65E-074 8.35F-12#
	11	# 33.59 #	.50 #	1.34[*13* 1	66+11# 3.296+07#	1.92E-06* 8.85E-12#
#	12	#	.55 #		L.91E+11# 4.45E+07#	
#	1.5	# 40.67 *	.60 #	3.45[+13+ 1	L. 45E+11# 5.27E+07#	
#	14	# 44.05 *	. 65		auE+11# 5.90E+07#	
#	15	# 47.45 #	.70 *	5.03E+13+ 1	L.75E+11# 6.37E+07#	3.12E-06* 8.85E-12#
#	16	# 53.24 +	.75	5.62E+13# 1	64E+11# 6.73E+07#	4.34E-06* 3.35E-12#
	17	# 54.23 *	. 80 #	6.96E+13# 1	L.64E+11# 6.99E+07#	1.046-054 8.855-12#
	19	# 57.62 *	.85 #	6.33E+13+ 1	63E+11# 7.17E+07#	1.126-05- 8.855-12#
	19	# 61.01 *	• 90 •	6.56E+13# 1	55E+11# 7.28E+07#	1.19E-05* 4.85E-12#
	20	# 64.40 *	.45 #	6.56c+13+ 1	L.51E+11# 7.34E+07#	1.248-054 9.858-12#
#	21	# 67.79 *	1.00 #	6.66E+13# 1	L.47E+11# 7.32E+07#	1.276-05- 0.856-12#
#	22	# 71.10 •	1.05 #	6.566+13# 1	L.44E+11# 7.27E+07#	1.29E-05* 9.85E-12#
	23	# 74.56 *	1.10 #	6.41E+13+ 1	40E+11# 7.19E+07#	1.290-05+ 0.850-12#
#	24	# 77 . 35 *	1.15 #	6.210+13+ 1	L. 57E+11# 7.07E+J7#	1.27E-35+ 8.85E-12#
#	25	# 91.34 *	1.20 #	5.356+13+ 1	35E+11# 6.92E+U7#	1.256-15+ 8.856-12#
#	25	# 34,73 *	1.25 #	5.66E+13# 1	32E+11# 6.76E+07#	1.21E-J5# 5.95E-12#
	27	# 38.12 *	1.30 #	5 . 36k +1 5* 1	JUE +11# 6.57E+07#	1.175-35* 8.358-12#
	24	# 91.51 *	1.35 #	5.0 SE+13+ 1	L.27E+11# 6.57±+07#	1.11E-05* 8.85E-12#
	23	# 44.40 m	1.40 #	4.705+13# 1	L.25E+11# 5.16E+07#	1.060-054 3.455-124
	30	# 99.2a *	1.45 #	4.376+13* 1	L.24E+11# 5.93E+07#	9.965-064 3.855-124
#	31	# 101.53 *	1.50 #	4.035+13+ 1	L.23E+11# 5.70E+07#	3.32E-06* 3.35E-12#
	32	# 105.07 #	1.55	3.718+134 1	L. 20E+11# 5.47E+37#	8.676-06* 8.855-12#
#	3 3	# 103.46 *	1.60	3.398+13+ 1	L.14E+11# 5.23E+07#	
		# 111.35 *			1.18E+11# 4.39E+07#	
#	35	# 115.24 *	1.70 #	2.75E+13# 1	L.17E+11# 4.74E+87#	6.72F-J64 3.85E-12#
	36	# 115.61 *	1.75 #	2.51t +13+ 1	L. 16E + 11# 4.49E+37#	6.105-064 8.355-124
	37	* 122.61 *	1.60	2.23E+13# 1	15E+11# 4.24E+07#	5.47E-06* 3.45E-124
#	3.9	# 125.40 +	1.85 #	1.935+13# 1	L.14E+11# 4.0GE+07#	4.90E-06# 5.35E-12#
#	34	# 125.73 *	1.90 #	1.74L+13# 1	L.13E+11# 3.74E+U7#	4.32E-06* 8.35E-124
	44	# 132.1a *	1.95	1.525+13+ 1	1.15E+11# 5.59E+07#	3.61E-J6+ 5.85E-12#
	41	* 135.57 *	2.00 #	1 . 3 15 + 1 3# 3	L.12E+11# 3.25E+07#	3.295-06* 3.455-12#
#	42	# 138.36 *				2.83F-06* 8.45E-12#
#	_	# 142.35 *		4.421+12# 1	L.11E+11# 2.76E+07#	2.391-064 4.455-12#
		# 145.74 #			1.11E+11# 2.5JE+07#	
		# 144.13 *				1.616-06* 4.356-12#
		# 152.52 *				1.256-06* 8.356-12#
		# 155.91 *				9.70E=27+ 6.45E=12#
#		# 151.30 *				6.62E-37* 8.85E-12#

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•	1		0.00	•		•											10 2,00E-05* 8.85E-12	
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	•				.15	•			+14								'# 1.35E-05+ 8.85E-12	
7	5		13.56	*		•											# 3.03E-06+ 8.85E-12	
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i	á	•							+1								'# 1.05E-0E* 0.85E-12 '# 5.71E-07* 8.85E-12	
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	16	#	50.84	*	• • •				+13					-			'# 5.21E-06+ 8.85F-12	
	17			•			_		+1	_							# 9.80E-06# 8.85E-12	
7	19	-	57.52	*	102	•			+1								# 1.36E-05* 8.85E-12	
-	19			•	•90	-	_		+13								# 1.13E-05* 8.85E-12	
-	20 21				.95	7			*13 *13				+11				'# 1.18E-05* 9.35E-12 '# 1.21F-05* 8.85E-12	
	22	•			1.05				. +13								# 1.22E-35* 8.85E-12	
	23		• • • • • • • • • • • • • • • • • • • •	#	1.10				+13							E+07		
•	24		77.95		1.15		_		+1				+11				# 1.22E-05+ #.85E-12	
	25		81.34		1.20		5.	726	+13	5			+11				# 1.19E-35* 8.85E-12	
#	26	#	84.73	#	1.25	•	5.4	•66	+13	*	1.3	3 3 E	+11	• 6	.63	E+07	# 1.16E-05# 8.95E-12	*
#	27		58.12	•		•	5.	1 4E	+13	54	1.	BJE	+11				'# 1.12F-J5+ 8.45E-12	
	28			*	1.35		4.	3 9 6	+13	5#			+11				'# i.07E-35+ 8.45E-12	#
	23	•		*	1.40				•13								# 1.J2F-15+ 8.55E-12	
-	30	#		_	1.45	•			+13				+11				# 9.66E-16* 8.85E-12	
-	35 31	-	101.68	*	1000	4			+13				+11			_	# 9.07F-06* 8.45E-12	
-	33		109.46			4			+13 +13				+110			-	# 8.47E-06# 8.95E-12	
	34	•		•	1.65	ě			+13								'# 7.86E-J6* 8.85E-12 '# 7.25E-U6* 9.85E-12	
	35		115.24	*		i											# 6.64E-06* 3.85E-12	
	35		113.63						+13								# 6.05E-06* 3.35E-12	
	37		122.01	¥													# 5.47E-36+ 8.95E-12	
#	3 3		125.46		1.85												# 4.92E-06* 3.35E-12	
	53		123.75	-		W	1.	7 F E	+13								# 4.37E-06* 4.55E-12	
#	49		132.1:	*					+13								# 3.87f-06+ 3.95E-12	
#	41		135.57	•													# 3.3/E-36* 4.95E-12	
#	42		133.96	•													# 2.93E-06* 9.85E-12	
#	43		142.35	*													# 2.49E-36# 8.95E-12	
	44 45		145.74														# 2.1JE-36* 3.85E-12 # 1./25-36* 3.85E-12	
	46		152.52														# 1.3cE=U6= 3.35E=12	
	47		153.91														* 1.Jet-Jt* 0.d5f-12	
	49		159.30	4													# 7.83E-07* 8.95E-12	
#	43		162.69	*	2.43												# 6.44F-97* 5.45E-12	
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RADIALO RELATIVE ASCLUTED ELECTRON COLLISION PLASMA PACTUS FACTUS CONSTITY FREQUENCY FREQUEN	
INDEX	
# 1	JK
#	
1 0 0.00 * 0.00 * 1.63E^14* 2.26E*110 1.15E*000 2.04E*05* 8.85E 2 8 3.39 * .05 8 1.50E*14* 2.25E*110 1.10E*0.50 1.87E*05* 8.85E 3 8 6.78 * .10 0 1.15E*14* 2.25E*110 1.10E*0.50 1.87E*05* 8.85E 4 9 10.17 * .15 8 0.12E*13* 2.23E*110 8.30E*070 1.49E*05* 9.85E 6 13.5E * .20 8 4.94E*13* 2.20E*110 8.30E*070 1.33E*05* 9.85E 6 8 16.95 * .25 3 2.03E*13* 2.14E*110 8.36E*070 3.45E*06* 8.55E 7 8 20.34 * .30 8 1.40E*13* 2.17E*110 8.66E*070 3.45E*06* 8.55E 8 9 0 27.73 * .35 8 6.32E*12* 2.10E*110 3.36E*070 9.22E*070 8.65E* 8 9 0 27.11 * .40 8 3.74E*12* 2.06E*110 1.74E*070 5.13E*07* 8.65E* 8 10 30.50 * .45 3 3.33E*12* 2.01E*110 1.64E*070 9.22E*070 8.65E* 8 11 8 33.50 * .45 3 3.33E*12* 2.01E*110 1.64E*070 9.22E*070 8.65E* 8 12 37.22 * .55 8 2.14E* 3* 1.96E*110 4.96E*070 4.68E*07* 9.85E* 8 12 37.22 * .55 8 2.14E* 3* 1.96E*110 4.96E*070 9.69E*070 9.85E* 8 13 40.67 * .60 8 3.95E*13* 1.86E*110 4.96E*070 4.63E*06* 8.85E* 8 14 44.06 * .65 8 3.83E*13* 1.80E*110 5.56E*070 4.63E*06* 8.85E* 8 15 8 47.45 * .70 8 4.49E*13* 1.75E*110 6.37E*070 3.16E*06* 8.85E* 8 16 9 50.84 * .75 9 5.03E*13* 1.70E*110 6.37E*070 3.32E*06* 8.85E* 8 17 6 54.23 * .80 8 5.44E*13* 1.75E*110 6.96E*070 3.22E*06* 8.85E* 8 19 0 10.01 * .90 8 5.44E*13* 1.75E*110 6.96E*070 1.00E*05* 8.35E* 8 19 0 10.01 * .90 8 5.44E*13* 1.57E*110 6.96E*070 1.15E*05* 8.35E* 8 19 0 10.01 * .90 8 5.44E*13* 1.57E*110 6.96E*070 1.15E*05* 8.35E* 8 21 6 77.79 * 1.00 8 6.05E*13* 1.49E*110 6.96E*070 1.15E*05* 8.85E* 8 22 71.11 * 1.05 8 5.71E*13* 1.35E*110 6.96E*070 1.15E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.16E*05* 8.85E* 8 24 8 77.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 74.95 * 1.15 8 5.71E*13* 1.35E*110 6.95E*070 1.15E*05* 8.85E* 8 24 8 74.95 * 1.15 8 5.71E*13* 1.35E*110	H)
2	
# 10.17 * .15 # 2.12E+14* 2.24E+114 # 3.75E+07# 1.49E-05* # 8.85E # 10.17 * .15 # 2.12E+13* 2.22E+114 # 3.75E+07# 1.32E-05* # 3.85E # 6 # 16.95 * .25 # 2.05E+13* 2.17E+11# 4.66E+07# 3.49E-06* 8.85E # 7 # 20.34 * .30 # 1.40E+13* 2.10E+11# 3.36E+07# 3.49E-06* 8.85E # 9 # 23.73 * .35 # 6.32E+12* 2.10E+11# 3.36E+07# 9.23E-07* 8.25E # 10 # 30.50 * .45 # 3.33E+12* 2.06E+11# 1.74E+07# 5.13E-07* 8.25E # 11 # 30.50 * .45 # 3.33E+12* 2.06E+11# 1.64E+07# 4.68E-37* 8.85E # 12 # 37.22 * .55 # 2.14E+13* 1.36E+11# 2.97E+07# 1.55E-06* 3.85E # 13 # 40.67 * .60 # 3.05E+13* 1.36E+11# 2.97E+07# 3.16E-06* 3.85E # 14 # 4.96 * .65 # 3.63E+13* 1.36E+11# 4.96E+07# 4.63E-36* 3.85E # 15 # 47.45 * .70 # 4.49E+13* 1.66E+11# 6.96E+07# 4.32E-06* 3.85E # 16 # 50.84 * .75 # 5.03E+13* 1.75E+11# 6.02E+37# 7.23E-06* 8.35E # 17 # 554.23 * .80 # 5.44E+13* 1.66E+11# 6.92E+07# 1.00E-05* 8.35E # 19 # 57.52 * .85 # 5.74E+13* 1.66E+11# 6.92E+07# 1.00E-05* 8.35E # 19 # 57.52 * .85 # 5.74E+13* 1.57E+11# 6.92E+07# 1.00E-05* 8.35E # 19 # 57.52 * .85 # 6.74E+13* 1.57E+11# 6.92E+07# 1.12E-05* 8.35E # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.92E+07# 1.12E-05* 8.35E # 21 # 67.75 * 1.00 # 5.99E+13* 1.49E+11# 6.93E+07# 1.12E-05* 8.35E # 22 # 71.12 * 1.05 # 5.99E+13* 1.49E+11# 6.93E+07# 1.15E-05* 8.35E # 23 # 74.56 * 1.10 # 5.71E+13* 1.39E+11# 6.79E+07# 1.15E-05* 8.35E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.15E-05* 8.35E # 25 # 74.56 * 1.10 # 5.50E+13* 1.49E+11# 6.93E+07# 1.15E-05* 8.35E # 26 # 4.73 * 1.55 # 5.50E+13* 1.49E+11# 6.79E+07# 1.15E-05* 8.35E # 27 # 4.15 * 1.55 # 5.50E+13* 1.49E+11# 6.79E+07# 1.15E-05* 8.35E # 28 # 31.51 * 1.55 # 5.50E+13* 1.49E+11# 5.75E+07# 1.16E-05* 8.35E # 29 # 34.36 * 1.55 # 1.55 # 3.35E+13* 1.29E+11# 6.35E+07# 1.15E-05* 8.35E # 30 # 30.50 * 1.55 # 3.35E+13* 1.29E+11# 5.75E+07# 1.01E-05* 8.35E # 31 # 101.5* * 1.55 # 3.35E+13* 1.29E+11# 5.35E+07# 1.01E-05* 8.35E # 32 # 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 * 30.50 *	-12
# # 10.17 * .15 # e.12E+13* 2.23E+11# 8.09E+07# 1.03E=05* 3.85E # # 13.5E * .20 # 4.94E+13* 2.20E+11# 6.31E+07# 6.32E=06* 8.85E # # 20.34 * .30 # 1.40E+13* 2.14E+11# 3.36E+07# 1.42E=06* 8.85E # # 23.73 * .35 # 6.32E+12* 2.10E+11# 3.36E+07# 1.42E=06* 8.85E # # 23.73 * .35 # 6.32E+12* 2.10E+11# 3.36E+07# 9.23E=07* 8.65E # # 23.73 * .35 # 6.32E+12* 2.10E+11# 1.74E+07# 5.13E=07* 8.65E # # 30.50 * .45 # 3.33E+12* 2.0EE+11# 1.74E+07# 5.13E=07* 8.85E # # 10 # 30.50 * .45 # 3.33E+12* 2.0EE+11# 1.74E+07# 5.13E=07* 8.85E # # 11 # 35.46 * .50 # 1.10E+13* 1.36E+11# 2.97E+07# 1.55E=06* 8.85E # # 12 # 37.22 * .55 # 2.14E+ 3* 1.91E+11# 4.15E+07# 3.16E=06* 8.85E # # 14 # 44.06 * .65 # 3.03E+13* 1.40E+11# 5.56E+07# 7.23E=06* 8.85E # # 14 # 44.06 * .65 # 3.03E+13* 1.40E+11# 5.56E+07# 7.23E=06* 8.85E # # 14 # 44.06 * .65 # 3.03E+13* 1.75E+11# 6.02E+37# 7.23E=06* 8.85E # # 15 # 50.84 * .75 # 5.03E+13* 1.75E+11# 6.62E+07# 7.23E=06* 8.85E # # 15 # 50.84 * .75 # 5.03E+13* 1.75E+11# 6.62E+07# 7.23E=06* 8.85E # # 19 # 57.52 * .85 # 5.74E+13* 1.75E+11# 6.62E+07# 7.23E=06* 8.85E # # 10 # 57.52 * .85 # 5.74E+13* 1.57E+11# 6.62E+07# 1.00E=05* 8.85E # # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.92E+07# 1.15E=05* 8.85E # # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.92E+07# 1.15E=05* 8.85E # # 24 # 77.95 * 1.00 # 6.05E+13* 1.42E+11# 6.93E+07# 1.16E=05* 8.85E # # 24 # 77.95 * 1.15 # 5.77E+13* 1.42E+11# 6.96E+07# 1.16E=05* 8.85E # # 24 # 77.95 * 1.15 # 5.77E+13* 1.42E+11# 6.96E+07# 1.16E=05* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.33E+11# 6.95E+07# 1.16E=05* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.35E+11# 6.95E+07# 1.16E=05* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.35E+11# 6.95E+07# 1.16E=05* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.35E+11# 6.95E+07# 1.16E=05* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.35E+11# 6.95E+07# 1.16E=05* 8.85E # # # # 40.25 * 1.25 # 5.26E+13* 1.26E+11# 6.35E+07# 1.26E+06* 8.85E # # # 40.25 * 1.25 # 5.26E+13* 1.26E+11# 6.35E+07# 1.26E+06* 8.85E # # # # 40.25 * 1.25 # 5.26E+13* 1.26E+11# 6.35E+07# 1.26E+0	-12
13.56	-12
# 6 # 16.95	-12
# 7 # 20.34 * .30 # 1.40E+13* 2.14E+11* 3.36E+07# 1.84E-06* 8.85E 9 # 23.73 * .35 # 6.32E+12* 2.10E+11# 2.36E+07# 9.23E-07* 8.23E # 10 # 30.50 * .45 # 3.33E+12* 2.01E+11# 1.74E+07# 5.13E-07* 8.85E # 11 # 35.49 * .50 # 1.10E+13* 1.36E+11# 2.97E+07# 1.55E-36* 9.85E # 12 # 37.20 * .55 # 2.14E+ 3* 1.36E+11# 2.97E+07# 1.55E-36* 9.85E # 14 # 44.06 * .60 # 3.05E+13* 1.86E+11# 4.96E+07# 4.68E-37* 9.85E # 15 # 47.45 * .70 # 4.49E+13* 1.75E+11# 5.56E+07# 4.68E-06* 8.85E # 16 # 50.84 * .75 # 5.03E+13* 1.75E+11# 6.32E+07# 3.2E+06* 8.85E # 17 # 55.22 * .80 # 5.74E+13* 1.66E+11# 6.32E+07# 3.2E+06* 8.85E # 19 # 57.52 * .85 # 5.74E+13* 1.66E+11# 6.32E+07# 3.2E+06* 8.35E # 19 # 51.01 * .90 # 5.34E+13* 1.57E+11# 6.36E+07# 1.12E+05* 8.35E # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.36E+07# 1.12E+05* 8.35E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.36E+07# 1.12E+05* 8.35E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.36E+07# 1.12E+05* 8.35E # 23 # 74.56 * 1.10 # 5.37E+13* 1.49E+11# 6.36E+07# 1.1E+05* 8.35E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.36E+07# 1.1E+05* 8.35E # 24 # 31.51 * 1.35 # 4.73E+13* 1.35E+11# 6.66E+07# 1.1E+05* 8.35E # 25 # 31.34 * 1.20 # 5.56E+13* 1.35E+11# 6.46E+07# 1.1E+05* 8.35E # 26 # 64.73 * 1.25 # 5.26E+13* 1.35E+11# 6.46E+07# 1.1E+05* 8.35E # 27 # 44.12 * 1.30 # 5.26E+13* 1.35E+11# 6.46E+07# 1.1E+05* 8.35E # 24 # 74.56 * 1.10 # 5.37E+13* 1.35E+11# 6.46E+07# 1.1E+05* 8.35E # 25 # 31.34 * 1.20 # 5.56E+13* 1.35E+11# 6.56E+07# 1.1E+05* 8.35E # 27 # 44.12 * 1.35 # 4.73E+13* 1.29E+11# 6.35E+07# 1.03E+05* 8.35E # 31 # 31.51 * 1.35 # 4.73E+13* 1.25E+11# 5.56E+07# 3.27E+06* 8.35E # 31 # 31.51 * 1.35 # 4.73E+13* 1.25E+11# 5.56E+07# 3.27E+06* 8.35E # 31 # 31.51 * 1.35 # 4.73E+13* 1.25E+11# 5.56E+07# 3.27E+06* 8.35E # 32 # 31.50 * 1.55 # 3.37E+13* 1.25E+11# 5.56E+07# 3.27E+06* 8.35E # 31 # 31.52 * 1.55 # 3.37E+13* 1.26E+11# 5.56E+07# 3.27E+06* 8.35E # 32 # 31.50 * 1.55 # 3.37E+13* 1.26E+11# 5.56E+07# 3.27E+06* 8.35E # 31 # 31.52 # 1.50 # 3.32E+13* 1.26E+11# 4.76E+07# 3.27E+06* 8.35E	
# # 23.73 * .35 # 6.92E+12* 2.10E+11# 2.36E+07# 9.23E-07* 8.67E # 9 # 27.11 * .40 # 3.74E+12* 2.36E+01# 1.77E+07# 5.13E-07* 8.85E # 10 # 30.50 * .45 # 3.33E+12* 2.01E+11# 1.56E+07# 4.68E-07* 9.85E # 11 # 33.50 * .45 # 3.33E+12* 2.01E+11# 1.56E+07# 4.68E-07* 9.85E # 12 # 37.22 * .55 # 2.14E+ 3* 1.96E+11# 2.97E+07# 1.55E-06* 9.85E # 12 # 37.22 * .55 # 2.14E+ 3* 1.91E+11# 4.15E+07# 3.16E-06* 8.85E # 13 # 40.67 * .60 # 3.05E+13* 1.86E+11# 4.5E+07# 3.16E-06* 8.85E # 14 # 44.06 * .65 # 3.03E+13* 1.70E+11# 5.56E+07# 7.23E+06* 3.85E # 15 # 47.45 * .70 # 4.49E+13* 1.75E+11# 6.02E+07# 7.23E+06* 8.85E # 16 # 50.84 * .75 # 5.03E+13* 1.70E+11# 6.92E+07# 7.23E+06* 8.85E # 17 # 55.23 * .80 # 5.44E+13* 1.66E+11# 6.92E+07# 7.23E+06* 8.85E # 19 # 57.52 * .85 # 5.74E+13* 1.66E+11# 6.90E+07# 1.07E+05* 8.85E # 19 # 51.01 * .90 # 5.74E+13* 1.52E+11# 6.90E+07# 1.07E+05* 8.85E # 20 # 64.40 * .95 # 6.04E+13* 1.52E+11# 6.90E+07# 1.12E+05* 8.85E # 21 # 67.79 * 1.00 # 6.95E+13* 1.49E+11# 6.96E+07# 1.12E+05* 8.85E # 22 # 71.15 * 1.05 # 5.97E+13* 1.49E+11# 6.96E+07# 1.17E+05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16E+05* 8.85E # 25 # 31.34 * 1.20 # 5.90E+13* 1.39E+11# 6.55E+07# 1.12E+05* 8.85E # 26 # 64.73 * 1.25 # 5.26E+13* 1.33E+11# 6.55E+07# 1.14E-05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.33E+11# 6.55E+07# 1.14E-05* 8.85E # 28 # 31.51 * 1.35 # 4.73E+13* 1.39E+11# 6.55E+07# 1.14E-05* 8.85E # 29 # 34.90 * 1.40 # 4.44F+13* 1.22E+11# 6.55E+07# 1.14E-05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.33E+11# 6.55E+07# 1.03E+05* 8.85E # 28 # 34.90 * 1.40 # 4.44F+13* 1.22E+11# 6.55E+07# 1.03E+05* 8.85E # 29 # 34.90 * 1.40 # 4.45E+13* 1.33E+11# 6.55E+07# 1.03E+05* 8.85E # 31 # 101.50 * 1.50 # 3.36E+13* 1.22E+11# 5.56E+07# 1.03E+05* 8.85E # 32 # 105.07 * 1.55 # 3.36E+13* 1.22E+11# 5.56E+07# 1.03E+05* 8.85E # 32 # 105.07 * 1.55 # 3.36E+13* 1.22E+11# 5.56E+07# 3.27E+06* 8.85E # 33 # 41.51 * 1.55 # 3.36E+13* 1.22E+11# 5.56E+07# 3.27E+06* 8.85E # 34 # 111.85 * 1.50 # 3.36E+13* 1.22E+11# 5.56E+07# 3.27E+06* 8.85E # 34 # 111.85 * 1.50	
# 9	
# 10 # 30.50 * .45 # 3.33E+12* 2.01E+11# 1.64E+07# 4.68E=07* 9.85E # 11 # 35.49 * .50 # 1.10E+13* 1.36E+11# 2.97E+07# 1.56E=06* 8.85E # 12 # 37.22 * .55 # 2.14E+ 3* 1.91E+11# 4.19E+07# 3.16E=06* 8.85E # 13 # 40.67 * .60 # 3.05E+13* 1.86E+11# 4.96E+07# 4.63E=16* 3.85E # 14 # 44.06 * .65 # 3.63E+15* 1.80E+11# 4.96E+07# 4.63E=16* 3.85E # 15 # 47.45 * .70 # 4.49E+13* 1.75E+11# 6.02E+07# 7.23E=06* 8.85E # 15 # 50.84 * .75 # 5.03E+13* 1.70E+11# 6.87E+07# 4.32E=06* 8.85E # 16 # 50.84 * .75 # 5.03E+13* 1.70E+11# 6.62E+07# 9.26E=06* 3.85E # 17 # 54.23 * .80 # 5.44E+13* 1.61E+11# 6.40E+07# 4.22E=06* 3.85E # 19 # 61.01 * .90 # 5.44E+13* 1.61E+11# 6.40E+07# 1.00E=05* 8.85E # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.92E+07# 1.07E=05* 8.85E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.98E+07# 1.15E=05* 8.85E # 22 # 71.12 * 1.05 # 5.99E+13* 1.49E+11# 6.98E+07# 1.15E=05* 8.85E # 23 # 74.56 * 1.10 # 5.37E+13* 1.49E+11# 6.98E+07# 1.16E=05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.36E+11# 6.66E+07# 1.14E=05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.66E+07# 1.14E=05* 8.85E # 27 # 46.12 * 1.30 # 5.01E+13* 1.36E+11# 6.35E+07# 1.16E=05* 8.85E # 27 # 46.12 * 1.30 # 5.01E+13* 1.36E+11# 6.35E+07# 1.09E=05* 8.85E # 28 # 31.51 * 1.25 # 4.73E+13* 1.36E+11# 6.35E+07# 1.09E=05* 8.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.27E+11# 6.35E+07# 1.09E=05* 8.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.27E+11# 5.50E+07# 1.09E=05* 8.85E # 31 # 101.60 * 1.55 # 4.73E+13* 1.29E+11# 5.50E+07# 1.09E=05* 8.85E # 32 # 105.07 * 1.55 # 4.73E+13* 1.29E+11# 5.50E+07# 3.63E=06* 8.85E # 31 # 101.60 * 1.40 # 4.44F+13* 1.27E+11# 5.50E+07# 3.63E=06* 8.85E # 31 # 101.60 * 1.40 # 4.44F+13* 1.27E+11# 5.50E+07# 3.63E=06* 8.85E # 32 # 105.07 * 1.55 # 3.57E+13* 1.29E+11# 5.50E+07# 3.63E=06* 8.85E # 31 # 101.60 * 1.40 # 4.44F+13* 1.29E+11# 5.50E+07# 3.63E=06* 8.85E # 32 # 105.07 * 1.55 # 3.57E+13* 1.20E+11# 5.50E+07# 3.63E=06* 8.85E # 33 # 103.46 * 1.60 # 3.23E+13* 1.20E+11# 5.50E+07# 3.63E=06* 8.85E	
# 11 # 35.49 * .50 # 1.10E+13* 1.36E+11# 2.97E+07# 1.55E-056* 9.45E # 12 # 37.28 * .55 # 2.14E+ 3* 1.91E+11# 4.15E+07# 3.16E-06* 8.85E # 13 # 40.67 * .60 # 3.05E+13* 1.86E+11# 4.96E+07# 4.63E-06* 8.85E # 14 # 44.06 * .65 # 3.63E+13* 1.80E+11# 5.56E+07# 5.99E-06* 8.35E # 15 # 47.45 * .70 # 4.49E+13* 1.75E+11# 6.02E+07# 7.23E-06* 8.85E # 16 # 50.84 * .75 # 5.03E+13* 1.70E+11# 6.62E+07# 7.23E-06* 8.85E # 17 # 54.23 * .80 # 5.44E+13* 1.66E+11# 6.62E+07# 9.26E+06* 3.85E # 19 # 57.52 * .85 # 5.74E+13* 1.61C+11# 6.62E+07# 1.00E-05* 8.35E # 19 # 57.52 * .85 # 5.74E+13* 1.57E+11# 6.98E+07# 1.07E-05* 8.35E # 19 # 57.52 * .85 # 5.74E+13* 1.57E+11# 6.98E+07# 1.07E-05* 8.35E # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.98E+07# 1.12E-05* 8.85E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.98E+07# 1.15E-05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.98E+07# 1.16E-05* 8.85E # 23 # 74.56 * 1.10 # 5.37E+13* 1.49E+11# 6.79E+07# 1.16E-05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.36E+11# 6.60E+07# 1.16E-05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.60E+07# 1.16E-05* 8.85E # 26 # 84.73 * 1.25 # 5.26E+13* 1.33E+11# 6.55E+07# 1.09E-05* 8.85E # 27 # 46.12 * 1.30 # 5.71E+13* 1.32E+11# 6.57E+07# 1.09E-05* 8.85E # 27 # 430.2 * 1.55 # 4.73F+13* 1.29E+11# 6.57E+07# 1.09E-05* 8.85E # 24 # 77.95 * 1.55 # 4.73F+13* 1.29E+11# 5.51E+07# 1.03E-05* 8.85E # 25 # 31.51 * 1.55 # 4.73F+13* 1.29E+11# 5.57E+07# 1.03E-05* 8.85E # 27 # 46.12 * 1.30 # 5.01E+13* 1.29E+11# 5.57E+07# 1.03E-05* 8.85E # 28 # 44.44F+13* 1.27E+11# 5.57E+07# 1.03E-06* 8.85E # 30 # 4.56 # 4.44F+13* 1.27E+11# 5.58E+07# 9.47E-06* 8.85E # 31 # 101.54 * 1.40 # 4.44F+13* 1.27E+11# 5.58E+07# 9.47E-06* 8.85E # 31 # 101.55 * 1.45 # 4.19F+13* 1.26E+11# 5.58E+07# 9.47E-06* 8.85E # 31 # 101.56 * 1.50 # 3.36C+13* 1.26E+11# 5.58E+07# 9.47E-06* 8.85E # 31 # 101.56 * 1.50 # 3.36C+13* 1.26E+11# 5.58E+07# 9.47E-06* 8.85E # 33 # 105.07 * 1.55 # 3.27E+13* 1.26E+11# 5.56E+07# 9.47E-06* 8.85E # 35 # 115.24 * 1.60 # 3.24E+13* 1.26E+11# 5.56E+07# 7.70E-06* 8.85E	_
# 12 # 37.20 # .55 # 2.14E+ 3# 1.91E+11# 4.15E+07# 3.16E-06# 3.85E 13 # 40.67 # .60 # 3.95E+13# 1.86E+11# 4.96E+07# 4.63E-36# 3.85E 14 # 44.06 # .65 # 3.03E+13# 1.80E+11# 5.56E+07# 5.99E-06# 8.85E 15 # 47.45 # .70 # 4.49E+13# 1.70E+11# 6.02E+07# 7.23E-06# 8.85E 16 # 50.84 # .75 # 5.03E+13# 1.70E+11# 6.02E+07# 7.23E-06# 8.85E 17 # 54.23 # .80 # 5.44E+13# 1.66E+11# 6.62E+07# 9.26E-06# 3.85E 19 # 57.52 # .85 # 5.74E+13# 1.61C+11# 6.92E+07# 1.00E-05# 8.35E 19 # 61.01 # .90 # 5.44E+13# 1.52E+11# 6.92E+07# 1.07E-95# 8.35E 20 # 64.40 # .95 # 6.04E+13# 1.57E+11# 6.93E+07# 1.15E-05# 8.35E 21 # 67.79 # 1.00 # 6.05E+13# 1.49E+11# 6.93E+07# 1.15E-05# 8.35E 22 # 71.15 # 1.05 # 5.99E+13# 1.49E+11# 6.96E+07# 1.15E-05# 8.35E 23 # 74.56 # 1.10 # 5.57E+13# 1.49E+11# 6.96E+07# 1.16E-05# 8.35E 24 # 77.95 # 1.15 # 5.71E+13# 1.35E+11# 6.79E+07# 1.16E-05# 8.35E 25 # 31.34 # 1.20 # 5.50E+13# 1.36E+11# 6.79E+07# 1.16E-05# 8.35E 26 # 84.73 # 1.30 # 5.01E+13# 1.33E+11# 6.35E+07# 1.10E-05# 8.35E 27 # 48.12 # 1.30 # 5.01E+13# 1.34E+11# 6.35E+07# 1.03E+05# 8.35E 28 # 31.34 # 1.25 # 5.26E+13# 1.34E+11# 6.35E+07# 1.03E+05# 8.35E 29 # 94.40 * 1.40 # 4.44F+13# 1.34E+11# 6.35E+07# 1.03E+05# 8.35E 21 # 11.50 # 3.36C+13# 1.25E+11# 5.56E+07# 1.03E+05# 8.35E 23 # 94.40 * 1.40 # 4.44F+13# 1.25E+11# 5.56E+07# 1.03E+05# 8.35E 24 # 11.50 # 3.36C+13# 1.25E+11# 5.56E+07# 1.03E+05# 8.35E 25 # 31.34 # 1.25 # 1.35 # 4.73E+13# 1.25E+11# 5.56E+07# 1.03E+05# 8.35E 26 # 31.50 # 1.35 # 4.73E+13# 1.25E+11# 5.56E+07# 1.03E+05# 8.35E 27 # 31.50 # 1.35 # 4.75E+13# 1.25E+11# 5.56E+07# 7.70E+06# 8.35E 28 # 105.07 # 1.50 # 3.36C+13# 1.25E+11# 5.56E+07# 7.70E+06# 8.35E 31 # 101.50 # 1.50 # 3.36C+13# 1.25E+11# 5.56E+07# 7.70E+06# 8.35E 33 # 105.07 # 1.50 # 3.36C+13# 1.25E+11# 5.56E+07# 7.70E+06# 8.35E 33 # 105.07 # 1.50 # 3.36C+13# 1.25E+11# 5.56E+07# 7.35E+06# 8.35E 34 # 111.35 # 1.50 # 3.36C+13# 1.20E+11# 5.56E+07# 7.35E+06# 8.35E	-
# 13 # 40.67 * .60 # 3.95E+13* 1.86E+11# 4.96E+07# 4.63E-06* 3.85E # 14 # 44.06 * .65 # 3.83E+13* 1.70E+11# 5.56E+07# 5.99E+06* 8.35E # 15 # 47.45 * .70 # 4.99E+13* 1.77E+11# 6.02E+07# 7.23E-06* 8.35E # 16 # 50.84 * .75 # 5.03E+13* 1.70E+11# 6.02E+07# 7.23E-06* 8.35E # 17 # 554.23 * .80 # 5.44E+13* 1.66E+11# 6.62E+07# 9.26E+06* 3.85E # 19 # 51.01 * .90 # 5.44E+13* 1.57E+11# 6.9E+07# 1.00E+05* 8.35E # 19 # 61.01 * .90 # 5.44E+13* 1.57E+11# 6.9E+07# 1.07E+05* #.35E # 20 # 64.40 * .95 # 6.04E+13* 1.52E+11# 6.98E+07# 1.12E+05* #.85E # 21 # 67.77 * 1.00 # 6.05E+13* 1.49E+11# 6.98E+07# 1.15E+05* #.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.98E+07# 1.15E+05* #.85E # 23 # 74.56 * 1.10 # 5.97E+13* 1.49E+11# 6.98E+07# 1.16E+05* #.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16F+05* #.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.66E+07# 1.14E+05* #.85E # 26 # 64.77 * 1.30 # 5.50E+13* 1.36E+11# 6.59E+07# 1.16F-05* #.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.33E+11# 6.35E+07# 1.09E-05* #.85E # 27 # dd.12 * 1.30 # 4.44F+13* 1.32E+11# 6.35E+07# 1.09E-05* #.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.2E+11# 6.35E+07# 1.09E-05* #.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.2E+11# 6.35E+07# 1.03E+05* #.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.2E+11# 6.35E+07# 1.03E+05* #.85E # 29 # 94.90 * 1.45 # 4.15E+13* 1.2E+11# 5.56E+07# 3.2FE-06* #.85E # 29 # 94.90 * 1.45 # 4.15E+13* 1.2E+11# 5.56E+07# 3.2FE-06* #.85E # 31 # 101.64 * 1.50 # 3.36C+13* 1.2E+11# 5.56E+07# 3.2FE-06* #.85E # 32 # 105.46 * 1.50 # 3.36C+13* 1.2EE+11# 5.56E+07# 3.2FE-06* #.85E # 34 # 103.46 * 1.65 # 3.3E+13* 1.2UE+11# 5.3EE+07# 7.7UE+06* #.85E # 35 # 111.85 * 1.65 # 3.3E+13* 1.2UE+11# 5.3EE+07# 7.7UE+06* #.85E	
# 14 # 44.06 * .65 # 3.83E+13* 1.40E+11# 5.56E+17# 5.99E+06* 8.35E # 15 # 47.45 * .70 # 4.49E+13* 1.75E+11# 6.02E+J7# 7.23E+06* 8.85E # 15 # 50.84 * .75 # 5.03E+13* 1.7UE+11# 6.37E+07# 4.32E+06* 3.85E # 17 6 54.23 * .80 # 5.44E+13* 1.66E+11# 6.62E+07# 9.26E+06* 3.85E # 19 # 57.52 * .85 # 5.74E+13* 1.66E+11# 6.92E+07# 1.00E+05* 8.35E # 19 # b1.01 * .90 # 5.44E+13* 1.57E+11# 6.92E+07# 1.07E+05* 8.35E # 20 # 64.40 * .95 # 6.04E+13* 1.57E+11# 6.92E+07# 1.07E+05* 8.35E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.94E+07# 1.15E+05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.98E+07# 1.16E+05* 8.85E # 23 # 74.56 * 1.10 # 5.37E+13* 1.42E+11# 6.98E+07# 1.16E+05* 8.85E # 24 # 77.95 * 1.15 # 5.57E+13* 1.39E+11# 6.79E+07# 1.16E+05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.35E+11# 6.35E+07# 1.11E+05* 8.85E # 26 # 64.73 * 1.25 # 5.26E+13* 1.35E+11# 6.35E+07# 1.11E+05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.35E+11# 6.35E+07# 1.03E+05* 8.85E # 29 # 94.90 * 1.40 # 4.44E+13* 1.29E+11# 6.35E+07# 1.03E+05* 8.85E # 29 # 94.90 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.03E+06* 8.85E # 30 # 35.29 * 1.45 # 4.15E+13* 1.25E+11# 5.50E+07# 3.03E+06* 8.85E # 31 # 101.60 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.03E+06* 8.85E # 31 # 101.60 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.03E+06* 8.85E # 31 # 101.60 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 31 # 101.60 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 31 # 101.60 * 1.40 # 4.44E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 31 # 101.60 * 1.40 # 4.45E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 31 # 101.60 * 1.40 # 4.45E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 31 # 101.60 * 1.40 # 4.10E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 32 # 105.07 * 1.45 # 3.32E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E # 32 # 105.07 * 1.40 # 3.24E+13* 1.29E+11# 5.50E+07# 3.27E+06* 8.85E	
# 15	
# 15 # 50.84	
# 17 6 54.23 * .80 # 5.44E+13* 1.66E+11# 6.62E+07# 9.26E+06* 3.85E # 19 # 57.52 * .85 # 5.74E+13* 1.61C+11# 6.90E+07# 1.00E+05* 8.35E # 19 # 61.01 * .90 # 5.94E+13* 1.57Z+11# 6.92E*07# 1.07E*05* 8.35E # 20 # 64.40 * .95 # 6.04E+13* 1.52E+11# 6.94E+07# 1.12E*05* 8.85E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.94E+07# 1.15E*05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.98E+07# 1.16E*05* 8.85E # 23 # 74.56 * 1.10 # 5.37E+13* 1.42E+11# 6.38E+07# 1.16E*05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16E*05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.66E+07# 1.14E*05* 8.85E # 26 # 64.73 * 1.25 # 5.26E+13* 1.33E+11# 5.51E+07# 1.09E*05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.33E+11# 5.51E+07# 1.09E*05* 8.85E # 27 # dd.12 * 1.35 # 4.73E+13* 1.29E+11# 6.17E+07# 1.03E*05* 8.85E # 29 # 94.90 * 1.40 # 4.44F+13* 1.29E+11# 5.98E+07# 9.37E*06* 8.85E # 31 # 101.65 * 1.45 # 4.15F+13* 1.25E+11# 5.50E+07# 9.37E*06* 8.85E # 32 # 105.07 * 1.55 # 3.37E*13* 1.23E+11# 5.50E+07# 3.63E*06* 8.85E # 34 # 103.46 * 1.60 # 3.26E+13* 1.20E+11# 5.50E+07# 3.63E*06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.19E+11# 4.92E+07# 7.13E*06* 8.85E	
# 19 # 57.52 * .85 # 5.74E+13# 1.61C+11# 6.9GE+07# 1.0GE-05# 8.35E # 19 # b1.01 * .90 # 5.44E+13# 1.57E+11# 6.92E*07# 1.07E*05# 8.35E # 20 # 64.40 * .95 # 6.04E+13# 1.52E+11# 6.98E*07# 1.12E*05# 8.85E # 21 # 67.79 * 1.00 # 6.05E+13# 1.49E+11# 6.98E*07# 1.15E*05# 8.85E # 22 # 71.15 * 1.05 # 5.99E+13# 1.45E+11# 6.96E*07# 1.16E*05# 8.85E # 25 # 74.56 * 1.10 # 5.37E+13# 1.42E+11# 6.48E*07# 1.16E*05# 8.85E # 24 # 77.95 * 1.15 # 5.71E+13# 1.39E+11# 6.79E*07# 1.16F*05# 8.85E # 25 # 31.34 * 1.20 # 5.50E*13# 1.35E*11# 6.66E*07# 1.14E*05# 8.85E # 26 # 84.73 * 1.25 # 5.26E*13# 1.35E*11# 6.55E*07# 1.09E*05# 8.85E # 27 # 31.51 * 1.35 # 4.73E*13# 1.31E*11# 6.35E*07# 1.09E*05# 8.85E # 29 # 94.40 * 1.40 # 4.44E*13# 1.29E*11# 6.17E*07# 1.03E*05# 8.85E # 31 # 101.54 * 1.50 # 3.36C*13# 1.25E*11# 5.78E*07# 9.89E*06# 8.85E # 32 # 105.07 * 1.55 # 3.37E*13# 1.25E*11# 5.78E*07# 9.87E*06# 8.85E # 34 # 103.46 * 1.60 # 3.28E*13# 1.25E*11# 5.58E*07# 3.63E*06# 8.85E # 34 # 111.85 * 1.50 # 3.36C*13# 1.29E*11# 5.78E*07# 7.70E*06# 8.85E # 34 # 111.85 * 1.50 # 3.28E*13# 1.20E*11# 5.78E*07# 7.70E*06# 8.85E # 35 # 115.24 * 1.70 # 2.74E*13# 1.19E*11# 4.92E*07# 7.13E*06# 8.85E	_
# 19 # 61.01 * .90 # 5.94E+13* 1.57E+11# 6.92E*07# 1.07E*05* 8.35E # 20 # 64.40 * .35 # 6.04E+13* 1.52E+11# 6.94E+07# 1.12E*05* 8.85E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.94E+07# 1.15E*05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.49E+11# 6.95E+07# 1.16E*05* 8.85E # 25 # 74.56 * 1.10 # 5.37E+13* 1.42E+11# 6.96E+07# 1.16E*05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16E*05* 8.85E # 25 # 61.34 * 1.20 # 5.50E*13* 1.36E+11# 6.66E*07# 1.14E*05* 8.85E # 26 # 64.73 * 1.25 # 5.26E*13* 1.35E*11# 6.55E*07# 1.09E*05* 8.85E # 27 # dd.12 * 1.30 # 5.26E*13* 1.35E*11# 6.35E*07# 1.09E*05* 8.85E # 28 # 94.90 * 1.45 # 4.73E*13* 1.29E*11# 6.17E*07# 1.03E*05* 8.85E # 29 # 94.90 * 1.40 # 4.44F*13* 1.27E*11# 5.98E*07# 9.89E*06* 8.85E # 30 # d8.26 * 1.45 # 4.15E*13* 1.25E*11# 5.56E*07# 9.87E*06* 8.85E # 31 # 101.58 * 1.50 # 3.36C*13* 1.25E*11# 5.56E*07# 9.87E*06* 8.85E # 32 # 105.07 * 1.55 # 3.37E*13* 1.23E*11# 5.56E*07# 3.63E*06* 8.85E # 34 # 111.85 * 1.60 # 3.28E*13* 1.20E*11# 5.56E*07# 7.70E*06* 8.85E # 35 # 115.24 * 1.66 # 3.28E*13* 1.20E*11# 5.15E*07# 7.70E*06* 8.85E	
# 20 # 64.40 * .35 # 6.04E+13* 1.52E+11# 6.38E+07# 1.12E-05* 8.85E # 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.38E+07# 1.15E-05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.45E+11# 6.38E+07# 1.16E-05* 8.85E # 25 # 74.56 * 1.10 # 5.37E+13* 1.42E+11# 6.38E+07# 1.16E-05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16E-05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.66E+07# 1.14E-05* 8.85E # 26 # 84.73 * 1.25 # 5.26E+13* 1.33E+11# 5.51E+07# 1.11E-05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.33E+11# 6.35E+07# 1.09E-05* 8.85E # 24 # 31.51 * 1.35 # 4.73E+13* 1.29E+11# 6.17E+07# 1.03E-05* 8.85E # 24 # 31.51 * 1.35 # 4.73E+13* 1.29E+11# 6.17E+07# 1.03E-05* 8.85E # 27 # dd.12 * 1.30 # 5.01E+13* 1.29E+11# 5.78E+07# 9.89E+06* 8.85E # 30 # 31.51 * 1.35 # 4.73E+13* 1.27E+11# 5.78E+07# 3.63E+06* 8.85E # 31 # 101.69 * 1.40 # 4.44F+13* 1.27E+11# 5.78E+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.23E+11# 5.58E+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.22E+11# 5.58E+07# 3.27E+06* 8.85E # 34 # 111.85 * 1.65 # 3.31F+13* 1.19E+11# 4.92E+07# 7.70E+06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E	
# 21 # 67.79 * 1.00 # 6.05E+13* 1.49E+11# 6.94E+07# 1.15E+05* 8.85E # 22 # 71.15 * 1.05 # 5.99E+13* 1.46E+11# 6.95E+07# 1.16E+35* 8.85E # 25 # 74.56 * 1.10 # 5.37E+13* 1.42E+11# 6.46E+07# 1.16E+05* 8.85E # 24 # 77.95 * 1.15 # 5.71E+13* 1.39E+11# 6.79E+07# 1.16E+05* 8.85E # 25 # 31.34 * 1.20 # 5.50E+13* 1.36E+11# 6.66E+07# 1.14E+05* 8.85E # 26 # 84.73 * 1.25 # 5.26E+13* 1.33E+11# 5.51E+07# 1.03E+05* 8.85E # 27 # 48.12 * 1.30 # 5.01E+13* 1.33E+11# 6.35E+07# 1.03E+05* 8.85E # 24 # 31.51 * 1.35 # 4.73E+13* 1.29E+11# 6.17E+07# 1.03E+05* 8.85E # 24 # 31.51 * 1.35 # 4.73E+13* 1.29E+11# 6.17E+07# 1.03E+05* 8.85E # 30 # 31.51 * 1.40 # 4.44E+13* 1.27E+11# 5.98E+07# 9.89E+06* 8.85E # 31 # 101.62 * 1.40 # 4.44E+13* 1.25E+11# 5.58E+07# 9.37E+06* 8.85E # 32 # 105.07 * 1.50 # 3.36C+13* 1.23E+11# 5.58E+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.23E+11# 5.58E+07# 3.63E+06* 8.85E # 34 # 111.85 * 1.60 # 3.23E+13* 1.20E+11# 5.15E+07# 7.70E+06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.19E+11# 4.70E+07# 7.13E+06* 8.85E	
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# 24 # 31.51 * 1.35 * 4.73E+13* 1.29E+11# 6.17E+07# 1.03E+05* 8.35E # 29 # 94.30 * 1.40 # 4.44E+13* 1.27E+11# 5.98E+07# 9.89E+06* #.85E # 30 # 35.29 * 1.45 # 4.15E+13* 1.25E+11# 5.78E+07# 9.37E+06* 8.85E # 31 # 101.5* * 1.50 # 3.36C+13* 1.23E+11# 5.58E+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.22E+11# 5.36E+07# 3.27E+06* 8.85E # 4 # 103.46 * 1.60 # 3.23E+13* 1.20E+11# 5.15E+07# 7.70E+06* 8.85E # 34 # 111.85 * 1.65 # 3.01E+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E	-12
# 29 # 94.30 * 1.40 # 4.44F+13* 1.27E+11# 5.98E+07# 9.89E+06* 8.85E # 30 # 38.29 * 1.45 # 4.15F+13* 1.25E+11# 5.78E+07# 9.37E+06* 8.85E # 31 # 101.5* * 1.50 # 3.36C+13* 1.23E+11# 5.58E+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.22E+11# 5.36E+07# 8.27E+06* 8.85E # 4 # 103.46 * 1.60 # 3.23E+13* 1.20E+11# 5.15E+07# 7.70E+06* 8.85E # 34 # 111.85 * 1.65 # 3.01F+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E	-12
# 30 # 48.29 * 1.45 # 4.156+13* 1.256+11# 5.786+07# 9.376=06* 8.856 # 31 # 101.69 * 1.50 # 3.366+13* 1.235+11# 5.586+07# 3.636+06* 8.856 # 32 # 105.07 * 1.55 # 3.376+13* 1.226+11# 5.366+07# 8.276+06* 8.856 # 4 # 103.46 * 1.60 # 3.236+13* 1.206+11# 5.156+07# 7.706+06* 8.856 # 34 # 111.85 * 1.65 # 3.016+13* 1.196+11# 4.926+07# 7.136+06* 8.856 # 35 # 115.24 * 1.70 # 2.746+13* 1.186+11* 4.706+07# 6.566=06* 8.856	-12
# 31 # 101.69 * 1.50 # 3.36c+13* 1.23E+11# 5.5dE+07# 3.63E+06* 8.85E # 32 # 105.07 * 1.55 # 3.37E+13* 1.22E+11# 5.36E+07# 8.27E+06* 8.85E # 43 # 103.46 * 1.60 # 3.23E+13* 1.20E+11# 5.15E+07# 7.70E+06* 8.85E # 34 # 111.85 * 1.65 # 3.01E+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.1dE+11# 4.70E+07# 6.56E=06* 8.85E	
# 32 # 105.07 * 1.55 # 3.576+13* 1.226+11# 5.366+07# 3.276+06* 3.856 # 33 # 103.46 * 1.60 # 3.236+13* 1.206+11# 5.156+07# 7.706+06* 8.856 # 34 # 111.85 * 1.65 # 3.316+13* 1.196+11# 4.926+07# 7.136+06* 8.856 # 35 # 115.24 * 1.70 # 2.746+13* 1.186+11* 4.706+07# 6.566=36* 8.856	
# 43 # 103.46 * 1.60 # 3.28E+13* 1.20E+11# 5.15E+JP# 7.70E+06* 8.85E # 34 # 111.85 * 1.65 # 3.31E+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.18E+11# 4.70E+07# 6.56E=96* 8.85E	
# 34 # 111.95 * 1.65 # 3.31F+13* 1.19E+11# 4.92E+07# 7.13E+06* 8.85E # 35 # 115.24 * 1.70 # 2.74E+13* 1.1dE+11# 4.7uE+07# 6.56E=96* 8.85E	
# 35 # 115.24 * 1.70 # 2.74E+134 1.1dE+11# 4.7uE+07# 6.56E-76* 8.35E-	-
#	
# 39 # 124.79 * 1.90 # 1.735+13* 1.14E+11# 3.73E+07# 4.416-36* 8.855	
# 40 # 132.16 * 1.95 # 1.555+13* 1.13E+11# 3.56E+37# 3.92E+3E* 9.85E	-
# 41 # 135.57 * 2.00 # 1.395+13* 1.136+11# 3.336+07# 3.456+06* 8.856	
# 42 # 130.96 * 2.35 # 1.208+13* 1.128+11# 3.118+07# 3.018+06* 8.858	-
# 43 # 142.35 * 2.10 # 1.020+13* 1.11E+11# 2.67E+07# 2.58F+06* 3.45F	
# 44 # 145.74 * 2.15 # 8.65F+12* 1.112+11# 2.65E+07# 2.20E+36* 8.85E	
# 45 # 143.13 + 2.23 # 7.156+12+ 1.116+11# 2.416+07# 1ca36+06+ 5.556	
# 45 # 152.52 * 2.25 # 5.475+12* 1.10E +11# 2.10E+07# 1.5GE+35* 8.85E	
# 47 # 155.91 * 2.30 # 4.646+12* 1.10E+11# 1.35E+0/# 1.19E+06* 8.85E	
# 41 # 154.30 * 2.35 # 3.540 +12* 1.395 +11# 1.695+07# 9.100 -07* 6.555	
# 49 # 162.69 * 2.40 # 2.578+12* 1.09£+11# 1.44E+07# 6.63E+37* ±.85E	
# 50 # 166.04 * 2.45 # 3.900+11* 2.316+10# 5.606+05# 4.930+07* d.456	
# 51 # 164.46 # 2.50 # 2.195+11* 2.218+10# 4.2JE+06# 2.766+J7* 9.856	-12

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222	****		***	*******	2 2 1	*********	********	********		******
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	_	6.7		.10		6.98E+13*				· · · -
•	4	10.1		.15	•				7.99E-06*	
₽ A	5 6	# 13.5 # 16.9		•?G •25	#	3.335+13* 2.21E+13*		5.62E+07# 4.22E+07#	5.G4F-06*	
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*	11 12	# 35.6 # 37.2		•50 •55	•	9.84E+12* 1.986+13*			1.42E-06* 2.33E-J6*	8.85E-12#
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•	14	# 44.0		.65		3.61E+13*		5.40E+07#		_
•	15	47.4		.70		4.25E+13*			-	8.855-12#
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ě	13	61.0		.90	#	5.65E+13*			1.016-05*	8.556-12#
		64.4	0 •	. 25	#	5.76E+13#			1.06E-05*	8.85E-12#
•	21	67.7	-	1.00		5.74E+13*			-	8.85E-12#
#		# 71.1		1.05		5.73E+13*	-			8.85E-12#
*	23 24	# 74.5 # 77.9		1.1C 1.15		5.63E+13* 5.43E+13*			1.11E-05*	4.85E-12#
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		# 54.7		1.25		5.035+13*			1.07E-05*	8.85F-12#
•		69.1		1.30		4.94E+13*			1.04E-05*	8.35E-12#
	23	# 31.5		1.35		4.5 4E+13*			9.535-064	3.85E-12#
;	24 30	# 44.9 # 49.2		1.49 1.45	#	4.32[+13* 4.05E+13*				8.85E-12#
	31	# 101.5		1.50	#	3.776+13*				8.855-12#
#	32	# 105.0		1.55	#	3.50E+13+				d. 35E-12#
	33	# 108.4	_	1.60	#	3 • 2 3F + 1 3*			7.555-06*	8.555-12#
#		# 111.9		1.65 1.70	*	2.978+13*			1 /.01E-06* 6.47E-06*	8.85E-12#
·		* 115.2 * 115.5		1.70					5.94E-36*	
		# 122.0		1.80					5.42E-06*	
•		# 125.4		1.85	#	2.01 +13*	1.15E+11#	4.02E+07#	4.91E-06+	3.855-12#
*		# 128.7		1.90					4.438-06*	
		# 132.1 # 135.5		1.95 2.00					3.56E=06*	
*		# 139.3 # 139.3		2.05					3.09E-06*	
		# 142.1		2.10					2.665-06*	
*	44	145.7	4	2.15	#	9.11F+12*	1.116+11#	2.71E+07#	2.31E-06*	9.95E-12#
		# 143.1		2.20					1.945-064	_
		# 152.5 # 155.9		2.25 2.30					1.61E-36*	
		# 153.3		2.35					1.00E-36*	
#		152.6	•	2.40					7.24E-07+	
#	_	# 166.0		2.45	#	1.648+12*	9.51E+16#	1.158+07#	4.36E-07*	8.855-12#
#	_	# 167.4		2.50					2.75E-37*	
= 2 = 1	- 	=======	: = = = = :	:	= = :	=========		=======================================		=======================================

MAXIMUM CONDUCTIVITY : 1.52E+05 (MHOS/M) 118

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******	:::::::::::::::::::::::::::::::::::::::			****************
#FOINT4	S# NOZZLE		REDEYE #	FREQUENCY #
# 9.00			5000(FT)/10(FT/S) #	
# (M)	# (M	PRESSURE +	0.432 (ATMCSPHERES#	(HZ) #
RESESS	222222222			
		AESCLUTE# ELECTRON*(SIGMA # EPSILUN #
# INDEX	# RACIUS *		REQUENCY#FREQUENCY#	•
•		(M) 0 (1/M3) 4	(1/S) # (1/S) #	(MHQ/M) + (FD/M) #

* 1	# 0.00 *		2.23E+11# 8.62E+07#	
# 2	# 3.39 *		2.23E+11# 9.30E+07#	
# 3	# 5.76 *	- · · · · · · · · · · · · · · · · · · ·	2.22E+11# 7.48E+07#	
# 4		***	2.2JE+11# 6.32E+07#	
# 5	# 13.56 *		2.16E+11# 5.05E+07#	
# 6			2.16E+11# 3.35E+07# 2.12E+11# 2.35E+07#	
-				7.23E=07* 8.85E=12#
# 8			2.04E+11# 1.55E+07#	
# 3				3.83E-37* 9.85E-12#
# 10	" "			1.27E-064 9.35E-12#
# 11	# 33.39 *			2.72E-06* 8.85E-12#
# 12	"		1.46E+11# 4.65E+07#	
# 13	" 1000.			5.32E+06* 8.35E-12#
# 14	" "			5.44E-06* 8.95E-12#
# 15	# 47.45 * # 50.84 *		1.71E+11# 5.03E+07#	
# 16 # 17			1.65E+11# 6.29E+07#	
	# 54.23 * # 57.62 *			*****
# 18 # 19	# 61.01 *			
# 23				
. # 21	# 64.40 * # 57.79 *			
# 22	# 71.15 #		1.466+11# 6.666+07#	
2 23	# 74.56 *			1.07E-05* d.85E-12#
# 24	# 77.95 #		1.40E+11# 6.53E+07#	
# 25	# 31.34 *		1.37E+11# 6.42E+07#	-
# 26	# 84.73 *	_	1.35E+11# 6.29E+07#	
# 27	# 69.12 *	• • • • • • • • • • • • • • • • • • • •	1.32E+11# 5.15E+07#	1.00E-05* 8.35E-12#
# 28	# +1.51 *			
# 23	# 94.90 *			9.27E-06* 3.85E-12#
* 30	# 93.29 #			d. 84E-06* 8.85E-12#
# 31	# 101.68 #			
# 32	# 105.37 *			7.89E-06# 8.85E-12#
# 33	# 104.46 #	-		7.39E-06* 8.85E-12#
# 34	# 111.95			
# 15	# 115.24	1.79 # 2.69E+13*	1.19E+11# 4.65E+07#	6.3cE-06# 8.85E-12#
# 36	# 115.67 *	1.75 # 2.45E+13*	1.17E+11# 4.44E+07#	5.87E-06+ 8.45E-12#
# 37	# 122.01 *	1.30 # 2.23E+13+	1.15E+11# 4.24E+07#	5.39E-06* 8.85E-12#
# 39	# 125.40 *	1.85 # 2.610+13*	1.15F+11# 4.02E+07#	4.90F-06+ 8.85T-12#
# 39	# 129.79	1.90 # 1.616+13*	1.15E+11# 3.32E+07#	
# 43	# 132.19 *		1.14E+11# 3.60E+07#	
# 41	# 135.57 .		1.13E+11# 5.40E+07#	
# 42	# 134096 *		1.13E+11# 3.13E+07#	
# 43	# 142.35 *	2.10 # 1.10F+13*	1.126+11# 2.976+07#	2.76E+15+ 6.85E+12#
# 44	# 145.74 *	2.15 # 9.478+12+	1.12E+11# 2.76E+07#	2.39E-06* 0.45E-10#
# 45	# 144.13 4	2.20 # 6.357+12*	1.116+11# 2.556+07#	2.04E+06* 3.85E+12#
# 46	# 152.52 *	2.25 # 6./6F+12*	1.11E+11# 2.'4E+07#	1.72F-06* 9.85E-12#
# 47	# 155.91	2.70 # 5.526+12#	1.106+11# 2.116+07#	1.416-06* 3.855-12#
# 49	# 154.30 *	2.35 # 4.42F+12*	1.1JE+11# 1.93E+07#	1.13F-06" 5.85E-12#
# 43	# 162.59		1.13E+11# 1.64E+37#	
# 50	# 165.JS		1.095+11# 1.40E+07#	
# 51	# 153.40		1.0-E+11# 1.11E+37#	
======	=======================================			*************

#	* = = = = :	: =	1122222	:==:		= :	=======	===	:====	2223		======	212227121:	*=======
# 1	FOINT47	*	NOZZL	.E #	RACILS	# (ROCKET	1	REDEY	Ē			FREGU	ENCY #
#	4.20	#	1.	486	E-02	# (POSITION	4	50000	FT)	148	(FT/S) #	2.50	E+08 #
#	(M)	#		(M))	#1	PRESSURE	1	0.832	(AT	MUS	SPHERESE	(H	Z) #
# :	* * * * * * * *	: z	=======	===	========	= :		: : :		2225	===	======	8535222222	22222222
					ABSCLUTE							PLASMA #	SIGMA 🐣	EPSILON #
	INDEX	#	FADIUS	. •		#	DENSITY	* F	REQUE	NCY#	FRE	EQUENCY#	#	#
#		#		4	(+)	#	(1/M5)	#	(1/S) #) ((1/S) #	(MHC/M) *	(FD/M) #
= :			=======			= :							*****	
	1	#	0.00	-	0.00								8.48E-06*	
	2	#	3,39	-									7.915-06+	
	3	#	6.78	#		#	5.14E+13			_			6.56E-06*	
-	4 5	¥	10.17	#									4.62E-06#	
7	6	#	13.56	*		#							3.21E-96*	
-	7	*	16.95 20.34	*	•25 •30	7							1.96E-06*	
- T	8	4	23.73	*	•35	#							6.32E-07*	
#	9	*	27.11	•	.48	#							3.688-07*	
	10	#	30.50	*									3.44E-07+	8 - 85E-12#
#	11		33.89	#	.50	#							1.13E-06*	8.85E-12#
	12	#	37.28	#	.55	*	1.70E+13						2.51E-06*	
#	13	#	40.67	*	.60		2.516+13						3.81E-06*	
#	14	#		#							-		5.00E-06*	
*	15	#	47.45	#	.70	#	3.802+13						6.08E-36#	
#	16	#	50.84	*	.75	#	4.28E+1	5*	1.71E	+11#	5.	37E-07#	7.03E+96*	8.85E-12#
#	17	#	54.23	#	• 30	#	4.66E+13	5 #	1.67E	+11#	6.	13E+07#	7.86E-86#	8.85E-12#
#	13	#	57.62	#	.85	Ħ	4.94E+13	5+	1.62E	+11#	6.	31E+07#	8.57E-06*	8.85E-12#
#	19	#	61.01	#	.90	#	5.14E+1	5 *	1.5 ₺E	+11#	6.	43E+07#	9.15E-06*	0.35E-12#
#	20	#	64.40	#	• 95	#	5.25F+13						3.60E-06*	
#	21	#		*		#	5.238+13						9.90E-06*	8.95E-12#
#	22	#	71.18	*		#	5.270+13		1.47E			-	1.01E-05*	6.85E-12#
#	23	#	74.56	*	1.10	#	5.1 JE+13						1.02E-05*	8.85E-12#
#	24	#		*	1.15	#	5.096+13						1.02E-05*	
-	25 26	#	81.34 64.73	*	1.20	*	4.938+13						1.01E-05*	
-	27	#		*	1.25 1.30	#	4.74E+13		1.35E	_			5.89E≈06* 9.65E=J6*	8.85E-12#
#	28	#	91.51	*	1.35	#							9.03E-06*	
#	29	#		*	1.40	#	4.035+13						8.975-06*	
	36	ø		*	1.45	#	3.356+1					-		-
*	31	#		#	1.50	#	3.51E+1						_	
#	35	it	165.67	+	1.55	#	3.36E+13		1.23E				7.708-36*	
#	33	#	103.46	•	1.60	#							7.24E-06*	8.85E-12#
#	34	#	111.85	*	1.65	Ħ	2.896+13	3 +	1.2JE	+11#	4.	825+07#	6.76E-06#	3.85E-12#
#	35	#	115.24	•	1.70	#	2.666+13	5#	1.19E	+11#	. 4.	63E+07*	6.29E-06+	8.456-12#
#	36	ŧ	110.63	₩.		Ħ	2.43E+13	5#	1.13E	+11#	14.	43E+07#	5.81F-06*	8.85E-12#
#	37	#	155.01	#									5.35E-06*	
#	" 4			#									4.99E-06+	
#	33		128.79	*									4.44E-36*	
#	40		132.15	#									4.0CE-06*	
	41		135.57	*									3.60E-06*	
#	42		138.96	*									3.196-76*	
#	43			#4 P1									2.e3F=06*	
#	44		145.7	- 65 - 4 4									2.47E=06*	
#	45 46		149.13 152.52	-									2.145-06*	
#	47		192.97	•									1.83E-06* 1.54E-06*	
#	44		154.30	*									1.288-06*	
#	49		152.69	*									1.01F-06*	
	50		165.04	*									7.86F-07*	
#	51		161.46	*									5.52E-07*	

*		= =		. = 2 :	222222	* = 1	:::::	=:22	315:	===	111	#32:	****	. = =		====
	FCINT4	3#	NCZZL	jë F	ACILS	# F	OCKE	T	t RE	DEY	Ε				FREGUENCY	
*	9.40	#	1.	486	-02	# (CSIT	ION	1 50	0000	FT)	/10	(FT/SI	#	2.50E+08	#
	(H)	#		(M)		4.5	PRESS	URE	. 0.	832	(A	THU	SPHERE	55₽	(dZ)	
=		==	=======	====	******	===	====	====	= 2 2 2	3 = =	3 3 3	## # #	=====	3 = 2	* # # 2 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	====
#	RADIAL	. #	RELATIV	IE+	AESCLUT	E#	ELEC	JOST	* COL	LIS	ICN	# 1	PLASM	4	SIGMA # EPSIL	ÜN #
#	INDEX	#	RACIUS	5 *	PACIUS	#	DE:15	ITY	+ FQE	QUE	NCY	#F 26	EQUEN	CY#	•	
		#		#	(٢)	#	(1/	M3)	* (11/5)	#	(1/5)	#	(MHU/M) * (FD/	M) #
I	* * * * * * * :	=	=======	====			====						****			# # # # #
	1	#	0.00	•	0.00										5.29E-06+ 8.85E	
#	2	#	3.39	*	.05			_	-	_					4.99E-06* 3.85E	
#	3	#	6.78	*	.10			_							4.28E-06# 5.85E	
	4	#	10.17	4	•15		2.56			_					3.31E-06# 8.85E	
	5	#	13.56	*	•20										2.32F-06+ 8.85E	
#	6	#	16.95	*	•25										1.51E-06* 8.35E	
#	7	7	20.34	*	•30							_		_	9.048-074 8.855	
	5 9	#	23.73	*	.35										5.39E+07* 8.85E 3.23E+07* 9.85E	
	19	*	30.50	4	.40 .45		2.15								3.14E-07+ 8.85E	
-	11		33.89	•	•50			L+12							9.86E+07* 3.85E	
*	12	#	37.28	*	•55	#		_	_						2.31E-06* 8.05E	
	13	-	46.67		.60		2.34		_						3.55E-06+ 8.85E	
4	14	#	44.06	#	.65					_					4.68E-06* 8.55E	
	15	#	47.45	*	.70	#		F +13							5.71E-06+ 8.85E	
#	16	#	50.64	*	.75	#									6.63E-06+ 8.85E	
#	17	#	54.23	*	.80		4.41								7.42E-06* 8.855	
#	19	#	57.62	•	.85	#		£ +13	_		-				8.10E-06* 8.85E	-12#
#	19	#	61.01	#	•90	#	4.88	E +13	- 1	5 9E	+11	# 5	.27E+	07#	8.66F-06* 8.85E	-12#
#	2 G	#	64.41	•	•95	#	5.00	E+13	+ 1	. 55E	+11	# 6	. 35E+	7#	9.10E+06* 9.85E	-12#
#	21	#	67.79	*	1.00	#	5.05	E+13	* 1	51E	+11	# 6	.38E+	7#	9.41E-06+ 8.85E	-12#
	5.5	#	71.18	#	1.05	#	5.04	t +13							9.61E-06* 8.85E	
#	23	#	74.56	#	1.10	#	4.98	E +13							9.71E-06* 9.35E	
#	24	#	77.45	*	1.15	Ħ	4.89								9.74E-06* 8.85E	
#	25	#	31.34	#	1.20	Ħ		E+13			+11				3.66E+06+ 8.35E	
#	25	#	64.73		1.25		4.56								9.50E-06* 3.85E	
#	27	#	34.12	*	1.30		4.39	-							9.29£-36* 8.85E	
	24	#	91.51	*	1.35										9.01E+JE+ 4.85E	
#	24	#	94.90	*	1.40		-	-	-		-				8.68696* 8.856	
#	30	#	94.29	*	1.45		3.77								7.33E-06* 8.35E	
#	31 72	#	101.68		1.50	#									7.936-06* 8.956 7.526-06* 8.856	
#	32 3₹	死	165.87 188.46	*	1.55 1.60		3.30 3.07				+11				7.09F-06# 8.85E	
#	34	#	111.55	•	1.65		2.35				+11		.79E+			
*	35	er di	115.24	•	1.70										6.20E-06* 8.35E	
#	36		113.63		1.75										5.75F-06* 8.85E	
#	37		122.01	•	1.60										5.31E-06+ 4.45E	
#	3 b		125.40	•	1.85										4.66E+J6# 8.456	
#	33		128.79	*	1.90										4.45E-06* 3.35E	
#	40		132.16		1.95										4.02E-06* 5.35E	
#	41		135.57	*	5.00										3.64E-76+ 3.85E	
#	42	#	134.96	4	8.05	#	1.50)F +1 3	* 1	. 1 SE	+11	# 5	.24E+	07#	3.24E-36# 8.95 <i>E</i>	-12#
#	43	H	142.35	*	2.19										2.90E+06* 8.855	
#	44	Ħ	145.74	*	2.15										2.555-46+ 4.955	
#	45		149.13	*	5.53										2.245-06* 3.855	
ø	46		152.52	+	2.25										1.945-06* 3.858	
#	47		155.71	*	c . 3 C										1.67E-36+ 8.356	
#	49		153.30	#	2.35										1.425-96* 8.355	
#	4.3		162.59		2.40										1.17E-064 8.45E	
#	50		150.38	*	2.45										9.4-6-374 8.855	
#	51		163.46	*	2,53										: 7.J4E+67* 6.556 :=========	
3		_ =	_ = = = = = =	:		_ =	_ ~ = = =					ڪ ښت				

282	****	=	*****	===	=======	# Z :	******	3 2 :	******	22:2222231	**********	ar regent
#50	INT49	#	NOZZ	LE F	FACIUS	# 6	FOCKET		REDEVE	4	FREQUE	NCY #
	9.60	#	1	.481	E-02	# 1	FOSITION	ŧ	5000(FT)	/10(FT/S) (2.509	+08 #
#	(M)	#		(M)		# 5	PRESSUPE		0.832 (A	THOSPHE: ESI	; (H2	Z) #
***	22222	: =		222	= 3 2 2 2 2 2 2	**	*======	==:		********		********
# R	ADIAL	. #	RELATI	VE*	AESCLUY	E#	ELECTRO	N# (COLLISION	# PLASMA #	SIGMA +	EPSILON #
	NDEX		RADIU							FREQUENCY!		•
		#		*	(4)	#	(1/M3)				(MHC/M) *	(FD/H) #
222	2224	:=	222222	. = = = :	======	22:	**=====	23:				*******
	1	#	9.90) #	0.00		1.60E+1	3#	2.20E+11	# 3.60E+07#	2.06E-06+	8.85E-12+
4	ž	4	3.39		. 05						2.055-06*	
Ä	3		6.78		.10		1.54E+1				1.99E-06*	
	4		10.17		.15						1.78E-06*	
Ä	5	×	13.56		.20						1.43E-06*	
-	6	Ĭ	16.95		.25		7.95E+1				1.05E-06*	
7	7		20.34		.30						6.87E-07+	
*		Ä	23.73		.35					# 1.62E+07		
	9	*	27.11		•40						2.77E-07+	
7	10	7	30.50		.45						2.64E-07*	
"	11	*	33.89		.50						8.43E-07#	
7		7	37.26		•55		1.42E+1				2.10E-J6+	
# 4	12 13	#	40.67		•60		2.17E+1				3.29E-06+	
#							2.30E+1	-			4.37E-06*	
#	14	#	44.36		•65		3.35E+1				5.35E-36*	
#	15	φ 4	47.49		.70						* 6.22E-06*	
#	16	#			. 75						# 6.99E-06+	
*	17	*	54.23 57.52		• 80 • 85		4.15E+1				7.64E-J6*	
#	18	#									* 8.19E-06*	
#	13		61.01		• 90	7					# 8.61E-06+	
#	23	#			.95	77						
#	21	#	• • •		1.00						# d.92E-96#	
#	22	#			1.05						# 9.13E-06* # 9.25E-06*	
# #	23	#			1.10	#				# 6.14E+97		8.85E-12#
#	24	#			1.15	F A	4.68E+1				# 9.24E-06*	
#	25	#	41.34		1.20	*						
#	26	#			1.25	#					# 9.11E-06#	8.35E-12#
#	27	#			1.39	#	4.25E+1			# 5.85E+07		8.85E-12#
#	23	#			1.35	#	4.06E+1			# 5.72E+07		
#	29	#	74.9		1.40	#					# 8.40E-064	8.856-12#
#	30	ñ			1.45	F	3.665+1			# 5.43E+07		9.85E-12#
*	31	#	101.6		1.50	#	3.44E+1				# 7.71E-064	8.956-12#
#	32	7	135.07		1.55	*			1.24E+11		# 7.34E-06+	
#	33	释	108.46		1.60						# 6.93E-16* # 6.52E-16*	
₹	34	#	111.89				2.316+1				# 6.10E-06+	
#	35		115.24		1.70	# #	2 43544	. J =	1 105 444	* 4*20270/3	# 5.68E-06+	4.855-124
#	35		114.63		1.75						# 5.27E-06+	
#	37		122.01		1.30	₩	2 0 2 UNT 1	24	- 40 おりたマムル - 1 - 17ピムイイ	# 40CAGTU! # 4.39F487	# 4.85E-06+	A ASE-124
#	39		125.40	•							# 4.45E-16+	
#	39		124.79	•	1.90						# 4.04E-86*	
#	40	#		-		4	4 605 41	. J ·	4 1/6 414	# 2 67EAD7	# 5.68E-06*	8.45F=12#
# #	41		135.5								# 3.295-36*	
#	42		138.90	-		#	1 40574	.j~ ∡&	4 - 1 - 25 - 4 - 4	.ㅠ .Josific 7 U f # .4.13E*1.7	# 2.97F-06*	A ARF-124
#	43	ŧ,	142.5		2.10						# 2.62E-06+	
#	44	#	145.7			#	1 • UDE +1	⊤د. سدرہ	1-1-25-41	# GOTUETU!	# 2.34E=J6*	4.455-124
#	45	#	_								# 2.05E-06+	
#	46		152.5								# 1.80E-06+	
#	47		155.9			#	7 . U 01. + 1	2"	1 145 44	. マービャンサビマリ/ ・ローフ・フラビエルサ	# 1.555=NE#	0 + 335 = 1 2 # 4 - 15 F = 1 2 #
#	4.9	#	·=			18 14	D. 110. 41	. C =	1.116.711	# 2026ETU/ # 2 265497	# 1.56E-06+	4.455=12#
#	43	#				#	5.181+1	→ ک	1.106+11		# 1.32E-06+	0+3755404 0-455404
#	50	#				#	4.336+1	. C T	1.105+11		# 1.11t-06* # #.56F-07*	0 + 0 7
#	51	#	164.4								# 0.90: -11/T	

*		# 1	*******	= = :	::::::::::	E Z :	====	::::::		****	2272	2:2:		223		******
#	PCINT50		HOZZLI	Ε.	ADILS	# 5	COCKE	T	ı	REDE	Y E				FREGUE	NCY #
	9.40	#	1.0	481	-02	# (CSI	NOL	1	5000	(FT)	/10	(FT/S)	#	2.505	+09 #
	(H)	#		(M)		#1	PESS	SURE		0.83	2 (A	THOS	SPHERE	SF	(HZ	*
=	*****	= =	******	= 3 :		: 2 :		2223	= = =	====	= = = =	###	=====	==:		3 = 3 = 3 = 1 3 =
	PADIAL		RELATIV	E#	ABSCLUTE	#	ELEC	CTROI	N# C	OLLI	SICN	# (PLASMA	. #	SIGMA *	EPSILUN #
	INDEX	#	RACIUS	#	RACIUS		DENS	SITY	+ F	REJU	ENCY			Y#	*	
		#		*	(M)	#	(1/	/M3)	#	(1/	s)	#	(1/5)	#	(HKOHK)	(FD/M) #
#		===	=======	= = :		: : :		====		2222				3 3 :		21121111
	1	#	0.00	#	0.60	#	0 •			2.13			0.	#		8.85E-12#
	2	#	3.39	#	•05	#	0.			2.18			D •	#		8.55E-12#
#	3	#	6.78	#	•10	#	0.			2.17			û •	#		8.85E-12#
	4	#	10.17	*	.15	#									2.32E-07*	
	5		13.56	*	•20	#										8.85E-12#
	6	₩	16.95	*	.25	#									- '	
	7	*	20.34 23.73	#	.30 .35	-		_	_			_				8.85E-12#
#	9	*	27.11	#	• 40	-										8.85E-12#
-	10	-	30.50	*	.45		1.5		-							8.85E-12#
-	11	#	33.99		.50		4.8								5.99E-0;	8.85E~12#
*	12	*	37.2e	*	.55		1.2									
	13		40.67	*	.60		1.9									8.85E-12#
	14		44.16	#	.65											8.45E-12#
	15	4	47.45	#	.76	#		26 +1								8.85E-12#
	16	#	50 . 44	#	.75	#				1.72	E+11	# 5	. 36E+0	7#	5.82E-06+	8.85E-12#
	17	ø	54.23	#	.80								.51E+0			8.85E-12#
	19	#	57.62	*	.05	#	4.1	0E+1	3*	1.64	E+11	# 5	. 40E+0	7#	7.18E-06+	8.85E-12#
#	19	#	61.01	*	•90	#	4.3	7E+1	3#	1.60	E+11	# 5	. 34E+0	7#	7.71E-06+	8.55E-12#
	20	#	64.46	#	.95	#	4.5	Bt +1	3#				. 02E+0			
#	21	#	67.79	*	1.00	#	4.5	6F+1	3*							3.95E-12#
#	22	#	71.18	#	1.05	#	4.5	85 + 1	3*							
#	23	#	74.56	*	1.10	#	4.5								8. 80E-06*	
#	24	#	77.95	*	1.15	#	4.4						. 01E+0			
#	25	#	51 - 34	*	1.20	#		9E+1					. 342+0			8.85E-12#
#	26	*	34.73	*	1.25	#		5E+1							8.73E-06*	
	27	#	83.12	*	1.39	#							.75£+0			8.85E-12# 8.85E-12#
- 1	2.5	#	91.51	*	1.35	#							•50E+0		8.37E-06*	8.85E-12#
#	29 39	#	94.90 98.29		1.40 1.45	-									7.e3E-0E*	
-	31	*	101.68	+	1.50											
	25	7	105.07	4	1.55	#									7.16.5-16*	8.85E-12#
	3 s	#	168.46	#	1.60	#										
#	34		111.15	*	1.65	ı.							.72E+0			
#			115.24	#	1.70	ü	2.5	75 +1	3+	1.20	E+1	# 4	. 55E+i	7#	6.01E-06*	
			115.63	#	1.75										5.625-06*	
#			122.01	#	1.80	#	2.1	3E+1	3*	1.13	E+1)	# 4	. 20E+0	17#	5.236-06*	8.95E-12#
#	34		125.40	•	1.e5	#	2.0	1f +1	45	1.17	£ +1:	# 4	.02E+0	7#	4. # 3E-06*	8.35E-12#
#			128.79	*	1.90	#	1.8	4f +1	3*	1.15	۲+1:	L# 3	. 35E+C	7#	4.465-964	8.85E-12#
#	43	P	132.15	#	1.45	#	1.6	60 + 1							4.U5E-J6*	
#	41	pŧ	135.57	*	2.90		1.5								3.727-36*	
#			134.96	4	2.05		1.5								5.34F.+JE+	
#			142.35	*	2.19		1.2						.14E+			
#			145.74	*	2.15	#	1.0	5E+1	3#	1.18	E+1:	L# 2	• 35L+(7#	2.70E-36*	3.85E-12#
#			144.13	#	2.20	#	9.7	2F +1	2*	1.12	E+1:		-30E+(17#	2.44E-jf+	8-85E-12#
*			152.52	*	2.25	#	ċ.5	i: +1	2#	1.12	L +1:	16 5	. 625+(1/#	2.155-064	で・サッシュー17年
#			155.71	*	2.30	#	7.6	Jb. + 1	ک ہ	1.11	t +1:	18 6	48t+1) / # 1 7 #	1.93E-06*	3.57E-12#
#			154.30	*	2.35										1.715-06*	
#			162.59	*	2.43	#	2.6	75.+1 75-4	ر د حور	1 . 1 .	C. T.L.		0.05E-71) (# } 7 #	1.4°E-06* 1.27E-06*	3 - 37E-12#
#			165.00 460.60	*	2.45	#	- 49 e 7/ - 7 - 3	76.71	2 T	4 40	C - 1	14 C	・リリにマレ	2 (M 1 7 #	1.01E-36*	4.85F-12#
#	51	7#	169.46												1.016-36	

The second secon

*		: #	*****	857	*****		*******		****	****	222222	* = :		******	22
#1	FOINTS:	L #	NU 27	LE (HACIUS	# 5	ROCKET		REDEY	E			FREQU	ENCY	3
#	10.00	#	1	. 4 3	E-02	# 6	POSITION	ŧ	5000(FT)/	10 (FT/S)	#	2.50	E+08	#
#	(16)	#		(H)	# 5	PRESSURE		0.832	(AT	MOSPHERE	5#	(H	2)	#
3:	322233				*******									2222222	==
#			_		ABSOLUTE		-							EPSILON	. #
#	INDEX	*	RACIU	5 🛨		#				_	FREQUENC		# 4 hái i 6 4 m		
		* 	32:3:22	.	(M)		(1/M3) :======		(1/5		: (1/S)			(FO/M)	
_	1		0.00		0.00	#	G •		2.17E				0. •	8.85E-1	78
•	2	4	3.39		•05	#	0.		2.175		• •		0. +		
	3				.10	*	0.		2.16E			ě	ā. •		
#	4	#	10.17		.15	#	0.	*	2.15E	+114			0. •	5.85E-1	24
#	5	#			•20	#	0.	*	2.13E	+114	0.	ŧ	0. *	5.85E-1	12#
	6	#	16.95		•25	#	1.03E+1	2#	2.11E	+114	9.12E+0	6#	1.34E-07#		
#	7	#	20.34	#	•30						1.21E+0		2.47E-07		
#	8	#	23.73		•35				-		1.23E+0		2.59E-07*		-
#	3	#	27.11		• 40								1.056-07-		
#	10	#	30.50		•45								1.84E-07*		
	11	*	33.89		•50						1.75E+0		5.54E-074		
#	12	#	37.28		•55						3.02E+0		1.68E+06*		
#	13	#	40 - 67		•60		1.82E+1.				: 3.83E+0 : 4.40E+0		2.77E-06*		
-	14 15	#	44.06 47.45		•65 •70		2.40E+1				4.84E+0		4.62E-06		
4	16	#			.75		3.32E+1				5.17E+0		5.42E-06		
	17		54.23		.80		3.668+1						6.12E-06*		
	18	#	57.52		.85		3.92E+1				5.62E+0		6.72E-06*		
#	19	#	51.01		.90		4.125+1		_				7.24E-96*		12#
#	20	#	64.40	#	.95	#	4.250+1	3#	1.57E	+114	5.45E+0	7#	7.65E-06*		
	21	#	67.79	*	1.09	*	4.32E+1	3#	1.53E	+114	5.30E+0	7#	7.96E-064	8.858-1	12#
#	22	#	71.18	#	1.05	#	4.35L+1	3*	1.50E	+114	5.92E+0	7#	8.19E-064	8.85E-1	12#
#	23	#	74.56	#	1.10	#	4.33E+1	3*	1.46E	+114	5.91E+0	7#	8.34E-064		
#	24	#	77.95		1.15	#	4.235+1				5.87E+0		0.42E-06*		
#	25	#	·		1.20	#					5.42E+U				
#	26	林	94.73		1.25	#					5.73E+0		9.35E-06*		
#	27	#			1.30		3.75E+1				5.64E+0		8.23E-364		
	23	#			1.35		3.eCE+1				5.53E+0		3.05E-06*		
	29	非社			1.40	#		_			5.41E+0 = 20E+0		7.83E-06* 7.56E-06*		
*	30 31	#			1.45 1.50		3.288+1						7.28E-064		
-	35		105.07		1.55	#	3.10E+1				5.00E+0				
	32	#	129.46		1.60	#	2.11E+1				4 . 34E+0		6.635-064		
#	34	4			1.65								6.298-064		
#	35	#	115.24		1.70	#	2.54E+1	3*	1.216	+11	¥ 4.52E+0	7#	5.92E-364	8.35E-	
#			119.03		1.75	Ħ	2.3EE+1	3*	1.205	+114	4 . 36E+0	7#	5.568-36	8.85E-	12#
#	37		122.01		1.80								5.198-06		
#	3.4	#			1.45								4.328-364		
#	39		123.79		1.90								4.4EE-06		
#			132.16		1.95								4.078-06		
#	41		135.57		2.00								3.76E-061		
#	42		139.96		2.15								3.395-064		
#	-		142.35		2.10								3.125-964		
#	44		145.74		2.15								2.78E+064 2.54E+064		
#		#	: 149.13 : 152.52		2.20 2.25								2.265-06		
#	46 47		155.31		2.29								2.05E-06		
*			157.32		2.35								1.846-06		
#	•		152.59										1.636-36		
*			166.08										1.435-36		
#			101.46										1.16E-06		
													=======================================		

BASE UNITS:

Quantita	2 6-24	al aumbol	
Quentity	<u>Unit</u>	SI Symbol	_Fermile_
length	metre		***
mass	kilogram	ke	***
time	second		•••
electric current	ampere	A	***
thermodynamic temperature	kelvin	K .	•••
amount of substance	mole .	mol	•••
luminous intensity	candela	cd	***
SUPPLEMENTARY UNITS:			
plane angle	redien	red	•••
solid angle	storedien	#	***
DERIVED UNITS:			
Acceleration	metre per second aquared		mis
activity (of a radioactive source)	disintegration per second	***	(disintegration)is
angular acceleration	radian per second squared	***	red/s
angular velocity	radian per second	***	red/s
eree	sdrate metre	•••	
density	kilogram per cubic metre	•••	kg/m
electric capacitance	fered	F	A-e/V
electrical conductance	siemens	S	AV
electric field strength	volt per metre	•••	V/m
electric inductance	henry	H	V-a/A W/A
electric potential difference	volt obs	V	W/A V/A
we are residence	ones voit	v ·	WIA
energy	ioule	3	N-m
entropy	joule per kelvin	•	VK
force	newton	 N	ke-m/s
fractioney	hertz	He	(cycle)/s
illuminance	lux	. lx	lm/m
lunvinance	candela per square metre	***	cd/sp
luminous flux	lumen	lm.	od-er
magnetic field strength	ampere per metre	***	A/m
regnetic flux	weber	WЪ	V-s
magnetic flux density	tesia	Ť	White
magnetomotive force	ampere	<u> </u>	
power	wett	w	y e.
pressure	pascal	Pe	N/m
quentity of electricity	coulomb	C	A-6
quantity of heat	joule	1	N-ca War
radiant intensity specific heat	watt per steradian	***	Wat Mg-K
stress	joule per kilogram-kelvin pascal	Pa	Nm
thermal conductivity	watt per metre-kelvin	• •	W/m-K
velocity	metre per second	***	m/s
viscosity, dynamic	pascal-second	***	Pa-a
viscosity, kinematic	square metre per second	***	m/s
voltage	volt	Ÿ	W/A
volume	cubic metre	•••	En .
wavenumber	reciprocal metre	•••	(weve)/m
work	joule]	N-m
	•	₹	

SI PREFIXES:

Multiplication Factors	Prof ix	SI Symbol
1 000 000 000 000 = 1012	lera	T
1 000 000 000 = 10°	gigo	G
$1000000 = 10^4$	maga	M
1 000 = 103	kilo	k
$100 = 10^2$	hecto*	h
10 = 10 ¹	deka*	de
$0.1 = 10^{-1}$	deci*	ď
$0.01 = 10^{-2}$	cesti*	Č
$0.001 = 10^{-1}$	milli	m
$0.000\ 001 = 10^{-6}$	micro	μ
0.004 000 001 = 10-4	neno	'n
$0.000000000001 = 10^{-12}$	pico	
0.000 000 000 000 001 = 10-15	femto	F
000 000 000 000 000 001 = 10-14	etto	

^{*} To be avoided where possible.

MISSION of Rome Air Development Center

RADC plans and conducts research, exploratory and advanced development programs in command, control, and communications (C³) activities, and in the C³ areas of information sciences and intelligence. The principal technical mission areas are communications, electromagnetic guidance and control, surveillance of ground and aerospace objects, intelligence data collection and handling, information system technology, icnospheric propagation, solid state sciences, microwave physics and electronic reliability, maintainability and compatibility.



